

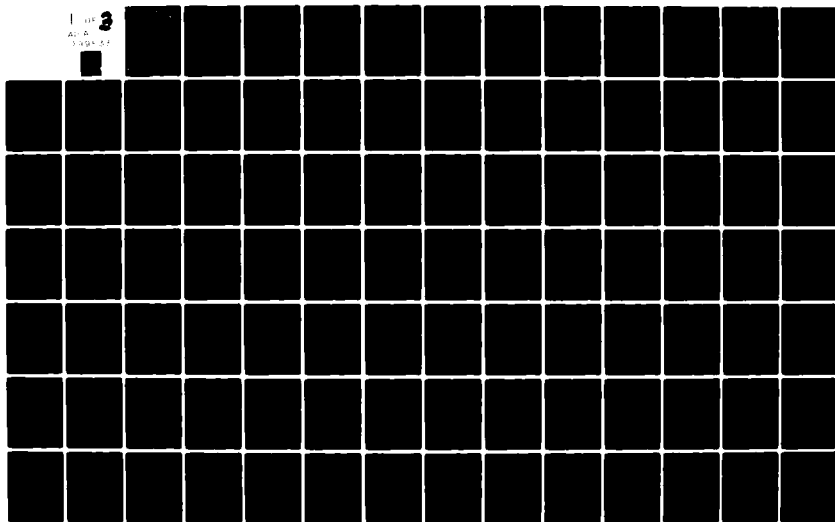
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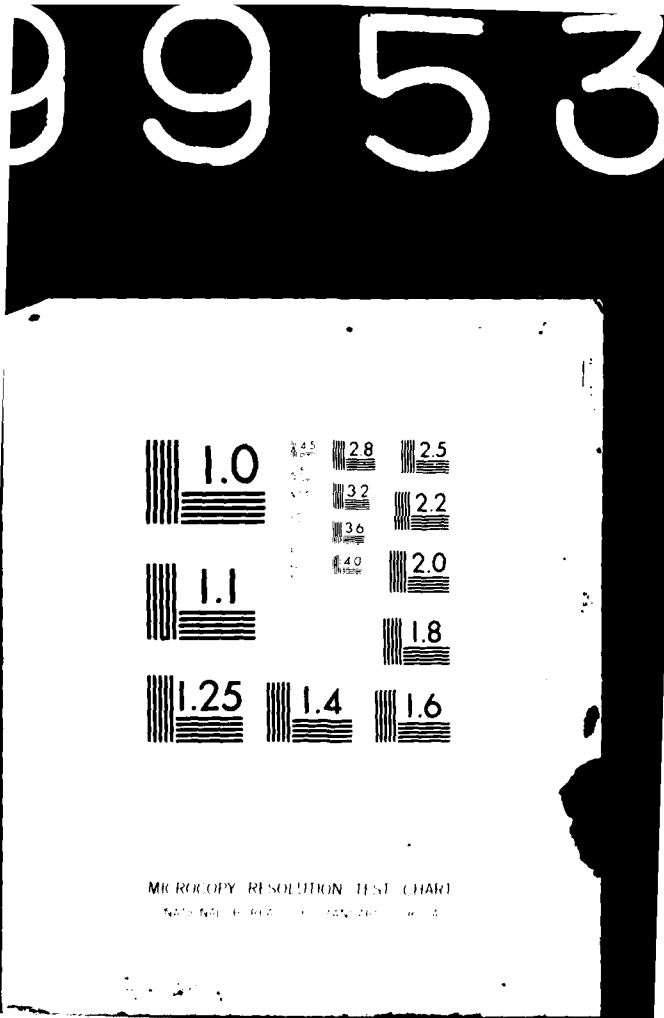
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DOCUMENTATION FOR SWATH SHIP RESISTANCE AND PROPULSION PREDICTION PROGRAMS  
(CLOSEFIT AND SYNTHESIS): MAINTENANCE MANUAL

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DAVID W. TAYLOR NAVAL SHIP  
RESEARCH AND DEVELOPMENT CENTER

Bethesda, Maryland 20084



DOCUMENTATION FOR SWATH SHIP  
RESISTANCE AND PROPULSION PREDICTION PROGRAMS

(CLOSEFIT AND SYNTHESIS):

MAINTENANCE MANUAL

Arthur M. Reed

Approved for Public Release: Distribution Unlimited

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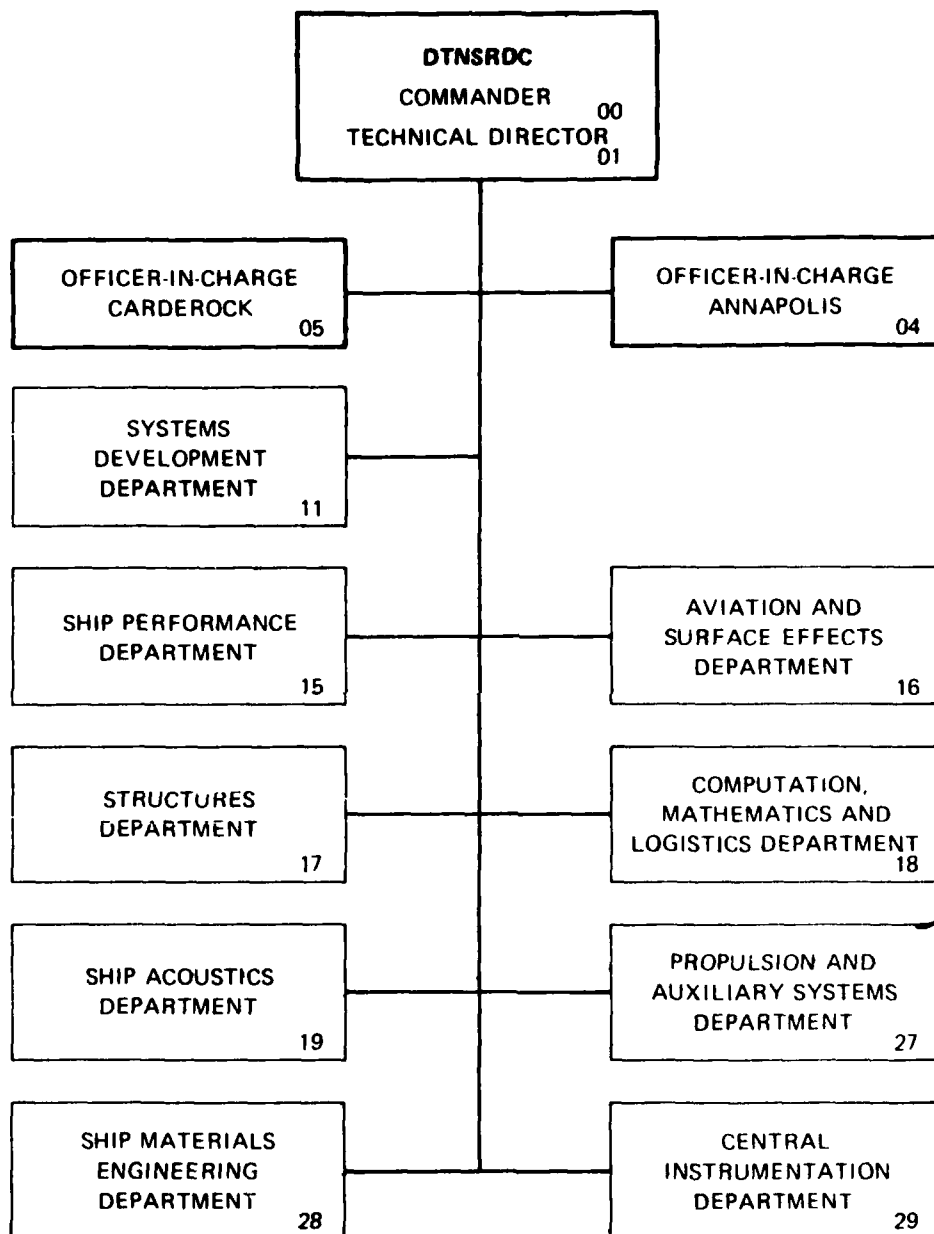
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of a SWATH ship's propulsive system at both design and off-design conditions.

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## NOMENCLATURE

<u>Symbol</u>	<u>Description</u>
$A(x)$	Body sectional area function
$A_o$	Maximum section area of body
$A_{Bm}$	Symmetric coefficients of Chebychev sine series for body
$A_{Sm}$	Symmetric coefficients of Chebychev sine series for strut
$A_{wp}$	Area of the waterplane
$b$	Half of the separation distance of the hulls
$B_{Bm}$	Anti-symmetric coefficients of Chebychev series for body
$B_{Sm}$	Anti-symmetric coefficients of chebychev sine series for strut
$C_A$	Correlation Allowance
$C_F$	Frictional resistance coefficient
$C_{Fm}$	Form drag coefficient
$C_P$	Body Prismatic coefficient
$C_{WP}$	Waterplane coefficient
$C_{IW}$	Waterplane inertia coefficient
$g$	Acceleration due to gravity
$h_B$	Maximum depth of submergence of axis of body
$h_S$	Maximum draft of strut
$J_n(a)$	Bessel functions
$L_B$	Maximum length of body
$L_S$	Maximum length of strut
$P_E$	Effective power

# NOMENCLATURE (CONT)

<u>Symbol</u>	<u>Description</u>
$R_n$	Reynolds number
$R$	Total ship resistance
$R_{WB}$	Wave resistance due to one main body
$R_F$	Frictional resistance
$R_{Fm}$	Eddy resistance
$R_{WS}$	Wave resistance due to one strut
$R_{WSB}$	Wave resistance due to the interaction of strut and main body
$R_W$	Wave resistance
$S$	Wetted surface
$T$	Thickness of mid length of strut
$t(x)$	Strut half thickness function
$T_{Bmn}$	Auxiliary function used in calculation of $R_B$
$T$ ( $T_{max}$ also used)	Thickness of mid length of strut
$T_{SBmn}$	Auxiliary wave resistance function used in calculation of $R_{SB}$
$T_{Smn}$	Auxiliary wave resistance function used in calculation of $R_S$
$U_m(x)$	Cheby chev cosine series
$V$	Velocity of ship
$V_m(x)$	Chebychev sin series
$W_{Bmn}$	Auxiliary wave resistance function used in calculation of $R_B$
$W_{Smn}$	Auxiliary wave resistance used in calculation of $R_S$

# NONMENCLATURE (CONT)

<u>Symbol</u>	<u>Description</u>
$W_{SBmn}$	Auxiliary wave resistance function used in calculation of $R_{SB}$ Variable of integration
$\rho$	Density of water
$\gamma_{OB}$	Dimensionless number related to body length and ship speed, used to remove singularities
$\gamma_{OS}$	Dimensionless number related to strut length and ship speed, used to remove singularities
$\zeta$	Variable of integration.

## ENGLISH/SI EQUIVALENTS

1 degree (angle)	= 0.01745 rad (radians)
1 foot	= 0.3048 m (meters)
1 foot per second (fps)	= 0.3048 m/sec (meters per second)
1 inch	= 25.40 mm (millimeters)
1 knot	= 0.5144 m/s (meters per second)
1 lb (force)	= 4.448 N (Newtons)
1 lb (force - inch lbs)	= 0.1130 N·m (Newton-meter)
1 long ton (2240 pounds)	= 1.016 metric tons; or 1016 kilograms
1 power	= 0.746 kW (kilowatts)

## ABSTRACT

This report documents two computer programs which determine the wave resistance and propulsive performance of Small-Waterplane-Area Twin-Hull (SWATH) ships. These programs are SYNTHESIS and CLOSEFIT, and they use as input data the moments and offsets of ship geometry, respectively. While they both employ linearized ship wave theory and thin-ship approximation and share many subroutines, CLOSEFIT is a more refined program capable of furnishing superior results. On the other hand, SYNTHESIS is simpler and includes several additional subroutines which can determine the characteristics and performance of a SWATH ship's propulsive system at both design and off-design conditions.

## ADMINISTRATIVE INFORMATION

This investigation was authorized under a direct funded block from the Naval Material Command (NAVMAT 08T23) under Program Element 62543N, Task Area ZF43-421-001, and funded through the High Performance Vehicles Office of the David W. Taylor Naval Ship Research and Development Center (DTNSRDC), Work Unit 1-1500-103.

## BACKGROUND

This report (Maintenance Manual) contains documentation for two computer programs, CLOSEFIT and SYNTHESIS, which have been developed at the David W. Taylor Naval Ship R&D Center (DTNSRDC) to predict the effective and delivered power for Small-Waterplane-Area Twin-Hull (SWATH) ships. This maintenance manual contains documentation for each subroutine in the programs, definitions of all of the variables in the COMMON BLOCKS, and a listing of the computer programs. This documentation is intended for the individual who must modify the computer programs, and must therefore be able to understand the functioning of the programs, and should be contrasted with the Users Manual, which serves to define the input to and output from the programs. The ability to prepare proper input, and to use the output does not require an understanding of the workings of the program.

SWATH ships are catamarans which combine a thin strut with a submerged elongated slender body. Each demi-hull of the SWATH has either one (single) or two (tandem) struts which support the lower hull. Figures 1 and 2 show schematic diagrams illustrating the geometry of single and tandem strut SWATH configurations, respectively.

Programs CLOSEFIT and SYNTHESIS have a similar theoretical foundation in that they are both based on linearized ship wave theory and the thin ship approximation in the framework of the potential flow of an incompressible, inviscid fluid. In general, thin-ship theory can be applied to any conventional catamaran with arbitrary camber. However, as this theory has been specialized to SWATH configurations, the ship geometry is

restricted to ships with "no-cross flow" cambers. In practice, this means SWATHS with very small strut thicknesses compared to the transverse strut separation.

In the theory of ship resistance extrapolation, the resistance of a ship is typically decomposed into residuary and frictional resistance components. The frictional resistance component is generally taken as equal to the resistance of a flat plate with area of the ship, and with length equal to the length of the ship. The three dimensional viscous effects are then included in the residuary resistance along with other resistance components such as wave making resistance. For a SWATH ship, the calculation of the frictional resistance is not as simple as stated above, however, the same principle applies if one calculated the frictional resistance of the bodies and struts separately.

The wave making resistance component of the residuary resistance can be computed using inviscid fluid flow theory. However, the other components of the residuary resistance are not easily calculated theoretically. Because of this, the remainder of the residuary resistance is computed empirically. The difference between the experimentally determined residuary resistance and the theoretically determined wave resistance is calculated for those cases where adequate experimental data exists. These differences which are denoted as "form drag", are then plotted as a function of strut speed-length ratio. Under the assumption that the form drag remains unchanged for reasonable changes of SWATH proportions, a curve can be faired through the individual form drag curves, and applied to new hull forms.

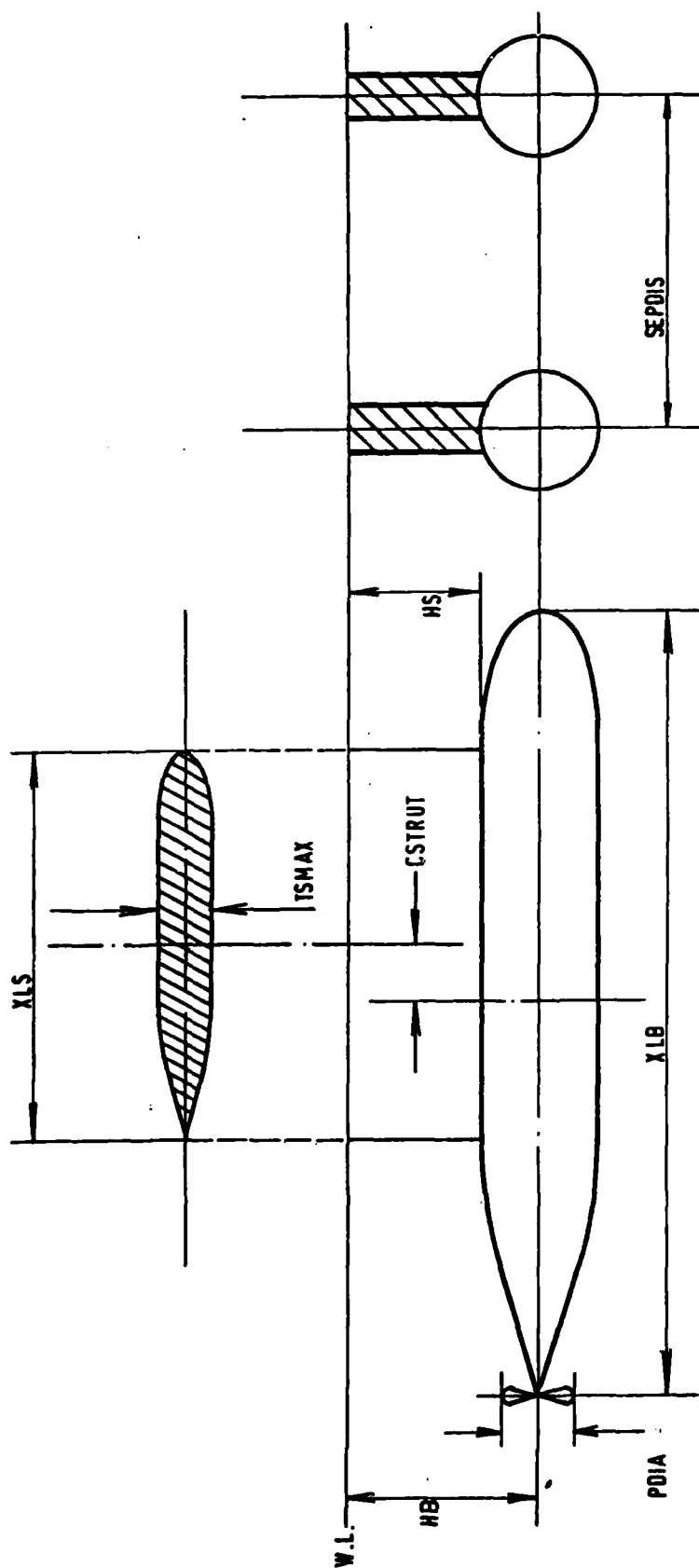


Figure 1 - Profile of SWATH Ship with Single Strut

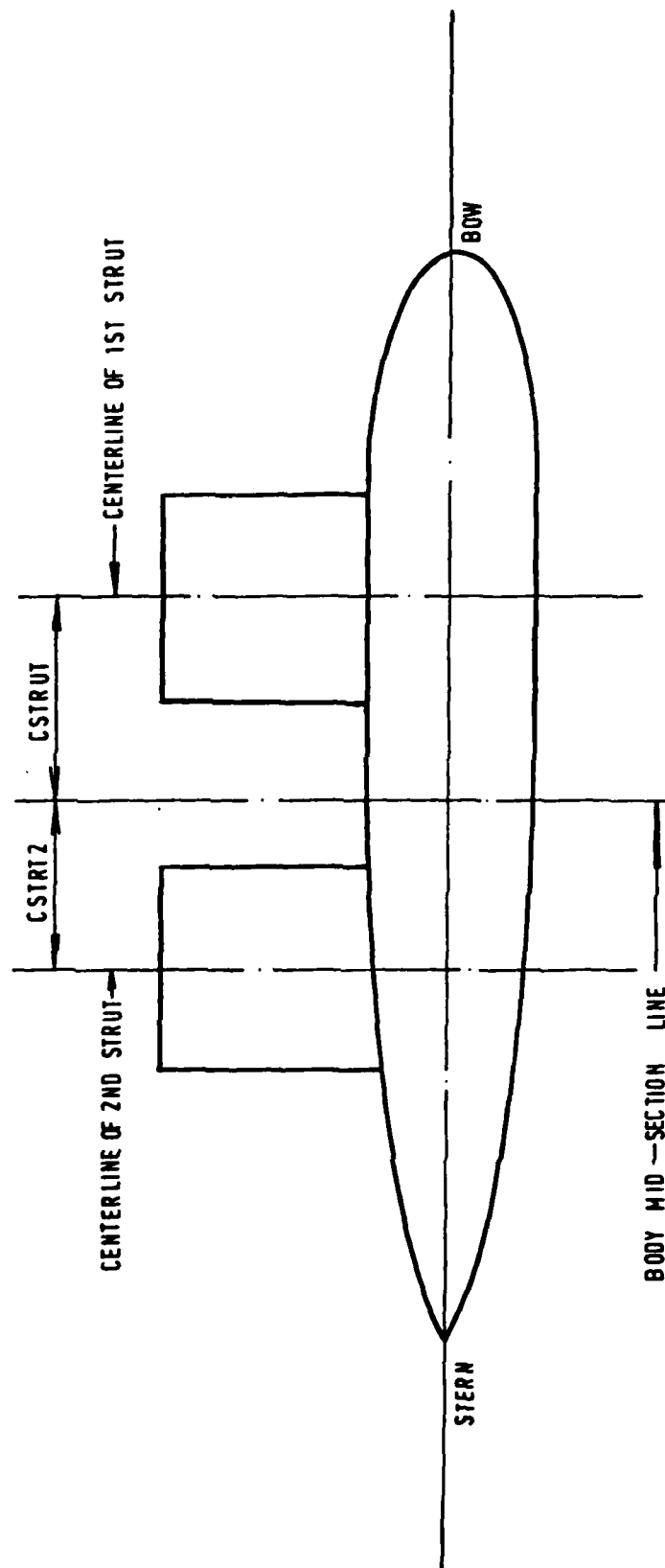


Figure 2 - Profile of SWATH Ship with Tandem Struts



For the wave resistance predictions, the geometries of the body and strut(s) are represented by modified Chebychev series. The methods used to determine these series are the principal differences between the programs CLOSEFIT and SYNTHESIS. The program CLOSEFIT uses an integration technique, similar to that used to determine the coefficients of a Fourier series, to determine the coefficients of the Chebychev series based on the actual hull offsets. The program SYNTHESIS uses statical moments of the strut waterplane and body to define the coefficients of the Chebychev series. Typically, the CLOSEFIT program uses a series of 10 to 20 pairs of terms to represent a body or strut, where each pair of terms contains an even and an odd Chebychev function, in the same fashion that a Fourier series consists of pairs of sine and cosine functions. The program SYNTHESIS uses a series consisting of only three pairs of terms to represent the body and strut. This reduction in the number of terms results in savings of ten to forty times in the computation of the wave resistance in SYNTHESIS as compared to CLOSEFIT.

In addition to the effective power computations, the program SYNTHESIS also computes the delivered power which would be required to propel the SWATH ship. The propulsion calculations are performed by a subprogram SHPCMP and its attendant subprograms. SHPCMP determines the wake and thrust deduction for the design based on empirical relations derived from earlier SWATH propulsion experiments. The program then calculated the optimum four bladed Troost series propeller at the design speed, along with the off design performance of the propeller. This data along with the effective power computations is used to calculate the delivered power.

## OVERVIEW OF CLOSEFIT

The CLOSEFIT SWATH program is composed of several modules, each of which consists of a number of subroutines and performs a specific function in the SWATH ship resistance calculation. Figure 1 presents a tree diagram which reflects the relationship among all subroutines.

Subroutine CHEB evaluates the coefficients of the Chebychev series, which represents the strut half thickness function and the body sectional area function in wave resistance equations. This is accomplished by calling READ, SCALE, COMPUT, CHECK and SURFACE. The offset tables are read in by Subroutine READ, then normalized by Subroutine SCALE. The driver Subroutine COMPUT calls Subroutine CHEV, which in turn calls SPLINE and SUMSPL to compute the coefficients of the Chebychev series. The integrals used to evaluate the strut Chebychev coefficients are as follows:

$$A_{sm} = \frac{2}{\pi} \int_{-\pi/2}^{\pi/2} t(\sin \theta) \cos(2m-1)\theta d\theta$$

$$B_{sm} = \frac{2}{\pi} \int_{-\pi/2}^{\pi/2} t(\sin \theta) \sin 2m\theta d\theta$$

where  $t(\sin \theta)$  is a function adopted to describe the offsets of the strut or the body. The Cubic Spline Function Technique is used to fit an analytic curve to the discrete offset points. Subroutine SPLINE solves

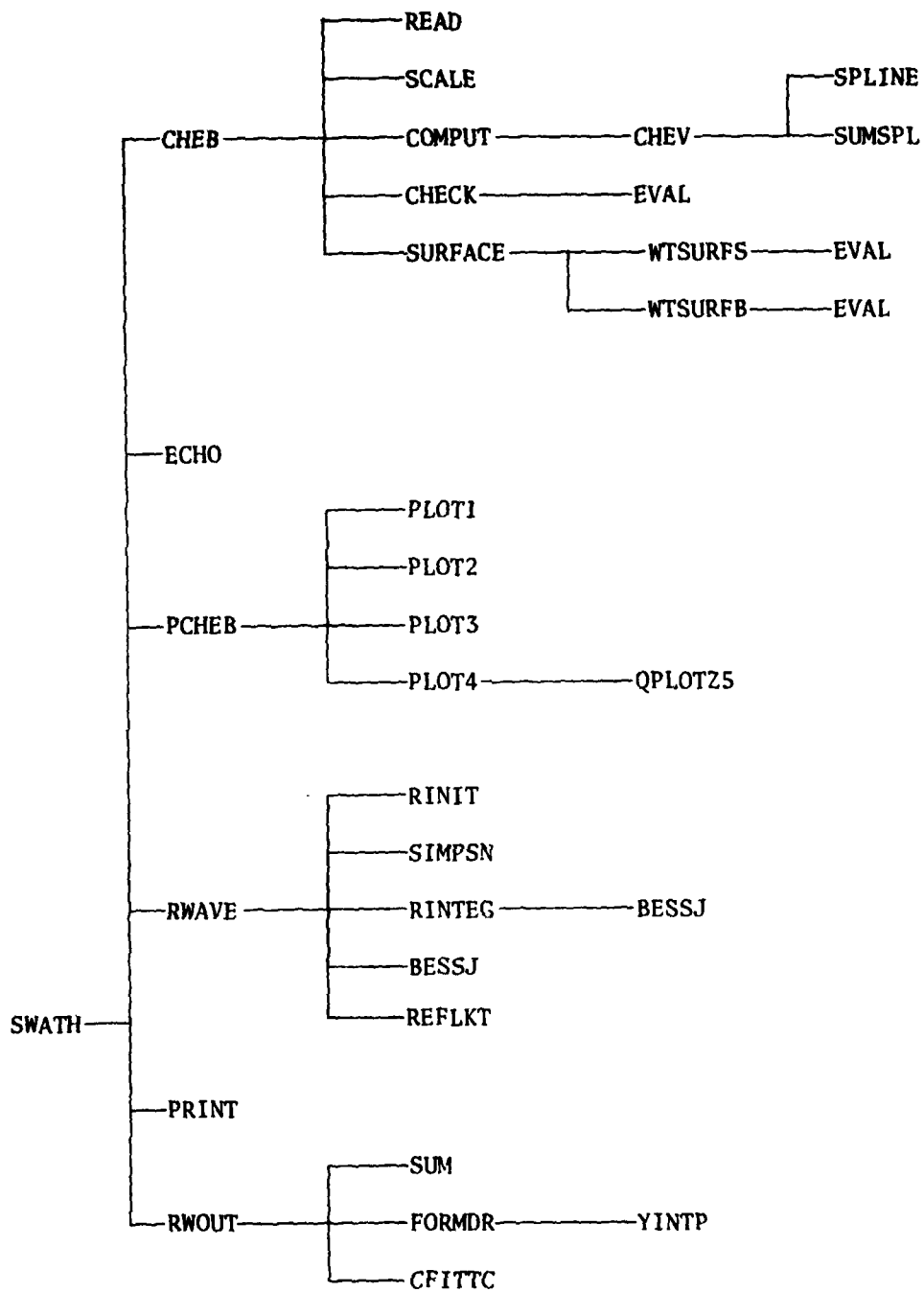


Figure 3 - Tree Diagram of CLOSEFIT SWATH Program

the set of simultaneous linear algebraic equations, which results from the spline fitting procedure and obtains the second derivatives of the analytical functions  $t(\sin \theta)$  at each offset point. Next, Subroutine SUMSPL uses these second derivatives in a set of integration formulas based on the Filon Quadrature Technique to evaluate the above trigonometric integrals. Subroutine CHECK evaluates the offsets approximated from the Chebychev series in Subroutine COMPUT and prints out the predicted offsets along with the true offsets. This permits a check on the accuracy of the Chebychev series approximations.

Subroutine SURFACE computes the total SWATH ship wetted surface by calling WTSURFS and WTSURFB. Subroutine ECHO echoes the input data of the SWATH program on the printer as a check of its accuracy. Subroutine PCHEB plots the strut half thickness curve and body sectional area curve on the printer in order to validate the Chebychev series approximation.

A large amount of the execution time of this program is spent in the evaluation of the auxiliary functions, T and W, given by:

$$\left\{ \begin{array}{c} \frac{T_{Smn}}{(2m-1)(2n-1)} \\ \frac{W_{Smn}}{(2m)(2n)} \end{array} \right\} = \int_{\gamma_{0S}}^{\infty} \frac{d\alpha}{\alpha^2 \sqrt{\alpha^2 - \gamma_{0S}^2}} D \left( \alpha; \frac{2b}{L_S}, \gamma_{0S} \right) \\ \times F_S^2(\alpha) \left\{ \begin{array}{c} J_{2m-1}(\alpha) J_{2n-1}(\alpha) \\ J_{2m}(\alpha) J_{2n}(\alpha) \end{array} \right\},$$

$$\left\{ \begin{array}{c} \frac{T_{Bmn}}{(2m-1)(2n-1)} \\ \frac{W_{Bmn}}{(2m)(2n)} \end{array} \right\} = \int_{\gamma_{0S}}^{\infty} d\alpha \frac{\alpha^2}{\sqrt{\alpha^2 - \gamma_{0S}^2}} D \left( \alpha; \frac{2b}{L_S}, \gamma_{0S} \right) \\ \times F_B^2(\beta) \left\{ \begin{array}{c} J_{2m-1}(\beta) J_{2n-1}(\beta) \\ J_{2m}(\beta) J_{2n}(\beta) \end{array} \right\}$$

$$\left\{ \frac{T_{SBmn}}{(2m-1)(2n-1)} \right\} = \int_{\gamma_{0S}}^{\infty} \frac{d\alpha}{\sqrt{\alpha^2 - \gamma_{0S}}} D\left(\alpha; \frac{2b}{L_S}, \gamma_{0S}\right) \\ \times E_S(\alpha) E_B(\beta) \left\{ \frac{J_{2m-1}(\alpha) J_{2n-1}(\beta)}{J_{2m}(\alpha) J_{2n}(\beta)} \right\}.$$

Due to the highly oscillatory nature of the integrands of these auxiliary functions, the integration range is divided into three separate intervals. For each interval, a particular numerical integration method is used to improve the accuracy of the calculation. To avoid the singularity in the denominator of the integrand, the integration variable ( $\alpha$ ) is replaced by  $Z = \sqrt{\alpha - \gamma_{0S}}$  in the interval from  $\gamma_{0S}$  to  $\gamma_{0S} + 1$ . The numerical method used in this interval is Simpson's Rule, which uses 30 points. The central region of the integration process goes from  $\alpha = \gamma_{0S} + 1$  to  $\alpha = \alpha_{\max}$ . The choice of  $\alpha_{\max}$  is based on the requirement for accuracy in the numerical integration method used in this region, where a step size is computed at a given  $\alpha$ , and a three-point Simpson's Rule is used until the upper integration limit of the region,  $\alpha_{\max}$ , is reached.

An analytical integration formula was developed to determine the effects of the final region, from  $\alpha = \alpha_{\max}$  to  $\alpha = \alpha_{l_{\max}}$ , where  $\alpha_{l_{\max}}$  is an empirical constant which defines the upper limit of the tail region. Beyond this point, the integration area is assumed to be negligible.

Subroutine PRINT will print the table of the T and W arrays, provided the flag JTEST is set other than zero.

Subroutine RWOUT calls SUM to evaluate the components of the wave

resistance, based on Lin and Day's equations<sup>1</sup>. Form drag is evaluated by Subroutine FORMDR, which is based on experimental data. Frictional drag is estimated by calling Subroutine CFITTC, which is based on the  $C_F$  curve adopted by the International Towing Tank Conference (ITTC)<sup>2</sup>. For each test speed, a table is printed showing all the components of total ship resistance and the effective power required to tow the SWATH ship at a constant speed.

---

<sup>1</sup>References are listed on page 112.

## OVERVIEW OF SYNTHESIS

The procedure of the SYNTHESIS SWATH program parallels the CLOSEFIT program in calculating total ship resistance, except in its approach to obtaining the coefficients of the Chebychev series. In SYNTHESIS, the waterplane area coefficients, waterplane moment, waterplane inertia, body prismatic and body moment are used to evaluate the Chebychev coefficients. The only other major difference between the two programs is that SYNTHESIS includes a propeller design and optimization program.

Figure 2 presents the tree diagram of all subroutines called by the SYNTHESIS program. The module CHEB is much simpler in SYNTHESIS than its CLOSEFIT counterpart due to its approach in evaluating the Chebychev coefficients through geometric identities as opposed to numerical integrations.

Modules RWAVE and ROUT are identical for both programs, and in both require a great deal of execution time.

Module FINDRG evaluates the fin drag of a SWATH ship. It is directly excerpted from coding documented in reference (3).

Module SHPCMP can determine propeller design and off-design performance if the propeller diameter is specified. The subroutines used in this module are excerpted from coding documented in reference (4).

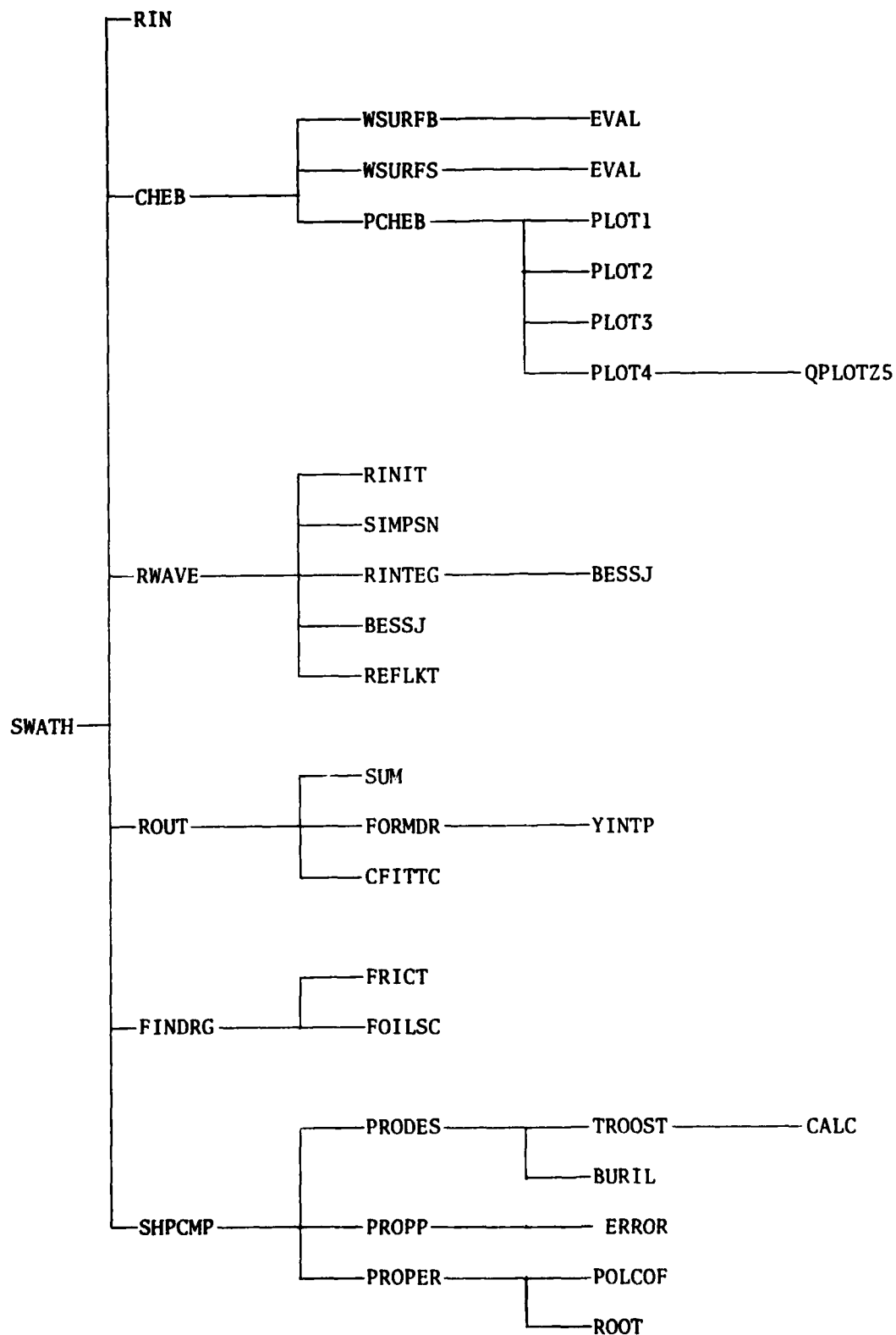


FIGURE 4 - Tree Diagram of SYNTHESIS SWATH Program



PROGRAM DOCUMENTATION OF CLOSEFIT

COMMON BLOCK DEFINITIONS FOR CLOSEFIT

COMMON/AUX/

PURPOSE: AUX stores the auxiliary function table.

NAME	TYPE	LENGTH	DEFINITION
TS	R	(10,10)	Auxiliary function T for strut
WS	R	(10,10)	Auxiliary function W for strut
TB	R	(10,10)	Auxiliary function T for body
WB	R	(10,10)	Auxiliary function W for body
TSB	R	(10,10)	Auxiliary function T for strut to body
WSB	R	(10,10)	Auxiliary function W for strut to body
TS12	R	(10,10)	Auxiliary function T for strut 1 to strut 2
WS12	R	(8,10,10)	Auxiliary function W for strut 1 to strut 2
TB12	R	(8,10,10)	Auxiliary function T for body 1 to body 2
WB12	R	(8,10,10)	Auxiliary function W for body 1 to body 2
TSB12	R	(8,10,10)	Auxiliary function T for strut 1 to body 2
WSB12	R	(8,10,10)	Auxiliary function W for strut 1 to body 2
TSBP	R	(10,10)	Auxiliary function T
WSBP	R	(10,10)	Auxiliary function W
TSB12P	R	(10,10)	Auxiliary function T
WSB12P	R	(10,10)	Auxiliary function W

COMMON/NAME/

PURPOSE: NAME stores a flag indicating whether the offset data are for the strut or the body and providing the alphanumeric information for the strut and the body.

NAME	TYPE	LENGTH	DEFINITION
INCHAR	I	8	INCHAR (1) = STRUT. Strut offset data will follow.  INCHAR (1) = BODY. Body offset data will follow.  INCHAR (2) to INCHAR (8). Hold the alphanumeric information for the strut or the body.
NAME	I	7	Temporary storage location for alphanumeric strut or body information.

COMMON/NORM/

PURPOSE: NORM stores the scaling factors for normalizing X and Y.

NAME	TYPE	LENGTH	DEFINITION
YMAX	R		Maximum value of Y
XDIVER	R		Divisor for normalizing X
YDIVER	R		Divisor for normalizing Y
XADDER	R		Number to be added to normalize X

COMMON/OMEGA/

PURPOSE: OMEGA stores the variables used in evaluating the auxiliary function.

NAME	TYPE	LENGTH	DEFINITION
NMAX	I		Maximum order of Chebychev Series
HSOLS	R		Ratio of draft of strut to length of strut ( $h_s/L_s$ )
HBOLB	R		Ratio of depth of submergence to length of body ( $h_b/L_b$ )
GAMAOS	R		$\gamma_{os} = \frac{1}{2} g L_s / v^2$
GMAOB	R		$\gamma_{ob} = \frac{1}{2} g L_b / v^2$
NOSEPS	I		Number of different hull separation distances
SEPDIS	R	(8)	Hull separation distance b (ft)
SEP	R	(8)	$2b/(\gamma_{os} \cdot L_s)$
CSTRUT	R	(8)	Distance of CL of strut to CL of body
CSTRT2	R	(8)	Distance of CL of 2nd strut (if present) from CL of body
GOSQ	R		$\gamma_{os}^2$
PHIS	R		$2(\frac{h_s}{L_s})/\gamma_{os}$
PHIB	R		$2(\frac{h_b}{L_b})/\gamma_{ob}$
RATIOI	R		$\gamma_{ob}/\gamma_{os}$

COMMON/OUT/

PURPOSE: OUT defines and stores physical constants and geometric parameters.

NAME	TYPE	LENGTH	DEFINITION	SET VALUES
HS	R		Draft of strut $h_s$ (ft)	
HB	R		Depth of submergence from surface to body centerline $h_b$ (ft)	
XLS	R		Length of strut $L_s$ (ft)	
XLB	R		Length of body $L_b$ (ft)	
TSMAX	R		Maximum thickness of strut $t_{max}$ (ft)	
AX	R		Maximum cross-sectional area of body $A_x$ (ft <sup>2</sup> )	
PI	R		3.1415926535897	
G	R		Acceleration due to gravity $g$ (ft/sec <sup>2</sup> )	32.155
RHO	R		Density of water $\rho$ (lb x sec <sup>2</sup> /ft <sup>4</sup> )	1.9367
GNU	R		kinematic viscosity $\nu$ (ft <sup>2</sup> /sec)	$1.2970 \times 10^5$
WETS	R		Wetted surface area of strut $S_s$ (ft <sup>2</sup> )	
WETB	R		Wetted surface area of body $S_b$ (ft <sup>2</sup> )	
WTSURF	R		Total wetted surface area $S_t$ (ft <sup>2</sup> )	
VMFPS	R		Test velocity $V$ (fps)	
DELCF	R		Correction allowance $\Delta C_F$	0.0005
TITLE	I	(8)	Array of characters containing the title of the test	

COMMON/PLOT/

PURPOSE: PLOT stores the constants and characters for the plotting routine

NAME	TYPE	LENGTH	DEFINITION	SET VALUES
NFIRST	I		Position in the arrays of the first ordered pair to be plotted	1
NLAST	I		Position in the arrays of the last ordered pair to be plotted	101
NPOINT	I		NPOINT equals "1" each point from NFIRST to NLAST is to be plotted, "2" if every other point is to be plotted, etc.	1
NMAX	R		Value of abscissa at right-most grid line	1.0
XMIN	R		Value of abscissa at left-most grid line	-1.0
NSCLI	L		Logical value (Should be false if PLOTI has not been called and standard grid is desired)	
NCHAR	I		Number of valid characters in label	
NSCALE	I	(4)	Printing scale factor of ordinate	
PCHAR	I	(2)	Plotting characters	



COMMON/PSI/

PURPOSE: PSI stores the parameters for the integration procedure

NAME	TYPE	LENGTH	DEFINITION	SET VALUES
NPTSZ	I		Number of integration steps from $\gamma$ to $\gamma+1$ (odd number) os os	31
PTSFA	R		Scaling factor of step size in integrating from $\alpha_{\max}$ to $\alpha_{\ell\max}$	10.0
EXPN	R		Empirical constant for intergration to stop	7.0
NALMAX	I		Maximum number of integration steps from $\gamma+1$ to $\alpha_{\max}$ os	300
NAL	I		Counter of integration steps	
TAIL	R		Integration made from $\alpha$ to $\alpha_{\ell\max}$	
ALFA	R		Integrating variable ( $\alpha$ )	
ALMAX	R		Upper limit of $\alpha$ for integration	
NSTEPS	I		Number of integration steps from $\alpha_{\max}$ to $\alpha_{\ell\max}$	

COMMON/XRPLTF/

PURPOSE: XRPLTF stores the values of variables for the plotting routine

NAME	TYPE	LENGTH	DEFINITION
XL	R		Value of abscissa at left-most grid line
XH	R		Value of abscissa at right-most grid line
YL	R		Value of ordinate at bottom grid line
YH	R		Value of ordinate at top grid line
XMOV	R		Abscissa index increment number for array GRAF
YMOV	R		Ordinate index increment number for array GRAF

COMMON/XRPLTG/

PURPOSE: XEPLTG stores the values and characters of variables for the plotting routine

NAME	TYPE	LENGTH	DEFINITION
GRAF	I	(11,204)	Array containing the image to be plotted

COMMON/XRPLQTQ/

PURPOSE: XRPLQTQ stores the constants and characters for the plotting routine

NAME	TYPE	LENGTH	DEFINITION	SET VALUES
II	I		Ordinate scale factor	
JJ	I		Ordinate scale factor	
KK	I		Ordinate scale factor	
LL	I		Ordinate scale factor	
NHL	I		Number of horizontal grid lines	6
NSBH	I		Number of spaces between adjacent horizontal grid lines	10
NVL	I		Number of vertical grid lines	11
NSBV	I		Number of spaces between adjacent vertical grid lines	10
NCHAR	I		Plotting character of horizontal grid lines	1H.
VCHAR	I		Plotting character of vertical grid lines	1H.
IY	I		Number of vertical spaces	
IX	I		Number of horizontal spaces	
V	L		Logical variable, = . TRUE . when the maximum and minimum values of the ordinate are determined	
H	L		Logical variable, = . TRUE . when the maximum and minimum values of the abscissa are determined	

SUBROUTINE DOCUMENTATION FOR CLOSEFIT

**NAME:** PROGRAM SWATH

**PURPOSE:** Program SWATH is the main program for the  
CLOSEFIT resistance prediction of Small-Water-  
plane-Area Twin-Hull Ships

**CALLING SERVICE:** Program SWATH (INPUT, OUTPUT, TAPE5 = INPUT  
TAPE6 = OUTPUT, TAPE8)

**ARGUMENTS:** NONE

**COMMON BLOCKS:** OUT, AUX, OMEGA, PSI, COEFS

**SUBROUTINES CALLED:** CHEB, ECHO, PCHEB, PRINT, RWAVE, RWOUT

**COMMENTS:**

NAME:	SUBROUTINE BESSJ
PURPOSE:	SUBROUTINE BESSJ evaluates the Bessel function from order 0 to order N.
CALLING SEQUENCE:	CALL BESSJ (X, N, VJ)
ARGUMENTS:	<p>X    Argument of the Bessel function</p> <p>N    Maximum order of the Bessel function</p> <p>VJ   Array holding (N+1) values of the Bessel function of order zero up to N, where</p> <p style="margin-left: 100px;"><math>VJ(0) = J_0(X)</math></p> <p style="margin-left: 100px;">.</p> <p style="margin-left: 100px;">.</p> <p style="margin-left: 100px;">.</p> <p style="margin-left: 100px;"><math>VJ(N) = J_N(X)</math></p>
COMMON BLOCKS:	NONE
SUBROUTINE CALLED:	NONE
CALLED BY:	RINTEG, RWAVE
COMMENTS:	

NAME: FUNCTION CFITTC

PURPOSE: Function CFITTC determines the ITTC  
frictional resistance coefficient  $C_f$

CALLING SEQUENCE: CF = CFITTC (RN)

ARGUMENT: RN Reynolds number  $R_n$  at test condition

COMMON BLOCKS: NONE

SUBROUTINE CALLED: NONE

CALLED BY: RWOUT

COMMENTS:

$$C_f = \frac{0.075}{[\log_{10}(R_n) - 2]^2}$$



NAME:	SUBROUTINE CHEB	
PURPOSE:	Subroutine CHEB computes from offset tables the coefficients of the Chebychev Series, which is an approximation of the outline of the waterplane area or body cross-sectional area curve.	
CALLING SEQUENCE:	CALL CHEB (AMC, BMC, MMAX)	
ARGUMENTS:	AMC	Coefficients of the Chebychev Cosine Series
	BMC	Coefficients of the Chebychev Sine Series
	MMAX	Maximum order of the Chebychev Series
COMMON BLOCKS:	NAVME, OFFSET	
SUBROUTINES CALLED:	READ, SCALE, COMPUT, CHECK, SURFACE	
CALLED BY:	SWATH	
COMMENTS:		

NAME:	SUBROUTINE CHEB	
PURPOSE:	Subroutine CHEB computes from offset tables the coefficients of the Chebychev Series, which is an approximation of the outline of the waterplane area or body cross-sectional area curve.	
CALLING SEQUENCE:	CALL CHEB (AMC, BMC, MMAX)	
ARGUMENTS:	AMC	Coefficients of the Chebychev Cosine Series
	BMC	Coefficients of the Chebychev Sine Series
	MMAX	Maximum order of the Chebychev Series
COMMON BLOCKS:	NAME, OFFSET	
SUBROUTINES CALLED:	READ, SCALE, COMPUT, CHECK, SURFACE	
CALLED BY:	SWATH	
COMMENTS:		

NAME:	SUBROUTINE CHECK	
PURPOSE:	Subroutine CHECK evaluates the Chebychev Series from the Chebychev coefficients obtained from Subroutine COMPUT and prints out the evaluated offset table for manual checking.	
CALLING SEQUENCE:	CALL CHECK (AMC, BMC, MMAX, ISBODY)	
ARGUMENTS:	AMC	Coefficients of the Chebychev Cosine Series
	BMC	Coefficients of the Chebychev Sine Series
	MMAX	Maximum order of the Chebychev polynomial
	ISBODY	Logical flag, indicating "Is this for body?"
	ISBODY = {	. TRUE . for body
		. FALSE . for strut
COMMON BLOCKS:	OFFSET, NAME	
SUBROUTINE CALLED:	EVAL	
CALLED BY:	CHEB	
COMMENTS:		

NAME:	SUBROUTINE CHEV	
PURPOSE:	Subroutine CHEV uses the offsets to compute the Chebychev coefficients via spline approximation and numerical integration.	
CALLING SEQUENCE:	AMC	Coefficients of the Chebychev Cosine Series
	BMC	Coefficients of the Chebychev Sine Series
	MMA	Maximum order of the Chebychev polynomial
	ISBODY	Logical flag, indicating "Is this for body?"
	ISBODY =	$\left\{ \begin{array}{l} . \text{ TRUE } . \text{ for body} \\ . \text{ FALSE } . \text{ for strut} \end{array} \right.$
COMMON BLOCKS:	OFFSET, NAME	
SUBROUTINES CALLED:	SPLINE, FUNCTION SUMPSPL	
CALLED BY:	COMPUT	
COMMENTS:		

NAME:	SUBROUTINE COMPUT	
PURPOSE:	Subroutine COMPUT initiates the computation of the Chebychev coefficients.	
CALLING SEQUENCE:	CALL COMPUT (AMC, BMC, MMAX, ISBODY)	
ARGUMENTS:	AMC	Coefficients of the Chebychev Cosine Series
	BMC	Coefficients of the Chebychev Sine Series
	MMAX	Maximum order of the Chebychev polynomials
	ISBODY	Logical flag, indicating "Is this for body?"
	ISBODY = {	. TRUE . for body
		. FALSE . for strut
COMMON BLOCKS:	OFFSET, NAME, NORM	
SUBROUTINE CALLED:	CHEV	
CALLED BY:	CHEB	
COMMENTS:		

NAME: SUBROUTINE ECHO

PURPOSE: Subroutine ECHO prints a summary of input data and  
the Chebychev coefficients

CALLING SEQUENCE: CALL ECHO (NLOC)

ARGUMENT: NLOC Number of strut locations to be  
tested

COMMON BLOCKS: AUX, OMEGA, OUT

SUBROUTINE CALLED: NONE

CALLED BY: SWATH

COMMENTS:

NAME:	SUBROUTINE EVAL	
PURPOSE:	Subroutine EVAL evaluates the Chebychev Series at a given station.	
CALLING SEQUENCE:	CALL EVAL (XX, MMAX, FFSET, AMC, BMC)	
ARGUMENTS:	XX	Value of X station on a range of -1 to +1
	MMAX	Maximum order of the Chebychev polynomial
	FFSET	Offset approximated by the Chebychev Series
	AMC	Coefficients of the Chebychev Cosine Series
	BMC	Coefficients of the Chebychev Sine Series
COMMON BLOCKS:	NONE	
SUBROUTINE CALLED:	NONE	
CALLED BY:	CHECK	
COMMENTS:		

NAME: FUNCTION FORMDR

PURPOSE: Function FORMDR evaluates the form drag coefficient, based on experimental data

CALLING SEQUENCE: FOR = FORMDR (VL)

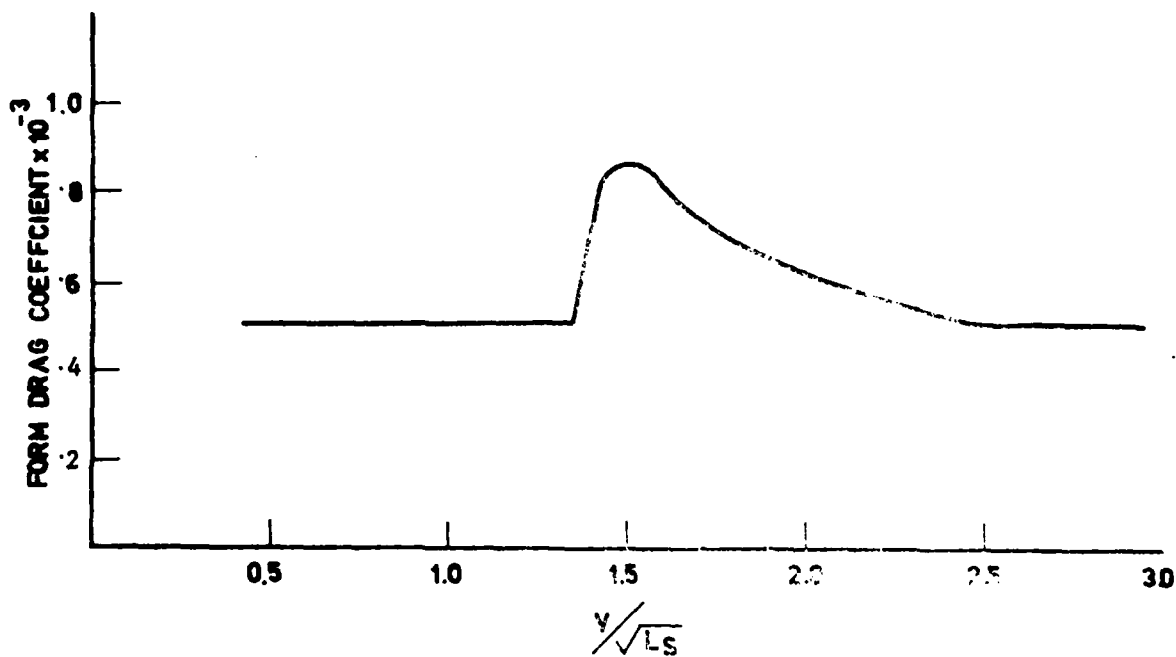
ARGUMENT: VL Ratio of ship speed to length of strut  $V/\sqrt{L_s}$

COMMON BLOCKS: NONE

SUBROUTINE CALLED: FUNCTION YINTP

CALLED BY: ROUT

COMMENTS: Form drag is assumed to be  $0.5 \times 10^{-3}$  for  $V/\sqrt{L_s}$  less than 1.325 and greater than 2.5





<b>NAME:</b>	<b>SUBROUTINE PCHEB</b>
<b>PURPOSE:</b>	Subroutine PCHEB plots by line printer the body sectional area curve and waterplane outline curve from the given Chebychev coefficients
<b>CALLING SEQUENCE:</b>	CALL PCHEB (AS, BS, AB, BB, NN, TITLE)
<b>ARGUMENTS:</b>	<p>AS      Coefficients of Chebychev Sine Series for strut</p> <p>BS      Coefficients of Chebychev Cosine Series for strut</p> <p>AB      Coefficients of Chebychev Sine Series for body</p> <p>BB      Coefficient of Chebychev Cosine Series for body</p> <p>NN      Maximum order of Chebychev Series</p> <p>TITLE   Array containing the alphanumeric characters of the title of the experiment</p>
<b>COMMON BLOCKS:</b>	PLOT, XRPLQT
<b>SUBROUTINES CALLED:</b>	PLOT1, PLOT2, PLOT3, PLOT4
<b>CALLED BY:</b>	CHEB
<b>COMMENTS:</b>	

NAME: SUBROUTINE PLOT1

PURPOSE: Subroutine PLOT1 sets up spacing and determines the values of the axes.

CALLING SEQUENCE: CALL PLOT 1 (NSCALE, A, B, C, D, E, F)

ARGUMENTS:

NSCALE	Integer array defined as follows:
NSCALE (1)	= I, if printed values of the ordinate are $10^{**} I$ times the actual value
NSCALE (2)	= J, if printed values of the ordinate are $10^{**} J$ times the actual value
NSCALE (3)	= K, if printed values of the abscissa are $10^{**} K$ times the actual values
NSCALE (4)	= L, if printed values of the abscissa are $10^{**} L$ times the actual value
A	Integer number of horizontal grid lines
B	Integer number of spaces beyond each horizontal grid line to the next grid line
C	Integer number of vertical grid lines
D	Integer number of spaces beyond each vertical grid line to the next grid line
E	Horizontal grid character
F	Vertical grid character

COMMON BLOCK: XRPLQT

SUBROUTINE CALLED: NONE

CALLED BY PCHEB

COMMENTS:

<b>NAME:</b>	<b>SUBROUTINE PLOT2</b>	
<b>PURPOSE:</b>	Subroutine PLOT2 examines the minimum and maximum values of the abscissa and the ordinate and establishes an internal formula for computing location in the image region corresponding to the point to be plotted.	
<b>CALLING SEQUENCE:</b>	CALL PLOT2 (XMAX, XMIN, YMAX, YMIN, NSCLI)	
<b>ARGUMENTS:</b>	XMAX	Value of abscissa at right-most grid line
	XMIN	Value of abscissa at left-most grid line
	YMAX	Value of ordinate at top grid line
	YMIN	Value of ordinate at bottom grid line
	NSCLI	Logical flat (should be .FALSE., if PLOT1 has not been called and standard grid is desired)
<b>COMMON BLOCKS:</b>	XRPLTF, SRPLTQ, XRPLTG	
<b>SUBROUTINE CALLED:</b>	NONE	
<b>CALLED BY:</b>	PCHEB	
<b>COMMENTS:</b>		

NAME: SUBROUTINE PLOT3

PURPOSE: Subroutine PLOT3 assigns an alpha-character to each point to be plotted.

CALLING SEQUENCE: CALL PLOT3 (PCHAR, X, Y, SDATA, FDATA, DDATA)

ARGUMENTS:

PCHAR	Plotting character
X	Array containing the X coordinates to be plotted
Y	Array containing the Y coordinates to be plotted
SDATA	Integer position in the arrays of the first ordered pair to be plotted
FDATA	<div style="display: inline-block; vertical-align: middle;"> <div style="font-size: 2em; vertical-align: middle;">{</div> <div style="display: inline-block; vertical-align: middle;"> 1 if each point from SDATA to DDATA is to be plotted  2 if every other point is to be plotted  3 if every third point is to be plotted </div> </div>
DDATA	Integer position in the array of the last ordered pair to be plotted

COMMON BLOCKS: XRPLTF, XRPLTG

SUBROUTINE CALLED: NONE

CALLED BY: PCHEB

COMMENTS:

NAME:	SUBROUTINE PLOT4	
PURPOSE:	Subroutine PLOT4 prints the image of the completed graph on the printer, including the values of the abscissa and the ordinate at the grid lines outside the bottom and left edge of the graph.	
CALLING SEQUENCE:	CALL PLOT4 (MCHAR, NCHAR)	
ARGUMENTS:	MCHAR	Single dimension array containing alpha-characters to be plotted at the left of the graph
	NCHAR	Number of valid characters in MCHAR
COMMON BLOCKS:	XRPLOTF, XRPLOTG, XRPLOTQ	
SUBROUTINE CALLED:	QPLOTZ5	
CALLED BY:	PCHEB	
COMMENTS:		

NAME:	SUBROUTINE PRINT								
PURPOSE:	Subroutine PRINT prints the auxiliary function tables of T and W.								
CALLING SEQUENCE:	CALL PRINT (I, NLOC2)								
ARGUMENTS:	<table border="0"> <tr> <td>I</td> <td>Index indicating strut location</td> </tr> <tr> <td>NLOC2</td> <td>Flag indicating the presence of a second strut</td> </tr> <tr> <td>NLOC2</td> <td>= { 0 if single strut</td> </tr> <tr> <td></td> <td>1 if tandem struts</td> </tr> </table>	I	Index indicating strut location	NLOC2	Flag indicating the presence of a second strut	NLOC2	= { 0 if single strut		1 if tandem struts
I	Index indicating strut location								
NLOC2	Flag indicating the presence of a second strut								
NLOC2	= { 0 if single strut								
	1 if tandem struts								
COMMON BLOCKS:	OUT, AUX, OMEGA								
SUBROUTINE CALLED:	NONE								
CALLED BY:	SWATH								
COMMENTS:									

NAME: SUBROUTINE QPLOTZ5

PURPOSE: Subroutine QPLOTZ5 calculates the scaling information needed to generate the format to label the left-hand side of the program.

CALLING SEQUENCE: CALL QPLOTZ5 (PDQ)

ARGUMENT: PDQ      Scaling factor for ordinate plot

COMMON BLOCKS: XRPLOTF, XRPLOTQ

SUBROUTINES CALLED: NONE

COMMENTS:

NAME:	SUBROUTINE READ
PURPOSE:	Subroutine READ reads the offset data of the strut or body and checks for error.
CALLING SEQUENCE:	CALL READ
ARGUMENTS:	NONE
COMMON BLOCKS:	OFFSET, NAME, NORM
SUBROUTINE CALLED:	NONE
CALLED BY:	CHEB
COMMENTS:	



NAME:	SUBROUTINE REFLKT
PURPOSE:	Subroutine REFLKT reflects all the symmetrical matrices of T and W.
CALLING SEQUENCE:	CALL REFLKT
ARGUMENTS:	NONE
COMMON BLOCKS:	AUX, OMEGA
SUBROUTINE CALLED:	NONE
CALLED BY:	RWAVE
COMMENTS:	

NAME: SUBROUTINE RINIT

PURPOSE: Subroutine RINIT initializes the T and W arrays to zero.

CALLING SEQUENCE: CALL RINIT

ARGUMENT: NONE

COMMON BLOCKS: AUX, OMEGA

SUBROUTINE CALLED: NONE

CALLED BY: RWAVE

COMMENTS:

NAME:	SUBROUTINE RINTEG																		
PURPOSE:	Subroutine RINTEG evaluates the integrand for T and W functions.																		
CALLING SEQUENCE:	CALL RINTEG (ALFA, B, D, NLOC2, WTINT, SEPCOS, SQ)																		
ARGUMENTS:	<table border="0"> <tr> <td>ALFA</td> <td>Integrating variable <math>\alpha</math></td> </tr> <tr> <td>B</td> <td>CSTRUT(I)/XLS</td> </tr> <tr> <td>D</td> <td>CSTRT2(I)/XLS</td> </tr> <tr> <td>NLOC2</td> <td>Flag indicating the presence of a second strut</td> </tr> <tr> <td>NLOC2 =</td> <td> <math display="block">\begin{cases} 0 &amp; \text{if single strut} \\ 1 &amp; \text{if tandem struts} \end{cases}</math> </td> </tr> <tr> <td>WTINT</td> <td>Weighting constant for the integrand</td> </tr> <tr> <td>SEPCOS</td> <td>Value of the cosine function in the integrand</td> </tr> <tr> <td>SQ</td> <td>Value of part of the integrand</td> </tr> <tr> <td></td> <td> <math display="block">\frac{1}{(\alpha^2 - \gamma^2)^{\frac{1}{2}}}</math> </td> </tr> </table>	ALFA	Integrating variable $\alpha$	B	CSTRUT(I)/XLS	D	CSTRT2(I)/XLS	NLOC2	Flag indicating the presence of a second strut	NLOC2 =	$\begin{cases} 0 & \text{if single strut} \\ 1 & \text{if tandem struts} \end{cases}$	WTINT	Weighting constant for the integrand	SEPCOS	Value of the cosine function in the integrand	SQ	Value of part of the integrand		$\frac{1}{(\alpha^2 - \gamma^2)^{\frac{1}{2}}}$
ALFA	Integrating variable $\alpha$																		
B	CSTRUT(I)/XLS																		
D	CSTRT2(I)/XLS																		
NLOC2	Flag indicating the presence of a second strut																		
NLOC2 =	$\begin{cases} 0 & \text{if single strut} \\ 1 & \text{if tandem struts} \end{cases}$																		
WTINT	Weighting constant for the integrand																		
SEPCOS	Value of the cosine function in the integrand																		
SQ	Value of part of the integrand																		
	$\frac{1}{(\alpha^2 - \gamma^2)^{\frac{1}{2}}}$																		
COMMON BLOCKS:	AUX, OMEGA																		
SUBROUTINE CALLED:	BESSJ																		
CALLED BY:	RWAVE																		
COMMENTS:																			

NAME: SUBROUTINE RWAVE

PURPOSE: Subroutine RWAVE computes the auxiliary function of T and W.

CALLING SEQUENCE: CALL RWAVE (B, D, NLOC2)

ARGUMENTS:

B	CSTRUT (I)/XLS
D	CSTRT2 (I)/XLS
NLOC2	Flag indicating the presence of a second strut
NLOC2 =	$\begin{cases} 0 & \text{if single strut} \\ 1 & \text{if tandem struts} \end{cases}$

COMMON BLOCKS: OUT, AUX, OMEGA, PSI

SUBROUTINES CALLED: RINIT, SIMPSN, RINTEG, BESSJ, REFLKT

CALLED BY: SWATH

COMMENTS:

#### Typical Auxiliary Functions

$$\left\{ \frac{T_{smn}}{(2m-1)(2n-1)} \right\} = \int_{\gamma_{0s}}^{\infty} \frac{d\alpha}{\alpha^2 \sqrt{\alpha^2 - \gamma_{0s}^2}} D \left( \alpha, \frac{2b}{L_s}, \gamma_{0s} \right) \times E_s^2(\alpha) \left\{ \frac{J_{2m-1}(\alpha) J_{2n-1}(\alpha)}{J_{2m}(\alpha) J_{2n}(\alpha)} \right\},$$

where

$$D = 1 + \cos \left[ \left( \frac{2b}{L_s} \right) \left( \frac{2}{\gamma_{0s}} \right) \alpha \sqrt{\alpha^2 - \gamma_{0s}^2} \right],$$

$$E_s = 1 - e^{-2(m_s/L_s)(\alpha^2/\gamma_{0s})},$$

$$\gamma_{0s} = \frac{gL_s}{(2U^2)}.$$

NAME:	SUBROUTINE RWOUT						
PURPOSE:	Subroutine RWOUT computes and prints drag coefficients and total resistance of the test model.						
CALLING SEQUENCE:	CALL RWOUT (I, NLOC2)						
ARGUMENTS:	<table border="0"> <tr> <td>I</td> <td>Index indicating strut location</td> </tr> <tr> <td>NLOC2</td> <td>Flag indicating the presence of a second strut</td> </tr> <tr> <td>NLOC 2 =</td> <td> <math display="block">\begin{cases} 0 &amp; \text{if single strut} \\ 1 &amp; \text{if tandem struts} \end{cases}</math> </td> </tr> </table>	I	Index indicating strut location	NLOC2	Flag indicating the presence of a second strut	NLOC 2 =	$\begin{cases} 0 & \text{if single strut} \\ 1 & \text{if tandem struts} \end{cases}$
I	Index indicating strut location						
NLOC2	Flag indicating the presence of a second strut						
NLOC 2 =	$\begin{cases} 0 & \text{if single strut} \\ 1 & \text{if tandem struts} \end{cases}$						
COMMON BLOCKS:	OUT, AUX, OMEGA						
SUBROUTINES CALLED:	SUM, FUNCTION FORMDR, FUNCTION CFITTC						
CALLED BY:	SWATH						
COMMENTS:							

NAME:	SUBROUTINE SCALE
PURPOSE:	Subroutine SCALE computes scaling factors and scales the input for length between -1.0 and +1.0 maximum beam and sectional area to 1.0.
CALLING SEQUENCE:	CALL SCALE (ISBODY)
ARGUMENT:	ISBODY    Logical flag indicating, "Is this for body?" ISBODY = { . TRUE . for body . FALSE . for strut
COMMON BLOCKS:	OFFSET, NAME, NORM
SUBROUTINE CALLED:	NONE
CALLED BY:	CHEB
COMMENTS:	

NAME: SUBROUTINE SIMPSN

PURPOSE: Subroutine SIMPSN sets up Simpson's multipliers for numerical integration by Simpson's rule.

CALLING SEQUENCE: CALL SIMPSN (NPTS, SIMP)

ARGUMENTS: NPTS Number of integration steps  
SIMP Array containing Simpson's multipliers

COMMON BLOCKS: NONE

SUBROUTINE CALLED: NONE

CALLED BY: RWAVE

COMMENTS:

NAME:	SUBROUTINE SPLINE	
PURPOSE:	Subroutine SPLINE fits smooth spline segments through a given set of discrete data points.	
CALLING SEQUENCE:	CALL SPLINE (X, Y, D, N, BC, KODE, KCODE, ISBODY)	
ARGUMENTS:	X	Value of abscissas of offset data
	Y	Value of ordinates of offset data
	D	Value of second derivatives at a point
	N	Total number of offset data points
	BC	Value of boundary conditions 0 if user is specifying boundary conditions
	KODE =	{ 1 if user is taking an extrapolation of second derivatives as boundary conditions
	KCODE =	{ 0 if there is no printout from spline routine 1 if spline prints abscissas, ordinates and second derivatives
	ISBODY	Logical flag indicating, "Is this for body?"
	ISBODY =	{ . TRUE . for body . FALSE . for strut
COMMON BLOCKS:	NONE	
SUBROUTINE CALLED:	NONE	
CALLED BY:	CHEV	
COMMENTS:		



NAME: SUBROUTINE SUM

PURPOSE: Subroutine SUM computes sums of the form:

$$\sum_{m=1}^M \sum_{n=1}^N \{A_{sm} A_{sn} T_{smn} + B_{sm} B_{sn} W_{smn}\}$$

CALLING SEQUENCE: CALL SUM (L, SUM1S, SUM1B, SUM1SB, SUM12S, SUM12B, SUM12SB)

ARGUMENTS:

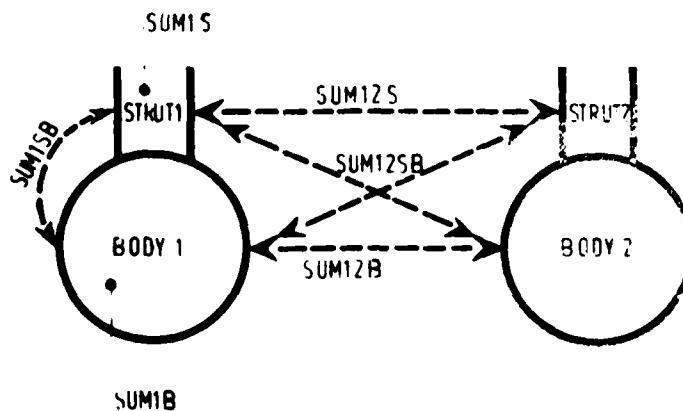
L	Number of different hull separation distances
SUM1S	Partial sum for strut 1
SUM1B	Partial sum for body 1
SUM1SB	Partial sum for interaction between strut 1 and body 1
SUM12S	Partial sum for interaction between strut 1 and strut 2
SUM12B	Partial sum for interaction between body 1 and body 2
SUM12SB	Partial sum for interactions between strut 1 and body 2 or strut 2 and body 1

COMMON BLOCKS: AUX, OMEGA, COEFS

SUBROUTINE CALLED: NONE

CALLED BY: RWOUT

COMMENTS:



NAME: FUNCTION SUMSPL

PURPOSE: Function SUMSPL uses the spline coefficients and integrates the trigonometric integrals  $F(X)*\sin(AK*X)$  or  $F(X)*\cos(AK*X)$ .

CALLING SEQUENCE: SUM = SUMSPL (X, Y, S, N, AK, KODE)

ARGUMENTS:

X	Values of abscissas of offset data
Y	Values of ordinates of offset data
S	Values of second derivatives
N	Total number of data points
AK	$(2m-1)$ or $(2m)$ , $m = 1, 2, 3 \dots MMAX$
KODE =	$\begin{cases} +1 & \text{if sine integration desired} \\ -1 & \text{if cosine integration desired} \end{cases}$

COMMON BLOCKS: NONE

SUBROUTINE CALLED: NONE

CALLED BY: CHEV

NAME:	SUBROUTINE SURFACE
PURPOSE:	Subroutine SURFACE finds the wetted surface area of the strut or body as well as the waterplane area or displaced volume.
CALLING SEQUENCE:	CALL SURFACE (AMC, BMC, MMAX, ISBODY)
ARGUMENTS:	<p>AMC        Coefficients of the Chebychev Cosine Series</p> <p>BMC        Coefficients of the Chebychev Sine Series</p> <p>MMAX       Maximum order of the Chebychev polynomials</p> <p>ISBODY     Logical flag indicating "Is this for body?"</p> <p>ISBODY = { . TRUE . for body           . FALSE . for strut</p>
COMMON BLOCKS:	OUT, NAME
SUBROUTINES CALLED:	WTSURFS, WTSURFB
CALLED BY:	CHEB
COMMENTS:	

NAME: SUBROUTINE WTSURFB

PURPOSE: Subroutine WTSURFB determines the surface area of a body of revolution given by the Chebychev coefficients.

CALLING SEQUENCE: CALL WTSURFB (AMC, BMC, MMAX)

ARGUMENTS: AMC Coefficients of the Chebychev Cosine Series  
BMC Coefficients of the Chebychev Sine Series  
MMAX Maximum order of the Chebychev Series

COMMON BLOCK: OUT

SUBROUTINE CALLED: EVAL

CALLED BY: SURFACE

COMMENTS:

NAME:	SUBROUTINE WTSURFS	
PURPOSE:	Subroutine WTSURFS determines the wetted surface area of a strut whose thickness distribution is given by the Chebychev coefficients.	
CALLING SEQUENCE:	CALL WTSURFS (AMC, BMC, MMAX)	
ARGUMENTS:	AMC	Coefficients of Chebychev Cosine Series
	BMC	Coefficients of Chebychev Sine Series
	MMAX	Maximum order of Chebychev Series
COMMON BLOCK:	OUT	
SUBROUTINE CALLED:	EVAL	
CALLED BY:	SURFACE	
COMMENTS:		

NAME: FUNCTION YINTP

PURPOSE: Function YINTP interpolates through a set of discrete data.

CALLING SEQUENCE: FR = YINTP (XA, X, Y, N)

ARGUMENTS: XA Point to be interpolated  
X Array of ordinate data  
Y Array of abscissa data  
N Number of data points

COMMON BLOCKS: NONE

SUBROUTINE CALLED: NONE

CALLED BY: FORMDR

COMMENTS: Uses linear interpolation

PROGRAM DOCUMENTATION OF SYNTHESIS

COMMON BLOCK DEFINITIONS FOR SYNTHESIS



COMMON/AUX/

PURPOSE: AUX stores the auxiliary wave resistance function table.

NAME	TYPE	LENGTH	DEFINITION
TS	R	(3,3)	Auxiliary function T for strut
WS	R	(3,3)	Auxiliary function W for strut
TB	R	(3,3)	Auxiliary function T for body
WB	R	(3,3)	Auxiliary function W for body
TSB	R	(3,3)	Auxiliary function T for strut to body
WSB	R	(3,3)	Auxiliary function W for strut to body
TS12	R	(3,3)	Auxiliary function T for strut 1 to strut 2
WS12	R	(3,3)	Auxiliary function W for strut 1 to strut 2
TB12	R	(3,3)	Auxiliary function T for body 1 to body 2
WB12	R	(3,3)	Auxiliary function W for body 1 to body 2
TSB12	R	(3,3)	Auxiliary function T for strut 1 to body 2
WSB12	R	(3,3)	Auxiliary function W for strut 1 to body 2
TSBP	R	(3,3)	Auxiliary function T
WSBP	R	(3,3)	Auxiliary function W
TSB12P	R	(3,3)	Auxiliary function T
WSB12P	R	(3,3)	Auxiliary function W

COMMON/BARCK/IE /

PURPOSE: BARCK stores the variables which define the propulsor design condition.

NAME	TYPE	LENGTH	DEFINITION
IE	I		Error message pointer

IE = {

- 0,if program ran in normal fashion
- 100,if limiting value of P/D has been used
- 200,if there is an iteration malfunction -- PD(2)  
used for P/D
- 3,if maximum BAR, 0.95, used -- marine screw
- 4,if minimum BAR, .4, used -- marine screw
- 5,if maximum tip speed used -- air screw
- 6,if blade number is outside program limit --  
closest number used

**COMMON/CDESC/**

**PURPOSE:** CDESC stores the values of constants which define water properties.

NAME	TYPE	LENGTH	DEFINITION
RHOD	R	(3)	Water density array
ANUD	R	(3)	Kinematic viscosity array
IP	I		Pointer indicating the particular water condition used. Set IP = 1 for this program to obtain sea water condition.

COMMON/COEFS/

PURPOSE: COEFS stores the values of the Chebychev coefficients for the strut and body.

NAME	TYPE	LENGTH	DEFINITION
ASM	R	(3)	Coefficients of Chebychev Sine Series for strut
BSM	R	(3)	Coefficients of Chebychev Cosine Series for strut
ABM	R	(3)	Coefficients of Chebychev Sine Series for body
BBM	R	(3)	Coefficients of Chebychev Cosine Series for body
MMAX	I		Maximum order of Chebychev Series

COMMON/CPROP/

PURPOSE: CPROP stores the values of the variables and constants used in the propulsor design routine.

NAME	TYPE	LENGTH	DEFINITION
IPTYP	I	(3)	Indicating propeller type
DIAM	R	(3)	Diameter of propeller (ft)
VADES	R	(3)	Speed of advance of propulsor at design condition (kts)
RPMDES	R	(3)	RPM of propeller at design point
TDES	R	(3)	Thrust of propulsor system (lbs)
QDES	R	(3)	Torque of propulsor system (ft-lbs)
EFFDES	R	(3)	Efficiency of propulsor at design condition
OMWTD	R	(3)	Thrust wake $(1-w_T)$
CAV	R	(3)	Percent back cavitation allowed on water screw
Z	I	(3)	Number of blades of propeller
H	R	(3)	Depth of water to centerline of propulsor shaft
BAR	R	(3)	Blade area ratio
PD	R	(3)	P/D of propulsor
J	R	(3)	J of propulsor
IERROR	I	(3)	Error message indicator
KT	R	(3)	Thrust coefficient ( $K_T$ )
KQ	R	(3)	Torque coefficient ( $K_Q$ )

## COMMON/INPUT/

PURPOSE: INPUT stores input data.

NAME	TYPE	LENGTH	DEFINITION
XLS	R		Length of strut $L_S$ (ft)
HS	R		Draft of strut $H_S$ (ft)
TSMAX	R		Maximum thickness of strut $t_{max}$ (ft)
CWP	R		Waterplane area coefficient $C_{WP} = A_W / (L_S t_{max})$ where $A_W$ = waterplane area of one strut
CLCF	R		Waterplane moment coefficient $C_{LCF} = M_{x_S} / (A_W \cdot L_S)$ *
CIYY	R		Waterplane inertia coefficient $C_{IYY} = I_{wp} / (A_W \cdot L_S^2)$ *
XLB	R		Length of body $L_B$ (ft)
HB	R		Draft of body $H_B$ (ft)
AX	R		Maximum cross-sectional area of body $A_X$ (ft <sup>2</sup> )
CP	R		Body prismatic coefficient $C_P = \nabla_b / (A_X L_b)$ where $\nabla_b$ = displaced volume of one body
CLCB	R		Body moment coefficient $C_{LCB} = M_{x_B} / (\nabla_e \cdot L_e)$ *
SEPDIS	R		Separation distance between centerline of the two bodies (ft)
CSTRUT	R		Distance from centerline of strut to centerline of body (ft)
CSTR2	R		Distance from centerline of second strut to centerline of body (ft)
PDIA	R		Diameter of propeller $D$ (ft)
SPAN	R		Span of a demi-fin (ft)
CHORD	R		Chord of a fin (ft)
TFINS	R		Maximum thickness of a demi-fin (ft)
NLOC	I		Switch indicating the presence of a second strut

\*All moments and moments of inertia are taken about the mid-length of the respective strut or body.

COMMON/OFFDES/

PURPOSE: OFFDES stores the variables which define the coefficients of KT/KQ curves.

NAME	TYPE	LENGTH	DEFINITION
PJAY	R	(4)	Coefficients of polynomial representing KT or KQ.

COMMON/OMEGA/

PURPOSE: OMEGA stores the values of variables and constants for evaluation of auxiliary functions and ship resistance coefficients.

NAME	TYPE	LENGTH	DEFINITION
VMFPS	R		Speed of ship $V_K$ (kts)
GAMAOS	R		$\gamma_{os} = \frac{1}{2} g L_s / V^2$ where U is speed in fps
GAMAOB	R		$\gamma_{ob} = \frac{1}{2} g L_b / V^2$
GOSQ	R		$(\gamma_{os})^2$
HSOLS	R		Ratio of draft to length of strut $H_s / L_s$
HBOLB	R		Ratio of draft to length of body $H_b / L_b$
WETS	R		Wetted surface area of strut $S_s$ (ft <sup>2</sup> )
WETB	R		Wetted surface area of body $S_b$ (ft <sup>2</sup> )
WETFIN	R		Wetted surface area of a fin $S_f$ (ft <sup>2</sup> )
WTSURF	R		Total wetted surface area
SEP	R		$2b / (\gamma_{os} \cdot L_s)$
PHIS	R		$2 \left( \frac{H_s}{L_s} \right) / \gamma_{os}$
PHIB	R		$2 \left( \frac{H_b}{L_b} \right) / \gamma_{ob}$
RATIOI	R		$\gamma_{ob} / \gamma_{os}$
CFS	R		Frictional drag coefficient of strut $C_{F_s}$
CFB	R		Frictional drag coefficient of body $C_{F_b}$
APPDRG	R		Appendage drag (lb)



COMMON/PCOF /

PURPOSE: PCOF stores coefficients for KQ/KT polynomial approximation.

NAME	TYPE	LENGTH	DEFINITION
CT	R	(4)	Coefficients of the polynomial which is an approximation of the KT curve
CQ	R	(4)	Coefficients of the polynomial which is an approximation of the KQ curve

COMMON/PHYSICO/

PURPOSE: PHYSICO stores physical constants.

NAME	TYPE	LENGTH	DEFINITION
RHO	R		Density of water
GNU	R		Kinematic viscosity of water
G	R		Acceleration due to gravity
PI	R		Ratio of circumference to diameter of a circle
DELCF	R		Correction allowance of friction drag from ITTC line.

COMMON/PLOT/

PURPOSE: PLOT stores the constants and characters for the plotting routine.

NAME	TYPE	LENGTH	DEFINITION
NFIRST	I		Position in the arrays of the first ordered pair to be plotted
NLAST	I		Position in the arrays of the last ordered pair to be plotted
NPOINT	I		NPOINT equals "1" if each point from NFIRST to NLAST is to be plotted, "2" if every other point is to be plotted, etc.
XMAX	R		Value of abscissa at right-most grid line
XMIN	R		Value of abscissa at left-most grid line
NSCLI	L		Logical value (Should be false if PLOT1 has not been called and standard grid is desired)
NCHAR	I		Number of valid characters in label
NSCALE	I	(4)	Printing scale factor of ordinate
PCHAR	I	(2)	Plotting characters

COMMON/PSI/

PURPOSE: PSI stores the values of the variables and constants used in integration routines.

NAME	TYPE	LENGTH	DEFINITION
NPTSZ	I		Number of integration steps from $\gamma$ to $\gamma+1$
PTSAF	R		Scaling factor of step size in integrating from $\alpha_{\max}$ to $\alpha_{\ell\max}$
EXPN	R		Empirical constant for integration to stop
NALMAX	R		Maximum number of integration steps from $\gamma+1$ to $\alpha_{\max}$
NAL	I		Counter of integration steps
TAIL	R		Integration correction made from $\alpha_{\max}$ to $\alpha_{\ell\max}$
ALFA	R		Integrating variable ( $\alpha$ )
ALSMAX	R		Maximum of $\alpha$ for integration
NSTEPS	I		Number of integration steps from $\alpha_{\max}$ to $\alpha_{\ell\max}$

COMMON/ROOTC/

PURPOSE: ROOTC stores the coefficients of a third order polynomial  
which is the approximation of the KT curve of a propeller.

NAME	TYPE	LENGTH	DEFINITION
A	R	4	Array holding the coefficient of a third order polynomial which is the approximation of the KT curve of a propeller

COMMON/XRPLOTF/

PURPOSE: XRPLOTF stores the values of variables for the plotting routine.

NAME	TYPE	LENGTH	DEFINITION
XL	R		Value of abscissa at left-most grid line
XH	R		Value of abscissa at right-most grid line
YL	R		Value of ordinate at bottom grid line
YH	R		Value of ordinate at top grid line
XMOV	R		Abcissa index increment number for array GRAF
YMOV	R		Ordinate index increment number for array GRAF

COMMON/XRPLLOTG/

PURPOSE: XRPLLOTG stores the values and characters of variables for the plotting routine.

NAME	TYPE	LENGTH	DEFINITION
GRAF	I	(11,204)	Array containing the image to be plotted

# COMMON/XRPLQTQ

PURPOSE: XRPLQTQ stores the constants and characters for the plotting routine.

NAME	TYPE	LENGTH	DEFINITION
I	I		Ordinate scale factor is $10^I$
J	I		Number digits following ordinate decimal point
K	I		Abcissa scale factor is $10^K$
L	I		Number digits following abscissa decimal point
NHL	I		Number of horizontal grid lines
NSBH	I		Number of spaces between adjacent horizontal grid lines
NVL	I		Number of vertical grid lines
NSBV	I		Number of spaces between adjacent vertical grid lines
HCHAR	I		Plotting character of horizontal grid lines
ISX	I		Number of horizontal spaces
ISY	I		Number of vertical spaces
V	L		Logical variable, = . TRUE . when the maximum and minimum values of the ordinate are determined
H	L		Logical variable, = . TRUE . when the maximum and minimum values of the abscissa are determined



SUBROUTINE DOCUMENTATION FOR SYNTHESIS

NAME: PROGRAM SYNTH

PURPOSE: Program SYNTH is the main program for calculating the propulsor resistance and design for SWATH ships.

CALLING SEQUENCE: PROGRAM SYNTH (INPUT, OUTPUT, TAPE 5 = INPUT, TAPE 6 = OUTPUT, TAPE 8)

ARGUMENTS: NONE

COMMON BLOCKS: COEFS, INPUT, OMEGA, PHYSCO, PSI

SUBROUTINES CALLED: RIN, CHEB, RWAVE, FINDRG, ROUT, SHPCMP, Function CFITTC

COMMENTS:

NAME:	SUBROUTINE BESSJ
PURPOSE:	Subroutine BESSJ evaluates the Bessel function from order 0 to order N.
CALLING SEQUENCE:	CALL BESSJ (X, N, VJ)
ARGUMENTS:	<p>X    Argument of the Bessel function</p> <p>N    Maximum order of the Bessel function</p> <p>VJ   Array holding (N+1) values of the Bessel function of order zero up to N, where</p> <p style="margin-left: 100px;"><math>VJ(0) = J_0(X)</math></p> <p style="margin-left: 100px;">.</p> <p style="margin-left: 100px;">.</p> <p style="margin-left: 100px;">.</p> <p style="margin-left: 100px;"><math>VJ(N) = J_N(X)</math></p>
COMMON BLOCKS:	NONE
SUBROUTINE CALLED:	NONE
CALLED BY:	RINTEG, RWAVE
COMMENTS:	

NAME: SUBROUTINE BURIL

PURPOSE: SUBROUTINE BURIL uses Burrill's cavitation criteria to determine if the blade area ratio (BAR) used is sufficient and, if it is not, to estimate what BAR is necessary.

CALLING SEQUENCE: CALL BURIL (T, D, H, VA, N, CAVI, BAR, IERROR, PD, NRET)

ARGUMENTS:

T	Thrust of propeller (lbs)
D	Diameter of propeller (ft)
H	Depth of propeller shaft (ft)
VA	Speed of advance (fps)
N	RPM of propeller
CAVI	Percent back cavitation allowed
BAR	Blade area ratio
IERROR	Error message indication as defined in Common Block BARCK
PD	P/D of propeller
NRET	Internal flag indicating BAR optimization

NRET =  $\begin{cases} 0 & \text{if not optimized} \\ 1 & \text{if optimized} \end{cases}$

COMMON BLOCK: BARCK

SUBROUTINE CALLED: NONE

CALLED BY: PRODES

COMMENTS:

NAME:	FUNCTION CALC										
PURPOSE:	FUNCTION CALC calculates "KT" or "KQ" for two to seven-bladed propellers, given J, BAR, P/D, Z, and an indicator for "KT" or "KQ."										
CALLING SEQUENCE:	TQ = CALC (J, BAR, PD, Z, ITQ)										
ARGUMENTS:	<table border="0"> <tr> <td>J</td> <td>Advance coefficient of propeller</td> </tr> <tr> <td>BAR</td> <td>Blade area ratio</td> </tr> <tr> <td>PD</td> <td>P/D of propeller</td> </tr> <tr> <td>Z</td> <td>Number of blades</td> </tr> <tr> <td>ITQ</td> <td>Index defined by</td> </tr> </table> $ITQ = \begin{cases} 1 & \text{if thrust is input} \\ 2 & \text{if power is input} \end{cases}$	J	Advance coefficient of propeller	BAR	Blade area ratio	PD	P/D of propeller	Z	Number of blades	ITQ	Index defined by
J	Advance coefficient of propeller										
BAR	Blade area ratio										
PD	P/D of propeller										
Z	Number of blades										
ITQ	Index defined by										
COMMON BLOCK:	OFFDES										
SUBROUTINE CALLED:	NONE										
CALLED BY:	TROOST, ROOT, POLCOF										
COMMENTS:											

NAME: FUNCTION CFITTC

PURPOSE: Function CFITTC determines the ITTC frictional resistance coefficient  $C_F$

CALLING SEQUENCE: CF = CFITTC (RN)

ARGUMENT: RN Reynolds number at  $R_n$  at test conditions

COMMON BLOCKS: NONE

SUBROUTINE CALLED: NONE

CALLED BY: SYNTH

COMMENTS:

$$C_F = \frac{0.075}{[\log_{10}(R_n) - 2]^2}$$

NAME: SUBROUTINE CHEB

PURPOSE: Subroutine CHEB determines the Chebychev coefficients and wetted surface area of the strut and body. It also plots the strut waterline and the body area distribution.

CALLING SEQUENCE: CALL CHEB (TITLE)

ARGUMENT: TITLE Array containing the alphanumeric characters of the title of the experiment

COMMON BLOCKS: COEFS, INPUT, OMEGA, PHYSCO

SUBROUTINES CALLED: WSURFB, WSURFS, PCHEB

CALLED BY: SYNTH

COMMENTS:

NAME:	SUBROUTINE ERROR
PURPOSE:	Subroutine ERROR prints the error message of the propulsor design.
CALLING SEQUENCE:	CALL ERROR (IE)
ARGUMENT:	IE     Error message pointer as defined in Common Block BARCK
COMMON BLOCKS:	NONE
SUBROUTINE CALLED:	NONE
CALLED BY:	PROPP
COMMENTS:	



NAME: FUNCTION EVAL

PURPOSE: Function EVAL evaluates the Chebychev Series:  

$$F(X) = \sum_{M=1}^{MMAX} A(M) * U(M,X) + B(M) * V(M,X)$$

CALLING SEQUENCE: EV = EVAL (X,A,B,MMAX)

ARGUMENTS:

X	Arguments of the Chebychev Series
A	Coefficients of the Chebychev Cosine Series
B	Coefficients of the Chebychev Sine Series
MMAX	Maximum order of the Chebychev Series

COMMON BLOCKS: NONE

SUBROUTINE CALLED: NONE

CALLED BY: WSURFS, WSURFB

COMMON BLOCKS: NONE

SUBROUTINE CALLED: NONE

CALLED BY: WSURFS, WSURFB

COMMENTS:

$$U_M(X) = \cos[(2M-1)(\theta)]$$

$$V_M(X) = \sin 2M \theta$$

$$\theta = \sin^{-1}(X)$$

NAME: SUBROUTINE FINDRG

PURPOSE: Subroutine FINDRG determines the fin drag.

CALLING SEQUENCE: CALL FINDRG (RHOS, XNUS, VSFW, SFINS, TFINS, CFINS, TBFINS, SBFINS, DS)

ARGUMENTS:

RHOS	Density of water
XNUS	Kinematic viscosity of water
VSFW	Ship speed (fps)
SFINS	Chord * span
TFINS	Thickness of a fin (ft)
CFINS	Chord of a fin (ft)
TBFINS	$0.01 * TFINS$
SBFINS	$TBFINS * span$
DS	Total fin drag

COMMON BLOCKS: NONE

SUBROUTINES CALLED: FRICT, FOILSC

CALLED BY: SYNTH

COMMENTS:

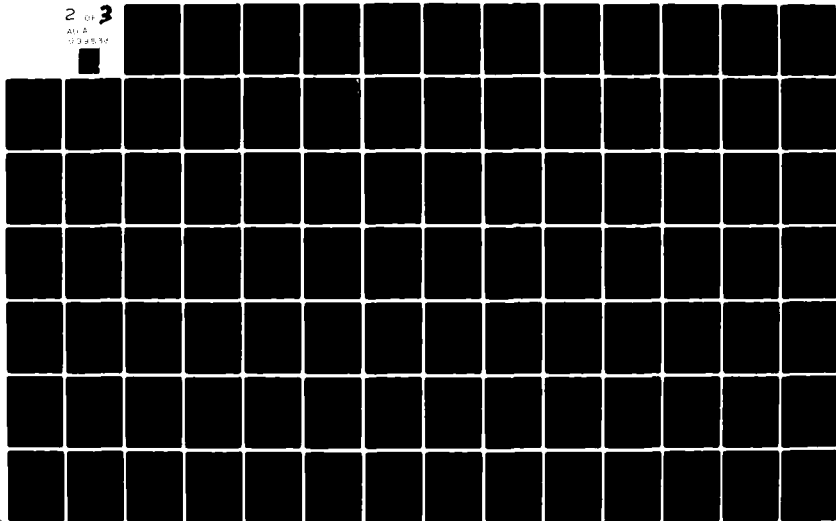
AD-A099 533

DAVID W TAYLOR NAVAL SHIP RESEARCH AND DEVELOPMENT CE--ETC F/G 20/4  
DOCUMENTATION FOR SWATH SHIP RESISTANCE AND PROPULSION PREDICTI--ETC(U)  
APR 81 A M REED  
DTNSRDC/SPD-0927-02

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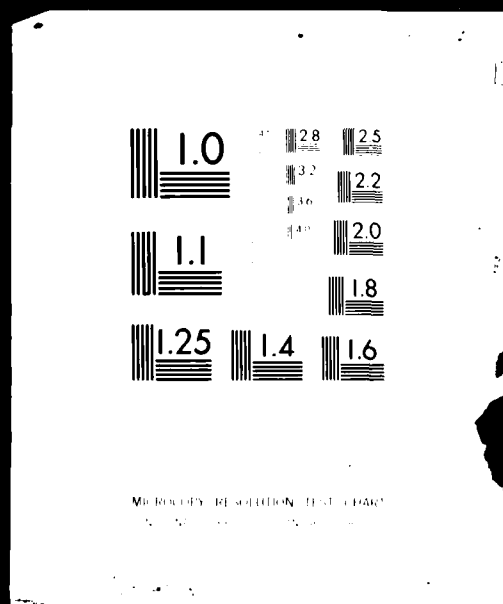
2 OF 3  
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NAME: SUBROUTINE FOILSC

PURPOSE: Subroutine FOILSC calculates the drag components for a symmetrical foil section.

CALLING SEQUENCE: CALL FOILSC (XS, CFS, TOC, TOC2, TOC4, SS, TS2, SBS, CLOTB, RFS, RFVAS, RPS, RINTS, RBS)

ARGUMENTS:

XS	Ship constant = $\frac{1}{2} * \rho * SFINS$ VSFW ** 2
CFS	Flat plate friction coefficient
TOC	Thickness/chord ratio
TOC2	T/C**2
TOC4	T/C**4
SS	Chord * span $\approx$ area of foil
TS2	(SS) ** 2 $\approx$ area squared
SBS	TBFINS * span
CLOTB	Chord/0.01 * TFINS
RFS	Frictional resistance of a flat plate
RFUAS	Resistance due to velocity argumentation
RPS	Resistance due to pressure and separation
RINTS	Resistance due to intersection with hull
RBS	Base drag due to bluntness of trailing edge

COMMON BLOCKS: NONE

SUBROUTINE CALLED: NONE

CALLED BY: FINDRG

COMMENTS:

NAME: FUNCTION FORMDR

PURPOSE: Function FORMDR evaluates the form drag coefficient.

CALLING SEQUENCE: FDR = FORMDR (VL)

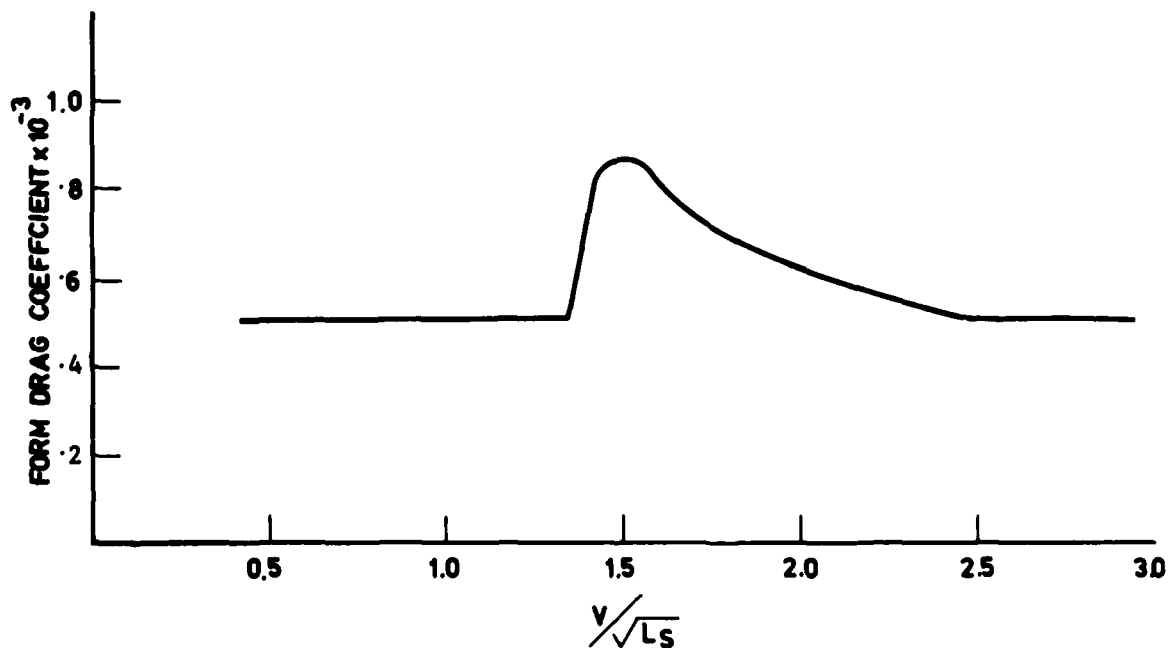
ARGUMENT: VL Ratio of ship speed to square root of length of strut  $V/\sqrt{L_S}$

COMMON BLOCKS: NONE

SUBROUTINE CALLED: FUNCTION YINTP

CALLED BY: RWOUT

COMMENTS:



NAME:	SUBROUTINE FRICT	
PURPOSE:	Subroutine FRICT calculates the flat plate friction coefficient based on the local Reynolds number.	
CALLING SEQUENCE:	CALL FRICT (CF, VF, XLEN, XNU)	
ARGUMENTS:	CF	Flat plate friction coefficient
	VF	Speed of ship (fps)
	XLEN	Chord of fin (ft)
	XNU	Kinematic viscosity
COMMON BLOCKS:	NONE	
SUBROUTINE CALLED:	NONE	
CALLED BY:	FINDRG	
COMMENTS:		

NAME: SUBROUTINE PCHEB

PURPOSE: Subroutine PCHEB plots by line printer the body sectional area curve and waterplane outline curve from the given Chebychev coefficients.

CALLING SEQUENCE: CALL PCHEB (AS, BS, AB, BB, NN, TITLE)

ARGUMENTS:

AS	Coefficients of Chebychev Sine Series for strut
BS	Coefficients of Chebychev Cosine Series for strut
AB	Coefficients of Chebychev Sine Series for body
BB	Coefficients of Chebychev Cosine Series for body
NN	Maximum order of Chebychev Series
TITLE	Array containing the alphanumeric characters of the title of the experiment

COMMON BLOCKS: PLOT, XRPLQTQ

SUBROUTINES CALLED: PLOT1, PLOT2, PLOT3, PLOT4

CALLED BY: CHEB

COMMENTS:



NAME: SUBROUTINE PLOT1

PURPOSE: Subroutine PLOT1 sets up spacing and determines the values of the axes.

CALLING SEQUENCE: CALL PLOT 1 (NSCALE, A, B, C, D, E, F)

ARGUMENTS:

NSCALE	Integer array defined as follows:
NSCALE (1)	= I, if printed values of the ordinate are $10^{**} I$ times the actual value
NSCALE (2)	= J, if printed values of the ordinate are $10^{**} J$ times the actual value
NSCALE (3)	= K, if printed values of the abscissa are $10^{**} K$ times the actual values
NSCALE (4)	= L, if printed values of the abscissa are $10^{**} L$ times the actual value
A	Integer number of horizontal grid lines
B	Integer number of spaces beyond each horizontal grid line to the next grid line
C	Integer number of vertical grid lines
D	Integer number of spaces beyond each vertical grid line to the next grid line
E	Horizontal grid character
F	Vertical grid character

COMMON BLOCK: XRPLQTQ

SUBROUTINE CALLED: NONE

CALLED BY: PCHEB

COMMENTS:

NAME: SUBROUTINE PLOT2

PURPOSE: Subroutine PLOT2 examines the minimum and maximum values of the abscissa and the ordinate and establishes an internal formula for computing location in the image region corresponding to the point to be plotted.

CALLING SEQUENCE: CALL PLOT2 (XMAX, XMIN, YMAX, YMIN, NSCLI)

ARGUMENTS:

XMAX	Value of abscissa at right-most grid line
XMIN	Value of abscissa at left-most grid line
YMAX	Value of ordinate at top grid line
YMIN	Value of ordinate at bottom grid line
NSCLI	Logical flag (should be false, if PLOT1 has not been called and standard grid is desired)

COMMON BLOCKS: XRPLTF, XRPLQT, XRPLTG

SUBROUTINE CALLED: NONE

CALLED BY: PCHEB

COMMENTS:

NAME:	SUBROUTINE PLOT3												
PURPOSE:	Subroutine PLOT3 assigns an alpha-character to each point to be plotted.												
CALLING SEQUENCE:	CALL PLOT3 (PCHAR, X, Y, SDATA, FDATA, DDATA)												
ARGUMENTS:	<table border="0"> <tr> <td>PCHAR</td> <td>Plotting character</td> </tr> <tr> <td>X</td> <td>Array containing the X coordinates to be plotted</td> </tr> <tr> <td>Y</td> <td>Array containing the Y coordinates to be plotted</td> </tr> <tr> <td>SDATA</td> <td>Integer position in the arrays of the first ordered pair to be plotted</td> </tr> <tr> <td>FDATA</td> <td> <div style="display: inline-block; vertical-align: middle;"> <div style="font-size: 2em; vertical-align: middle;">{</div> <div style="display: inline-block; vertical-align: middle;"> 1 if each point from SDATA to DDATA is to be plotted  2 if every other point is to be plotted  3 if every third point is to be plotted </div> </div> </td> </tr> <tr> <td>DDATA</td> <td>Integer position in the array of the last ordered pair to be plotted</td> </tr> </table>	PCHAR	Plotting character	X	Array containing the X coordinates to be plotted	Y	Array containing the Y coordinates to be plotted	SDATA	Integer position in the arrays of the first ordered pair to be plotted	FDATA	<div style="display: inline-block; vertical-align: middle;"> <div style="font-size: 2em; vertical-align: middle;">{</div> <div style="display: inline-block; vertical-align: middle;"> 1 if each point from SDATA to DDATA is to be plotted  2 if every other point is to be plotted  3 if every third point is to be plotted </div> </div>	DDATA	Integer position in the array of the last ordered pair to be plotted
PCHAR	Plotting character												
X	Array containing the X coordinates to be plotted												
Y	Array containing the Y coordinates to be plotted												
SDATA	Integer position in the arrays of the first ordered pair to be plotted												
FDATA	<div style="display: inline-block; vertical-align: middle;"> <div style="font-size: 2em; vertical-align: middle;">{</div> <div style="display: inline-block; vertical-align: middle;"> 1 if each point from SDATA to DDATA is to be plotted  2 if every other point is to be plotted  3 if every third point is to be plotted </div> </div>												
DDATA	Integer position in the array of the last ordered pair to be plotted												
COMMON BLOCKS:	XRPLTF, XRPLTG												
SUBROUTINE CALLED:	NONE												
CALLED BY:	PCHEB												
COMMENTS:													

NAME: SUBROUTINE PLOT4

PURPOSE: Subroutine PLOT4 prints the image of the completed graph on the printer, including the values of the abscissa and the ordinate at the grid lines outside the bottom and left edge of the graph.

CALLING SEQUENCE: CALL PLOT4 (MCHAR, NCHAR)

ARGUMENTS: MCHAR Single dimension array containing alpha characters to be plotted at the left of the graph  
NCHAR Number of valid characters in MCHAR

COMMON BLOCKS: XRPLTF, XRPLTG, XRPLTQ

SUBROUTINE CALLED: QPLOTZ5

CALLED BY: PCHEB

COMMENTS:

NAME: SUBROUTINE POLCOF

PURPOSE: Subroutine POLCOF determines the coefficients of the polynomials which approximate the KT and KQ curves.

CALLING SEQUENCE: CALL POLCOF ( PD, BAR, Z)

ARGUMENTS: PD P/D of propeller  
BAR Blade area ratio  
Z Number of blades

COMMON BLOCKS: OFFDES, PCOF

SUBROUTINE CALLED: Function CALC

CALLED BY: PROPER

COMMENTS:

NAME: SUBROUTINE PRODES

PURPOSE: Subroutine PRODES is used in the design of a propulsion system to determine characteristics and performance at the design condition.

CALLING SEQUENCE: CALL PRODES (IS)

ARGUMENT: IS Type of propulsor (in this program set equal to 1 to indicate conventional fixed blade propellers)

COMMON BLOCKS: BARCK, CDESC, CPROP

SUBROUTINES CALLED: TROOST, BURIL

CALLED BY: SHPCMP

COMMENTS:

NAME: SUBROUTINE PROPER

PURPOSE: Subroutine PROPER calculates the open water curves' table and off-design performance of propulsor system "IS."

CALLING SEQUENCE: CALL PROPER (IS, VOF, TOF, PWR, TITLE)

ARGUMENTS:

IS	Type of propulsor system (in this program, set to 1 to indicate conventional fixed blade propellers)
VOF	Off design speed (ft)
TOF	Off design thrust (lbs)
PWR	SHP at off design condition
TITLE	Array containing the alphanumeric characters of the title of the experiment

COMMON BLOCKS: CDESC, CPROPR, PCOF, ROOTC

SUBROUTINES CALLED: POLCOF, ROOTP

CALLED BY: SHPCMP

COMMENTS:

NAME:	SUBROUTINE PROPP
PURPOSE:	Subroutine PROPP prints all data in common block "CPROP"
CALLING SEQUENCE:	CALL PROPP (IS, TITLE)
ARGUMENTS:	<div>IS       Type of propulsor system (in this           program, set to 1 to indicate           conventional fixed blade propellers)</div> <div>TITLE    Array containing the alphanumeric           characters of the title of the           experiment</div>
COMMON BLOCK:	CPROP
SUBROUTINE CALLED:	ERROR
CALLED BY:	SHPCMP
COMMENTS:	



NAME: SUBROUTINE QPLOTZ5

PURPOSE: Subroutine QPLOTZ5 calculates the scaling information needed to generate the format to label the left-hand side of the program.

CALLING SEQUENCE: CALL QPLOTZ5 (PDQ)

ARGUMENT: PDQ      Scaling factor for ordinate plot

COMMON BLOCKS: XRPLOTF, XRPLOTQ

SUBROUTINES CALLED: NONE

COMMENTS:

NAME: SUBROUTINE REFLKT

PURPOSE: Subroutine REFLKT reflects the symmetrical  
matrices to T and W.

CALLING SEQUENCE: CALL REFLKT

ARGUMENTS: NONE

COMMON BLOCKS: AUX, COEFS

SUBROUTINE CALLED: NONE

CALLED BY: RWAVE

COMMENTS:

NAME:	SUBROUTINE RIN
PURPOSE:	Subroutine RIN reads input data for the program.
CALLING SEQUENCE:	CALL RIN (TITLE)
ARGUMENT:	TITLE     Array containing the alphanumeric characters of the title of the experiment
COMMON BLOCK:	INPUT
SUBROUTINE CALLED:	NONE
CALLED BY:	SYNTH
COMMENTS:	

NAME:	SUBROUTINE RINIT
PURPOSE:	Subroutine RINIT initializes the T and W arrays.
CALLING SEQUENCE:	CALL RINIT
ARGUMENTS:	NONE
COMMON BLOCKS:	AUX, COEFS
SUBROUTINE CALLED:	NONE
CALLED BY:	RWAVE
COMMENTS:	

NAME: SUBROUTINE RINTEG

PURPOSE: Subroutine RINTEG provides numerical integration for the auxiliary function of T and W.

CALLING SEQUENCE: CALL RINTEG (ALFA, B, D, NLOC2, WTINT, SEPCOS, SQ)

ARGUMENTS:

ALFA	Integrating variable ( $\alpha$ )
B	Ratio of distance between centerlines of strut and body to the length of strut
D	Ratio of distance between centerlines of second strut and body to the length of strut
NLOC2 =	$\begin{cases} 0 & \text{if single strut} \\ 1 & \text{if tandem struts} \end{cases}$
WTINT	Weighting constant for numerical integration
SEPCOS	Value of the Cosine function in the integrand
SQ	Value of $\frac{1}{(\gamma^2 - \gamma'^2)^{1/2}}$ in the integrand

COMMON BLOCKS: AUX, COEFS, INPUT, OMEGA

SUBROUTINE CALLED: BESSJ

CALLED BY: RWAVE

COMMENTS:

NAME: SUBROUTINE ROOT

PURPOSE: Subroutine ROOT uses the Regula Falsi method to find the intersection of the "K" curve and the "K/J\*\*2" curve.

CALLING SEQUENCE: CALL ROOT (PD, Z, BAR, COEFF, IPJ, ITQ, KT, KQ, EFFIN, J2)

ARGUMENTS:

PD	P/D of propeller
Z	Number of blades
BAR	Blade area ratio
COEFF	Optimization coefficients as defined in TROOST
IPJ	Optimization index defined by:
	1, no optimization
	2, optimize N with $KT/J^{**2}$
IPJ =	3, optimize N with $KQ/J^{**3}$
	4, optimize D with $KT/J^{**4}$
	5, optimize D with $KQ/J^{**5}$
ITQ	Index indicating the following:
	1, if thrust is input
ITQ =	2, if power is input
KT	Thrust coefficient
KQ	Torque coefficient
EFFIN	Open water efficiency
J2	Advance coefficient

COMMON BLOCK: ROOTC

SUBROUTINE CALLED: FUNCTION CALC

CALLED BY: TROOST

COMMENTS:

NAME: SUBROUTINE ROUT

PURPOSE: Subroutine ROUT outputs the computed results for all components of drag coefficients and effective horsepower.

CALLING SEQUENCE: CALL ROUT (TITLE, EHP)

ARGUMENTS: TITLE Array containing the alphanumeric characters of the title of the experiment  
EHP Effective horsepower of the ship

COMMON BLOCKS: INPUT, OMEGA, PHYSCO

SUBROUTINES CALLED: SUM, Function FORMDR

CALLED BY: SYNTH

COMMENTS:

NAME: SUBROUTINE RWAVE

PURPOSE: Subroutine RWAVE evaluates the auxiliary functions of T and W.

CALLING SEQUENCE: CALL RWAVE (B, D, NLOC2)

ARGUMENTS:

B Ratio of distance between center-lines of strut and body to the length of strut

D Ratio of distance between center-lines of second strut and body to the length of strut

NLOC2 Switch indicating the presence of a second strut

NLOC2 =  $\begin{cases} 0 & \text{if single strut} \\ 1 & \text{if tandem struts} \end{cases}$

COMMON BLOCKS: AUX, COEFS, INPUT, OMEGA, PHYSCO, PSI

SUBROUTINES CALLED: RINIT, SIMPSN, RINTEG, BESSJ, REFLKT

CALLED BY: SWATH

COMMENTS:

#### Typical Auxiliary Functions

$$\left\{ \begin{array}{l} \frac{T_{smn}}{(2m-1)(2n-1)} \\ \frac{W_{smn}}{(2m)(2n)} \end{array} \right\} = \int_{\gamma_{0s}}^{\infty} \frac{d\alpha}{\alpha^2 \sqrt{\alpha^2 - \gamma_{0s}^2}} D \left( \alpha, \frac{2b}{L_s}, \gamma_{0s} \right) \times E_s^2(\alpha) \left\{ \begin{array}{l} J_{2m-1}(\alpha) J_{2n-1}(\alpha) \\ J_{2m}(\alpha) J_{2n}(\alpha) \end{array} \right\},$$

where

$$D = 1 + \cos \left[ \left( \frac{2b}{L_s} \right) \left( \frac{2}{\gamma_{0s}} \right) \alpha \sqrt{\alpha^2 - \gamma_{0s}^2} \right],$$

$$E_s = 1 - e^{-2(n_s/L_s)(\alpha^2/\gamma_{0s})},$$

$$\gamma_{0s} = \frac{gL_s}{(2U^2)}.$$



NAME: SUBROUTINE SHPCMP

PURPOSE: Subroutine SHPCMP determines a propeller's design and off-design performance and uses this to determine shaft horsepower.

CALLING SEQUENCE: CALL SHPCMP (VDES, EHPDES, PDIA, BDIA, HB, VOFF, EHP, SHP, NV, TITLE)

ARGUMENTS:

VDES	Ship speed at design point (fps)
EHPDES	Effective horsepower at design point
PDIA	Diameter of propeller (ft)
BDIA	Diameter of hull body (ft)
HB	Draft of body (ft)
VOFF	Off-design speed of ship (fps)
EHP	Effective horsepower at off design speeds
SHP	Shaft horsepower at off design speeds
NV	Number of test speeds
TITLE	Array containing the alphanumeric characters of the title of the experiment

COMMON BLOCKS: CDESC, CPROP

SUBROUTINES CALLED: PRODES, PROPP, PROPER, PROPERO

CALLED BY: SYNTH

COMMENTS:

NAME: SUBROUTINE SIMPSN

PURPOSE: Subroutine SIMPSN sets up Simpson's multiplier table for numerical integration using Simpson's rule.

CALLING SEQUENCE: CALL SIMPSN (NPTS, SIMP)

ARGUMENTS: NPTS Number of integration steps (odd and greater than one)  
SIMP Array containing Simpson's coefficients

COMMON BLOCKS: NONE

SUBROUTINE CALLED: NONE

CALLED BY: RWAVE

COMMENTS:

NAME: SUBROUTINE SUM

PURPOSE: Subroutine SUM computes the matrix products as follows:

$$\text{SUM} = \sum_{m=1}^n \sum_{n=1}^m \{A_{sm} A_{sn} T_{smn} + B_{sm} B_{sn} W_{smn}\}$$

CALLING SEQUENCE: CALL SUM (SUM1S, SUM1B, SUM1SB, SUM12S, SUM12B, SUM12SB)

ARGUMENTS:

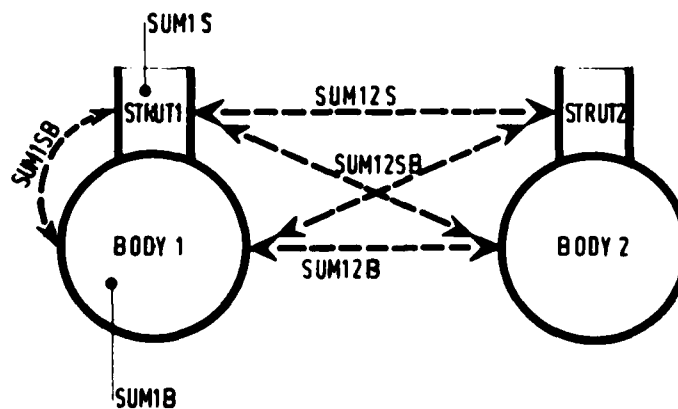
SUM1S	Partial sum for strut 1
SUM1B	Partial sum for body 1
SUM1SB	Partial sum for interaction between strut 1 and body 1
SUM12S	Partial sum for interaction between strut 1 and strut 2
SUM12B	Partial sum for interaction between body 1 and body 2
SUM12SB	Partial sum for interactions between body 1 and strut 2 or body 2 and strut 1

COMMON BLOCKS: AUX, COEFS

SUBROUTINE CALLED: NONE

CALLED BY: ROUT

COMMENTS:



NAME: SUBROUTINE TROOST

PURPOSE: Subroutine TROOST is used with Subroutine ROOT and Function CALC. Either rpm or diameter can be optimized given the other.

CALLING SEQUENCE: CALL TROOST (VAL, P, T, N1, D, Z, PDNEW, BAR, KT, KQ, EFFNEW, J, ITQ, IPJ, RHO, IERROR)

ARGUMENTS:

VAL	Waked ship velocity (kts)
P	Torque per shaft (ft-lb)
T	Propeller thrust (lbs per shaft)
N1	Propeller rpm
D	Propeller diameter (ft)
Z	Number of blades of propeller
PDNEW	P/D of propeller
BAR	Blade area ratio
KT	Thrust coefficient
KQ	Torque coefficient
EFFNEW	Open water efficiency
J	Advance coefficient
ITQ	Index defined by:
	1 if thrust is input
ITQ =	2 if power is input
IPJ	Optimization index defined by:
	1 - no optimization, J known, calculates KT, KQ, EFFNEW only
	2 - optimize N with $KT/J^{**2}$
IPJ =	3 - optimize N with $KQ/J^{**3}$
	4 - optimize D with $KT/J^{**4}$
	5 - optimize D with $KQ/J^{**5}$
RHO	Water density
IERROR	Error message indicator

COMMON BLOCKS: NONE

SUBROUTINES CALLED: ROOT, TROST2, FUNCTION CALC

CALLED BY: PRODES

COMMENTS:

NAME: SUBROUTINE TROST2

PURPOSE: Subroutine TROST2 is used to calculate a single KT, KQ and efficiency value for a given propeller.

CALLING SEQUENCE: CALL TROST2 (KT, KQ, J, PDTR2, BAR, Z, EFFTR2)

ARGUMENTS:

KT	Thrust coefficient
KQ	Torque coefficient
J	Advance coefficient
PDTR2	Pitch to diameter ratio
BAR	Blade area ratio
Z	Number of blades
EFFTR2	Open water efficiency

COMMON BLOCKS: NONE

SUBROUTINE CALLED: Function CALC

CALLED BY: TROOST

COMMENTS:

NAME: SUBROUTINE WSURFB

PURPOSE: Subroutine WSURFB determines the surface area of a body of revolution given by Chebychev coefficients.

CALLING SEQUENCE: CALL WFSURFB (AREA)

ARGUMENT: AREA Surface area of a body (ft<sup>2</sup>)

COMMON BLOCKS: COEFS, INPUT, PHYSCO

SUBROUTINE CALLED: FUNCTION EVAL

CALLED BY: CHEB

COMMENTS:

NAME: SUBROUTINE WSURFS

PURPOSE: Subroutine WSURFS determines the wetted surface area of a strut.

CALLING SEQUENCE: CALL WSURFS (AREA)

ARGUMENT: AREA Wetted surface area of a strut (ft<sup>2</sup>)

COMMON BLOCKS: COEFS, INPUT

SUBROUTINE CALLED: FUNCTION EVAL

CALLED BY: CHEB

COMMENTS:

NAME:	FUNCTION YINTP								
PURPOSE:	Function YINTP interpolates through a set of discrete data.								
CALLING SEQUENCE:	YTP = YINTP (XA, X, Y, N)								
ARGUMENTS:	<table border="0"> <tr> <td>XA</td> <td>Point to be interpolated</td> </tr> <tr> <td>X</td> <td>Array of ordinate data</td> </tr> <tr> <td>Y</td> <td>Array of abscissa data</td> </tr> <tr> <td>N</td> <td>Number of data points</td> </tr> </table>	XA	Point to be interpolated	X	Array of ordinate data	Y	Array of abscissa data	N	Number of data points
XA	Point to be interpolated								
X	Array of ordinate data								
Y	Array of abscissa data								
N	Number of data points								
COMMON BLOCKS:	NONE								
SUBROUTINE CALLED:	NONE								
CALLED BY:	FORMDR								
COMMENTS:									



#### REFERENCES

- (1) Lin, L.W. and W.G Day, "The Still-Water Resistance and Propulsion Characteristics of Small-Waterplane-Area Twin-Hull (SWATH) Ships." AIAA/SNAME Advanced Marine Vehicles Conference. San Diego, California, 1974.
- (2) Proceedings of the 10th International Towing Tank Conference, London, England, 1963. Published by the National Physical Laboratory, England.
- (3) Lasky, M.P., "An Investigation of Appendage Drag." NSRDC/SPD Report 458-H-01.
- (4) Roddy, R.F. and J. Strom-Tejsen, "Study of Air Cushion Vehicle Propulsion System - Propulsor Design and Performance." NSRDC/SPD Report 378-09.

APPENDICES

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PROGRAM LISTING OF CLOSEFIT

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1      PROGRAM SWATH(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT,TAPE8)
2      SWATH
3      SWATH
4      SWATH
5      C      MAIN PROGRAM FOR RESISTANCE OF SWATH SHIP USING CHEBYCHEV
6      C      REPRESENTATION OF LINES- REVISED FALL 1974 WINTER 1975 - A.M. REED
7      C      2-D STRUTS PLUS SUBMERGED ELONGATED BODIES
8      C      INCLUDES 1-2 INTERFERENCE AND MULTIPLE HULL SPACINGS
9      C      MERGED WITH CHEB AND REVISED FOR TOTAL RESISTANCE--SPRING 1978
10     C
11     COMMON/OUT/HS,HB,XLS,XLB,TSMAX,AX,PI,G,RHO,GNU,WETS,WETB,WTSURF,
12     VMFPS,DELCF,TITLE(8),SPACE
13     C
14     COMMON/AUX/TS(10,10),WS(10,10),TB(10,10),WB(10,10),TSB(10,10),
15     WSB(10,10),TS12(8,10,10),WS12(8,10,10),TB12(8,10,10),
16     WB12(8,10,10),TSB12(8,10,10),WSB12(8,10,10),
17     TSBP(10,10),WSBP(10,10),TSB12P(8,10,10),WSB12P(8,10,10)
18     C
19     COMMON/OMEGA/MMAX,HSOLS,HBOILB,GAMAOS,GAMA0B,NOSEPS,
20     SEPDIS(8),SEP(8),CSTRUT(8),CSTR12(8),GOSO,PHIS,PHIB,
21     RATIOL
22     C
23     COMMON/PSI/NPTSZ,PTSAF,EXPN,NALMAX,NAL,TAIL,ALFA,ALSMAX,NSTEPS
24     C
25     COMMON / COEFS / ASM(10),BSM(10),ABM(10),BBM(10)
26     C
27     DATA D,MMAX / 0.0, 10 /
28     C
29     XLS = LENGTH OF STRUT (FT)
30     HS = DRAFT OF STRUT (FT)
31     TSMAX = MAXIMUM THICKNESS OF STRUT (FT)
32     ASM(1) = STRUT COSINE COEFFICIENTS
33     BSM(1) = STRUT SINE COEFFICIENTS
34     XLB = LENGTH OF BODY (FT)
35     HB = DEPTH OF SUBMERGENCE TO BODY CENTERLINE (FT)
36     AX = MAXIMUM BODY CROSS-SECTIONAL AREA (FT**2)
37     ABM(1) = BODY COSINE COEFFICIENTS
38     BBM(1) = BODY SINE COEFFICIENTS
39     SEPDIS = SEPARATION DISTANCE OF HULL CENTERLINES (FT)
40     NOSEPS = NUMBER OF SEPARATION DISTANCES TO BE TESTED (FT)
41     CSTRUT = DISTANCE OF CL OF STRUT FROM CL OF BODY (FT)
42     CSTR12 = DISTANCE OF CL OF SECOND STRUT( IF PRESENTED) FROM CL OF
43     BODY (FT)
44     (+ FORWARD OF THE BODY CL, - AFT OF THE BODY CL )
45     NLOC = NUMBER OF DIFFERENT STRUT LOCATIONS TO BE TESTED
46     NLOC2 = FLAG INDICATES 2-D STRUTS
47     NLOC2=0, SINGLE STRUT
48     NLOC2 .NE. 0, 2-D STRUTS
49     C      MMAX = MAXIMUM NUMBER OF TERMS USED IN CHEBYCHEV APPROXIMATION
50     C      WETS = WETTED SURFACE AREA OF STRUT
51     C      WETB = WETTED SURFACE AREA OF BODY
52     C      WTSURF = TOTAL WETTED SURFACE AREA OF STRUT AND BODY
53     C      SPACE = DECIMAL FRACTION OF SPACE BETWEEN TANDEM STRUTS TO STRUT
54     C      --FOR TANDEM STRUTS WHICH ARE NOT EQUAL
55     C
56     INPUT
57     SWATH
58     SWATH

```

```

60      C      699 CONTINUE
        READ ( 5,210 ) ( TITLE(K),K=1,8)
        READ (5,215) XLS,HS,TSMAX,SPACE
        C
        C CALL CHEB TO INPUT STRUT DATA AND COMPUTE CHEBYCHEV
        C COEFFICIENTS
        C
        C CALL CHEB (ASM,BSM,MMAX)
        C
        C READ(5,215) XLB,HB,AX
        C
        C CALL CHEB TO INPUT BODY DATA AND COMPUTE CHEBYCHEV
        C COEFFICIENTS
        C
        C CALL CHEB (ASM,BBM,MMAX)
        C
        C COMPUTE TOTAL WETTED SURFACE AREA
        C
        C WTSURF = WETS + WETB
        C
        C READ(5,220) NOSEPS
        C READ(5,215) (SEPDIS(I),I=1,NOSEPS)
        C READ(5,220) NLOC,NLOC2
        C READ(5,215) (CSTRUT(I),I=1,NLOC)
        C IF(NLOC2.NE.0) READ(5,215) (CSTR2(I),I=1,NLOC)
        C IF(NLOC2.NE.0) WTSURF=WTSURF+WETS-XLS-TSMAX*ASM(1)*PI/4.0
        C
        C ECHO INPUT
        C
        C CALL ECHO (NLOC)
        C
        C PLOT BODY SECTIONAL AREA CURVE AND STRUT WATERPLANE OUTLINE
        C CURVE
        C
        C CALL PCHEB (ASM,BSM,ABM,BBM,MMAX,TITLE)
        C
        C HSOLS = HS/XLS
        C HBOLB = HB/XLB
        C RATIQL =XLB/XLS
        C
        C INPUT TEST VELOCITIES
        C
        C VMFPS=SHIP SPEED IN FEET PER SECOND
        C JTEST = SWITCH SET TO ZERO IF NO PRINTING OF T AND W
        C MATRICES IS NEEDED
        C
        C 710 READ (5,603) VMFPS, JTEST
        C IF (VMFPS.EQ.0.) GO TO 699
        C IF(VMFPS.LT.0.0) STOP
        C GAMADS = G*XLS*.5 / VMFPS**2
        C GAMAOB = GAMADS*XLB/XLS
        C
        C CALCULATE T, W FOR ALL MODEL CONFIGURATION AT ONE

```

```

115      C      SPEED BY CALLING RWAVE
      C
      DO 732 I=1,NLOC
      B=CSTRUT(I)/XLS
      IF(NLOC2.NE.0) D=CSTRT2(I)/XLS
      CALL RWAVE(B,D,NLOC2)
      IF (JTEST.EQ.0) GO TO 722
120
      C      PRINT THE AUXILIARY FUNCTION TABLES , IF JTEST .NE. 0
      C
      C      CALL PRINT (I,NLOC2)
      C
      C      CALCULATE DRAG COEFFICIENTS AND DRAG FORCES
      C
      C      CALL RWOUT(I,NLOC2)
      C
      C      CONTINUE
      C      GO TO 710
130
      C      210 FORMAT(8A10)
      C      215 FORMAT(8F10.5)
      C      220 FORMAT(5I5)
      C      603 FORMAT(F10.5,2I5)
      C      END
135

```

```

SWATH 116
SWATH 117
SWATH 118
SWATH 119
SWATH 120
SWATH 121
SWATH 122
SWATH 123
SWATH 124
SWATH 125
SWATH 126
SWATH 127
SWATH 128
SWATH 129
SWATH 130
SWATH 131
SWATH 132
SWATH 133
SWATH 134
SWATH 135
SWATH 136
SWATH 137
SWATH 138
SWATH 139

```

13.06.42

04/07/81

FTN 4.6+460

TRACE

74/74

BLOCK DATA BLKDAT.

OPT=0

ROUND=

/

```

1      C      BLOCK DATA
COMMON/OUT/HS,HB,XLS,XLB,TSMAX,AX,PI,G,RHO,GNU,WETS,WETB,WTSURF,
1      VMFPS,DELCP,TITLE(8),SPACE
5      C      COMMON / PSI / NPTSZ,PTSFAF,EXP,NALMAX,NAL,TAIL,ALFA,ALMAX,NSTEPS
COMMON/PLOT/NFIRST,NLAST,NPOINT,XMAX,XMIN,NSCL1,NCHAR,NSCALE(4),
1      PCHAR(2)
COMMON/XRPLQTQ/I,J,K,L,NHL,NSBH,NVL,NSBV,HCHAR,VCHAR,ISX,ISY,V,H
10     C      LOGICAL NSCL1
C      DEFINE PHYSICAL CONSTANTS
C
15     C      DATA PI / 3.1415926535897 /
DATA RHO / 1.9367 /
DATA G / 32.155 /
DATA GNU / 1.2970E-5 /
DATA DELCP / 5.0E-4 /
20     C      DEFINE CONSTANTS FOR NUMERICAL INTEGRATION
C
25     C      DATA NPTSZ / 31 /
DATA PTSFAF / 10.0 /
DATA EXPN / 7.0 /
DATA NALMAX / 300 /
DATA ALSMAX / 26.0 /
30     C      DEFINE DATA FOR PLOT ROUTINE
C
35     C      DATA NHL, NSBH, NVL, NSBV, HCHAR, VCHAR, PCHAR(1), PCHAR(2) /
1      6, 10, 11, 10, 1H., 1H., 1HS, 1HB /
C      DATA NFIRST, NLAST, NPOINT / 1, 101, 1 /
C      DATA XMAX, XMIN, NSCL1 / 1.0, -1.0, .TRUE. /
C      DATA NCHAR / 0 /
40     C      DATA NSCALE / 0.3, 0.3 /
END

```

04/07/81 13.06.42

FTN 4.6+460

74/74 OPT=0 ROUND=0/ TRACE

SUBROUTINE ECHO

```

1      SUBROUTINE ECHO (NLOC)
      C
      C      ECHO SHIP DATA
      C
      COMMON/AUX/TS(10,10),WS(10,10),TB(10,10),WB(10,10),TSB(10,10),
1      WSB(10,10),TS12(8,10,0),WS12(8,10,10),TB12(8,10,10),
2      WS12(8,10,10),TSB12(8,10,10),WSB12(8,10,10)
3      ,TSBP(10,10),WSP(10,10),TSB12P(8,10,10),WSB12P(8,10,10)
      C
      COMMON/OMEGA,MNAX,HSOLS,H8OLB,GAMAQS,GAMA0B,NOSEPS,
1      SEPDIS(8),SEP(8),CSTRUT(8),CSTRT2(8),GOSQ,PHIS,PHIB,
2      RATIOI
      C
      COMMON/OUT/HS,HB,XLS,XLB,TSMAX,AX,PI,G,RHO,GNU,WETS,WETB,WTSURF,
1      VMFPS,DELCF,TITLE(8),SPACE
      C
      COMMON/COEFS/ASM(10),BSM(10),ABM(10),BBM(10)
      WRITE (6,310) (TITLE(K),K=1,8)
      WRITE (6,315) MNAX
      WRITE (6,325) XLS,HS,TSMAX
      WRITE (6,330) (ASM(K),K=1,MNAX)
      WRITE (6,335) (BSM(K),K=1,MNAX)
      WRITE (6,340) (ABM(K),K=1,MNAX)
      WRITE (6,345) (BBM(K),K=1,MNAX)
      WRITE (6,350) (WTSURF)
      WRITE (6,355) (SEPDIS(I),I=1,NOSEPS)
      WRITE (6,356) (CSTRUT(I),I=1,NLOC)
      RETURN
310 FORMAT(1H1,///,3X,* SUMMARY OF DATA FOR *.8A10//)
315 FORMAT(1H,5X,45H NUMBER OF TERMS IN HULL COEFFICIENT SERIES =,I6)
325 FORMAT(1H,3X,35H STRUT GEOMETRIC CHARACTERISTICS ,///,5X,
1      BH XLS =,F12.6,9X,BH HS =,F12.6,9X,8H TSMAX =,F12.6)
330 FORMAT(1H0,33X,*STRUT CHEBYCHEV COEFFICIENTS ASM(M)*/(10X,5E16.8))
335 FORMAT(1H0,33X,*STRUT CHEBYCHEV COEFFICIENTS BSM(M)*/(10X,5E16.8))
340 FORMAT(1H0,3X,35H BODY GEOMETRIC CHARACTERISTICS ,///,5X,
1      BH XLB =,F12.6,9X,8H HB =,F12.6,9X,8H AX =,F12.6)
345 FORMAT(1H0,33X,*BODY CHEBYCHEV COEFFICIENTS ABM(M)*/(10X,5E16.8))
350 FORMAT(1H0,33X,*BODY CHEBYCHEV COEFFICIENTS BBM(M)*/(10X,5E16.8))
355 FORMAT(1H0,5X,* SEPARATION DISTANCE IN FEET =*,8F8.3)
356 FORMAT(1H0,3X,35H STRUT LOCATION IN FEET =*,8(2X,F10.4))
357 FORMAT(1H0,4X,* WEIETED SURFACE IN SQUARE FEET =*,F12.3)
      END

```





PRINT 59  
PRINT 60  
PRINT 61  
PRINT 62  
PRINT 63  
PRINT 64  
PRINT 65

712 CONTINUE  
RETURN  
903 FORMAT(1X,8I10)  
904 FORMAT(1X,10E13.5)  
905 FORMAT(1X)  
906 FORMAT (1H1,30X,\* AUXILIARY FUNCTION TABLE OF T AND W \*)  
END

13.06.42

04/07/81

FTN 4.6+460

74/74 OPT=0 ROUND=0/ TRACE

SUBROUTINE RWOUT

```

1      SUBROUTINE RWOUT(I,NLOC2)
C
C      COMPUTE DRAG COMPONENTS, DRAG COEFFICIENTS, AND TOTAL
C      RESISTANCE
C
5      COMMON/OUT/HS,HB,XLS,XLB,TSMAX,AX,PI,G,RHO,GNU,WETS,WEIB,WTSURF,
C      VMFPS,DELCF,TITLE(8),SPACE
C
10     COMMON/AUX/TS(10,10),WS(10,10),TB(10,10),WB(10,10),TSB(10,10),
C      WSB(10,10),TS12(8,10,10),WS12(8,10,10),TB12(8,10,10),
C      WB12(8,10,10),TSB12(8,10,10),WSB12(8,10,10),
C      TSBP(10,10),WSBP(10,10),TSB12P(8,10,10),WSB12P(8,10,10)
C
15     COMMON/OMEGA/MNAX,HSOLS,HBOLB,GAMAOS,GMAO8,NOSEPS,
C      SEPDIS(8),SEP(8),CSTRUT(8),CSTRT2(8),GOSQ,PHIS,PHIB,
C      RATIOI
C
20     DO 88 L=1,NOSEPS
C      SUM = A(TRANSPQSE)*T*A + B(TRANSPQSE)*W*B
C
25     CALL SUM(L,SUM1S,SUM1B,SUM1SB,SUM12S,SUM12B,SM12SB)
C
30     B2OLB = SEPDIS(L)/XLB
C      CSOLB=CSTRUT(L)/XLB
C
35     REYNOLDS NUMBER OF STRUT AND BODY
C
C      RNS = XLS * VMFPS / GNU
C      RNB = XLB * VMFPS / GNU
C      IF(NLOC2.NE.0) CSOLB2=CSTRT2(L)/XLB
C      AAS = (TSMAX/HS)/(PI/2.0)*GMAO8
C      AAB = 2.0*PI*(AX/XLB**2)*(GMAO8/GMAO8**2)
C      AASB = (2.0*PI)*AX/(HS*XLS)
C      AAWTSF = (0.5*RHO*WTSURF*VMFPS**2)/1000.
C
40     COMPUTE WAVE RESISTANCE
C
C      CMS1 = AAS*SUM1S
C      R1S = CMS1*RHO*G*TSMAX*HS*XLS
C      CWS1 = R1S/AAWTSF
C
45     CMB1 = AAB*SUM1B
C      R1B = CMB1*RHO*G*AX*XLB
C      CWB1 = R1B/AAWTSF
C
50     CMSB1 = AASB*SUM1SB
C      R1SB = CMSB1*RHO*G*TSMAX*HS*XLS
C      CWSB1 = R1SB/AAWTSF
C      C1 = CWS1+CWB1+CWSB1
C
55     CMS12 = AAS*SUM12S
C      R12S = CMS12*RHO*G*TSMAX*HS*XLS
C      CWS12 = R12S/AAWTSF
C
C      CMB12 = AAB*SUM12B
C      R12B = CMB12*RHO*G*AX*XLB

```

```

60      C
      CWB12 = R12B/AWTSF
      CMSB12 = AASB*SM12SB
      R12SB = CMSR12-RHO-G*TSMAX*HS*XL5
      CWSB12 = R12SB/AWTSF
      C2 = CWS12+CWB12+CWSB12
      C3 = C1+C2
      C
      FROUDE NUMBER
      FROUDS = VMFPS/SQRT(32.155*XL5)
      VLS = FROUDS*SQRT(G)/1.6878
      FROUDB = VMFPS/SQRT(32.155*XL5)
      VLB = FROUDB*SQRT(G)/1.6878
      VMKNITS = VMFPS/1.6878
      C
      COMPUTE THE FORM DRAG
      CFORM = FORMDR (VLS)
      CR = C3 + CFORM
      RR = CR * AWTSF
      C
      COMPUTE FRICTIONAL DRAG
      CFS = CFITTC (RNS)
      CFB = CFITTC (RNB)
      RFS = 0.5*RHO*VMFPS*VMFPS*WETS*(CFS+DELCF)
      RFB = 0.5*RHO*VMFPS*VMFPS*WETB*(CFS+DELCF)
      RF = RFS + RFB
      CFSP = RFS / AWTSF
      CFBP = RFB / AWTSF
      CF = CFSP + CFBP
      C
      COMPUTE TOTAL DRAG
      CT = CR + CF
      RT = RR + RF
      C
      COMPUTE EHP
      EHP = RT * VMFPS / 550.
      C
      OUTPUT
      WRITE(6,410) (TITLE(K),K=1,8)
      WRITE(6,325) XLS,HS,TSMAX
      WRITE(6,415) GAMAOB,FROUDS,MSOLS
      WRITE(6,340) XLB,HB,AX
      WRITE(6,420) GAMAOB,FROUDB,HBOLB
      WRITE(6,356) SEPDIS(L),B2OLB
      IF(NLOC2.NE.0) GO TO 15
      WRITE(6,358) CSTRUT(1),CSOLB
      GO TO 20
      15 WRITE(6,359) CSTRUT(1),CSOLB,CSTRUT2(1),CSOLB2
      20 WRITE(6,357) WTSURF
      WRITE (6,360) VMFPS,VMKNITS,VLS,VLB
      WRITE(6,430) CNS1,RIS,CWS1

```

13.06.42

04/07/81

FTN 4.6+460

74/74 OPT=0 ROUND=\*/ TRACE

SUBROUTINE RWOUT

```

115 WRITE(6,440) CNB1,R18,CWB1
    WRITE(6,445) CNSB1,R15B,CWSB1,C1
    WRITE(6,450) CNS12,R12S,CWS12
    WRITE(6,455) CNB12,R12B,CWB12
    WRITE(6,460) CNSB12,R12SB,CWSB12,C2,C3
120 WRITE(6,510) CR,RR
    WRITE(6,520) CF,RF
    WRITE(6,530) CT,RT
    WRITE(6,540) EHP
125 CONTINUE
    RETURN
325 FORMAT(1H,3X,35H STRUT GEOMETRIC CHARACTERISTICS ,//.5X,
1 8H XLS =,F12.6,9X,8H HS =,F12.6,9X,8H TSMAX =,F12.6)
340 FORMAT(1H0,3X,35H BODY GEOMETRIC CHARACTERISTICS ,//.5X,
1 8H XLB =,F12.6,9X,8H HB =,F12.6,9X,8H AX =,F12.6)
356 FORMAT(*0 SEPARATION DISTANCE IN FEET =*,F8.3,
1 5X,* B/LB =*,F7.3)
357 FORMAT(1H0,4X,* WETTED SURFACE OF A DEMI-HULL IN SQUARE FEET =*,
1 F12.3)
358 FORMAT(*0 STRUT CL FROM BODY CL IN FEET =*,F8.3,
1 5X,*STRUT OFFSET/LB =*,F7.3)
359 FORMAT(*0 FORWARD STRUT CL FROM BODY CL IN FEET =*,F8.3,
1 5X,*FORWARD STRUT OFFSET/LB =*,F7.3//
2 * AFT STRUT CL FROM BODY CL IN FEET =*,F8.3,
3 5X,*AFT STRUT OFFSET/LB =*,F7.3)
140 FORMAT(1H0,5X,* SHIP SPEED IS *,F8.3,* FPS, *,F8.3,* KNOTS, *,
1 6X,* STRUT V-L RATIO =*,F8.3,6X,*BODY V-L RATIO = *,F8.3)
410 FORMAT(*1 *.35H SHIP RESISTANCE CALCULATIONS FOR ,8A10)
415 FORMAT(1H,4X,
1 F12.6,9X,8H HS/LS =,F12.6)
420 FORMAT(1H,4X,
1 F12.6,9X,8H HB/LB =,F12.6)
430 FORMAT(1H0,30H WAVE RESISTANCE IN POUNDS
1 30H RSW/(RHO*G*TSMAX*HS*LS) = ,E16.8,
2 /.30H FOR A DEMI-HULL
3 32H STRUT WAVE DRAG IN POUNDS = ,F10.3,/30X,
2 32H R15/(RHO/2*WTSURF*V**2) = ,F10.3,4HE-03)
440 FORMAT(1H0,29X,30H RBW/(RHO*G*AX*LB)
1 32H BODY WAVE DRAG IN POUNDS = ,E16.8,/30X,
2 32H R13/(RHO,2*WTSURF*V**2) = ,F10.3,/30X,
2 32H R18/(RHO,2*WTSURF*V**2) = ,F10.3,4HE-03)
445 FORMAT(1H0,29X,30H RSBW/(RHO*G*TSMAX*HS*LS) =,E16.8,/30X,
1 32H STRUT-BODY WAVE DRAG IN LBS = ,F10.3,/30X,
2 32H R15B/(RHO/2*WTSURF*V**2) = ,F10.3,4HE-03,
3 10X,10H CW1 TOT =,F10.3,4HE-03)
450 FORMAT(1H0,29X,30H R12SB/(RHO*G*TSMAX*HS*LS) =,E16.8,/30X,
1 32H STRUT INTERFERENCE DRAG LBS = ,F10.3,/30X,
2 32H R12S/(RHO/2*WTSURF*V**2) = ,F10.3,4HE-03)
455 FORMAT(1H0,29X,30H R12BW/(RHO*G*AX*LB)
1 32H BODY INTERFERENCE DRAG LBS = ,E16.8,/30X,
2 32H R12B/(RHO,2*WTSURF*V**2) = ,F10.3,/30X,
2 32H R12B/(RHO,2*WTSURF*V**2) = ,F10.3,4HE-03)
460 FORMAT(1H0,29X,30H R12SBW/(RHO*G*TSMAX*HS*LS) =,E16.8,/30X,
1 32H STRUT-BODY INTERFERENCE DRAG LB = ,F10.3,/30X,
2 32H R12SB/(RHO,2*WTSURF*V**2) = ,F10.3,4HE-03,
3 10X,10H CW2 TOT =,F10.3,4HE-03,/.66X,10H CW TOT =,F10.3,
4 4HE-03)
510 FORMAT(1H0,29H RESIDUAL RESISTANCE
1 30H RESIDUAL DRAG COEFFICIENT = ,F10.3,4HE-03,
170 RWOUT
171 RWOUT
172 RWOUT

```

SUBROUTINE	RWOUT	74/74	OPT=0	ROUND=*	TRACE	FTN	4.6+460	04/07/81	13.06.42	PAGE	4
175											
	2	/30X,30H	RESIDUAL RESISTANCE	=			.F10.3,4H LBS)	RWOUT			173
	520	FORMAT(1H0.29X,30H	FRICTIONAL DRAG COEFF.				=,F10.3,4HE-03,	RWOUT			174
	1	/30X,30H	FRICTIONAL RESISTANCE				=,F10.3,4H LBS)	RWOUT			175
	530	FORMAT(//13X,*TOTAL	DRAG COEFFICIENT IS	*			.F10.3,4HE-03,	RWOUT			176
	1	//15X,*TOTAL	RESISTANCE FOR A DEMI-HULL	*			.F10.3,4H LBS)	RWOUT			177
	540	FORMAT (//20X,* EHP	FOR A DEMI-HULL	*			.F10.3)	RWOUT			178
		END						RWOUT			179

```

1      SUBROUTINE SIMPSN(NPTS,SIMP)
      C
      C      SET UP SIMPSON'S MULTIPLIERS FOR INTEGRATION
      C      ODD NUMBER OF POINTS GREATER THAN 1 REQUIRED
      C
5      DIMENSION SIMP(NPTS)
      IF((NPTS/2)-2.NE.NPTS) GO TO 3
      WRITE(5,90)
      NPTS = NPTS+1
      SIMP(1) = 1.0
      SIMP(NPTS) = 1.0
      NPTSM1=NPTS-1
      SM=2.0
      DO 5 J=2,NPTSM1
      SM=6.0-SM
      SIMP(J)=SM
      RETURN
      FORMAT(1H0,*EVEN NO. OF POINTS GIVEN - ADDITIONAL POINT SUPPLIED-)
      END
10
15
90
20

```





```

1      SUBROUTINE RWAVE(B,D,NLOC2)
C
C      SUBROUTINE FOR COMPUTING AUXILIARY FUNCTIONS T AND W
C      USING CHEBYSHEV EXPANSION - PROGRAM VERSION OF 8/05/72
C      MODIFICATIONS BY A M REED OCTOBER 1974
C
5      DIMENSION VJALFA(21), SIMP(100), SEPCOS(8)
C
10     COMMON/OUT/HS,HB,XLS,XLB,TSMAX,AX,PI,G,RHO,GNU,WETS,WETB,WTSURF,
C      VMFPS,DELCP,TITLE(8),SPACE
C
15     COMMON/AUX/TS(10,10),WS(10,10),TB(10,10),WB(10,10),TSB(10,10),
C      WSB(10,10),TS12(8,10,10),WS12(8,10,10),TB12(8,10,10),
C      WB12(8,10,10),TSB12(8,10,10),WSB12(8,10,10),
C      TSBP(10,10),WSBP(10,10),TSB12P(8,10,10),WSB12P(8,10,10)
C
20     COMMON/OMEGA/MNAX,HSOLS,HBOLB,GAMAOS,GMAOB,NOSEPS,
C      SEPDIS(8),SEP(8),CSTRUT(8),CSTRT2(8),GOSQ,PHIS,PHIB,
C      RATIOL
C
25     COMMON/PSI/NPTSZ,PTSAF,EXP,NALMAX,NAL,TAIL,ALFA,ALSMAX,NSTEPS
C
C      DATA PI / 3.1415926535897 /
C
C      NOSEPS IS THE NUMBER OF HULL SEPARATIONS
C      MNAX IS MAXIMUM NUMBER OF TERMS IN CHEBYSHEV SERIES
C
30     MNAX2 = 2*MNAX
C      GOSQ=GAMAOS**2
C      PHIS = 2.0*HSOLS/GAMAOS
C      PHIB = 2.0*HBOLB/GMAOB
C      RATIOL = GMAOB/GAMAOS
C
C      SET THE T AND W ARRAYS TO ZERO
C
35     CALL RINIT
C      DO 5 L=1,NOSEPS
C      SEP(L) = (2.0/GAMAOS)*SEPDIS(L)/XLS
C
40     INTEGRATION OF T AND W FROM ALPHA EQUALS GAMAOS TO GAMAOS+1.0
C      MAKE TRIGONOMETRIC SUBSTITUTION TO AVOID SQUARE ROOT
C      SINGULARITY AT ALPHA EQUALS GAMAOS
C
45     ZETA IS THE VARIABLE OF INTEGRATION--ZETA=SQRT(ALPHA-GAMAOS)
C      NPTSZ IS THE NUMBER OF POINTS TO TAKE IN THE INTERVAL
C      0.0 LESS THAN OR EQUAL ZETA LESS THAN OR EQUAL 1.0
C      AINCR IS THE STEP SIZE FOR THE ZETA INTEGRATION
C      ALFAZ IS THE VALUE OF ALPHA FOR ZETA VARYING FROM ZERO TO ONE
C
50     CALL SIMPSON(NPTSZ,SIMP)
C      XNPTZ=FLOAT(NPTSZ)
C      AINCR = 1.0/(XNPTZ-1.0)
C      HZETA = AINCR/3.0
C      DO 30 I=1,NPTSZ
C      SIMP(I) = SIMP(I)+HZETA
C      EI=FLOAT(I-1)

```

13.06.42

04/07/81

FTN 4.6+460

74/74 OPT=0 ROUND=0/ TRACE

SUBROUTINE RWAVE

```

60      ZETA = AINCR*EI
      ALFAZ = GAMMAOS+ZETA**2
      ALFASQ=ALFAZ**2
      SQZTA=2.0/SQRT(GAMMAOS*ALFAZ)
      DO 11 L=1,NOSEPS
      SEPCOS(L) = COS(SEP(L)*ALFAZ*SQRT(ALFASQ-GOSQ))
      CALL RINTEG(ALFAZ,B,D,NLOC2,SIMP(1),SEPCOS,SQZTA)
      CONTINUE
11      C
65      C
      C
      C      INTEGRATION FOR T AND W FROM ALPHA EQUALS GAMMAOS+1.0 TO ALMAX
      NAL = 0
      ALFA = GAMMAOS + 1.
      PWT = 0.
      ALMAX = ((2.302585*EXPN*GAMMAOS) / (2.*HBDLB*RATIOI)
1          + (GAMMAOS+1.)**2)**.5
      ISIMP = 1
210      IF (ALFA.GT.ALMAX) GO TO 215
      IF (NAL.LT.NALMAX) GO TO 212
      WRITE (6,302)
      GO TO 215
212      NAL = NAL + 2
      DQDA = (2.*ALFA**2 - GAMMAOS**2)/(ALFA**2-GAMMAOS**2)**.5
      SSIZE=(2.*PI)/((2.*RATIOI+DQDA*SEP(1))*PTSAP)
      TWT= SSIZE/3.
      WTINT = TWT + PWT
      PWT = TWT
      GO TO 250
      ISIMP=3
215      WTINT = PWT
      GO TO 250
      WTINT = 4.*TWT
      ISIMP = 2
      CONTINUE
      ALFASQ=ALFA**2
      SQ=1.0/SQRT(ALFASQ-GOSQ)
      DO 41 L=1,NOSEPS
      SEPCOS(L) = COS(SEP(L)*ALFA/SQ)
      CALL RINTEG(ALFA,B,D,NLOC2,WTINT,SEPCOS,SQ)
      ALFA = ALFA + SSIZE
      IF (ISIMP-2) 220,210,270
      C
      C      ADD TAIL INTEGRATION TO TS AND WS
      C
      ALFA = ALFA - SSIZE
      NSTEPS = 0
      IF (ALSMAX.LE.ALFA) GO TO 278
      SSIZE = PI/PTSAP
      ANSTEP = (ALSMAX-ALFA)/SSIZE
      NSTEPS = IFIX(ANSTEP/2.)*2 + 2
      SSIZE = (ALSMAX-ALFA) / NSTEPS
      WT = SSIZE/3.
      ANWT = 1.
      NDO = NSTEPS + 1
      CON=1.0
      CO 277 100 = 1,NDO
      ALFASQ=ALFA**2
110      C
100      C
270      C
105      C
110      C

```

04/07/81 13.06.42

FTN 4.6+460

74/74 OPT=0 ROUND=\*\*/ TRACE

SUBROUTINE RWAVE

```

115 IF(NLOC2.NE.0) CON=2.0*(1.0+COS((B-D)*ALFA*2.0))
    CALL BESSJ(ALFA,MNAX2,VJALFA)
    VS = PHIS*ALFASQ
    SQ=1.0/SQRT(ALFASQ-GOSQ)
    ESA = 1.0
    IF ( VS .LT. 300.0 ) ESA = ESA- EXP(-VS)
    ES = SQ * ESA**2 / ALFASQ
    DO 276 M = 1,MNAX
        MAA = 2*M
        MBB = MAA + 1
    DO 276 N = 1,MNAX
        NAA = 2*N
        NBB = NAA + 1
        WTINT = ANWT * WT
        TSA = WTINT*ES*VJALFA(MAA)*VJALFA(NAA)*CON
        WSA = WTINT*ES*VJALFA(MBB)*VJALFA(NBB)*CON
        TS(M,N) = TS(M,N) + TSA
        WS(M,N) = WS(M,N) + WSA
        ALFA = ALFA + SSIZE
        BNWT = 2.
    IF (ANWT.LE.2.) BNWT = 4.
    IF (100.EQ.NDO-1) BNWT = 1.
    ANWT = BNWT
276 ALFASQ=ALFA**2
277 RAT = GAMAOS/ALFA
278 IF (RAT.LT.1.E-4) GO TO 280
    TAIL=(-SQRT(ALFASQ-GOSQ)/ALFASQ+ASIN(RAT)/GAMAOS)/(2.0*PI*GOSQ)
    GO TO 290
    TAIL=1.0/(3.0*PI*ALFA*ALFASQ)
280 C
    C
    C
290 C
    DO 296 M = 1,MNAX
    DO 296 N = 1,MNAX
        SIGN = (-1)**(M+N)
        TS(M,N) = TS(M,N) - SIGN*TAIL
        WS(M,N) = WS(M,N) + SIGN*TAIL
    CONTINUE
    C
    C
    C
    MULTIPLY BY CONSTANTS AND REFLECT SYMMETRIC MATRICIES)
    CALL REFLKT
    RETURN
    FORMAT ('=1ALFA INTEGRATION REACHED NALMAX=')
302 END

```

```

1      SUBROUTINE RINIT
2
3      C
4      C
5      C
6      C
7      C
8      C
9      C
10     C
11     C
12     C
13     C
14     C
15     C
16     C
17     C
18     C
19     C
20     C
21     C
22     C
23     C
24     C
25     C
26     C
27     C
28     C
29     C
30     C
31     C
32     C
33     C
34     C
35     C
36     C
37     C
38     C
39     C
40     C
41     C
42     C
43     C
44     C
45     C
46     C

```

INITIALIZE THE T AND W ARRAYS TO ZERO

COMMON/AUX/TS(10,10),WS(10,10),TB(10,10),WB(10,10),TSB(10,10),  
 1 WSB(10,10),TS12(8,10,10),WS12(8,10,10),TB12(8,10,10),  
 2 WB12(8,10,10),TSB12(8,10,10),WSB12(8,10,10),  
 3 TSBP(10,10),WSBP(10,10),TSB12P(8,10,10),WSB12P(8,10,10)

COMMON/OMEGA/MNAX,HSOLS,HBOLB,GAMAOS,GAMADB,NOSEPS,  
 1 SEPDIS(8),SEP(8),CSTRUT(8),CSTR2(8),GOSO,PHIS,PHIB,  
 2 RATIOI

DO 4 M=1,MNAX  
 DO 4 N=M,MNAX  
 TS(M,N) = 0.0  
 WS(M,N) = 0.0  
 TB(M,N) = 0.0  
 WB(M,N) = 0.0  
 TSB(M,N) = 0.0  
 TSBP(M,N) = 0.0  
 TSB(N,M) = 0.0  
 TSBP(N,M) = 0.0  
 WSB(M,N) = 0.0  
 WSBP(M,N) = 0.0  
 WSB(N,M) = 0.0  
 WSBP(N,M) = 0.0

DO 4 L=1,NOSEPS  
 TS12(L,M,N) = 0.0  
 WS12(L,M,N) = 0.0  
 TB12(L,M,N) = 0.0  
 WB12(L,M,N) = 0.0  
 TSB12(L,M,N) = 0.0  
 TSB12P(L,M,N) = 0.0  
 TSB12(L,N,M) = 0.0  
 TSB12P(L,N,M) = 0.0  
 WSB12(L,M,N) = 0.0  
 WSB12P(L,M,N) = 0.0  
 WSB12(L,N,M) = 0.0  
 WSB12P(L,N,M) = 0.0

CONTINUE  
 RETURN  
 END

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FTN 4.6+460

TRACE

74/74

SUBROUTINE RINTEG

OPT=0

ROUND=

/

TRACE

```

1      SUBROUTINE RINTEG(ALFA,B,D,NLOC2,WTINT,SEPCOS,SQ)
2      RINTG
3      C
4      C
5      C
6      C
7      C
8      C
9      C
10     C
11     C
12     C
13     C
14     C
15     C
16     C
17     C
18     C
19     C
20     C
21     C
22     C
23     C
24     C
25     C
26     C
27     C
28     C
29     C
30     C
31     C
32     C
33     C
34     C
35     C
36     C
37     C
38     C
39     C
40     C
41     C
42     C
43     C
44     C
45     C
46     C
47     C
48     C
49     C
50     C
51     C
52     C
53     C
54     C
55     C
56     C
57     C
58     C

      NUMERICAL INTEGRATION FOR AUXILIARY FUNCTIONS T AND W

      COMMON/AUX/TS(10,10),WS(10,10),TB(10,10),WB(10,10),TSB(10,10),
      WSB(10,10),TS12(8,10,10),WS12(8,10,10),TB12(8,10,10),
      WB12(8,10,10),TSB12(8,10,10),WSB12(8,10,10),
      TSBP(10,10),WSBP(10,10),TSB12P(8,10,10),WSB12P(8,10,10)

      COMMON/OMEGA/MMAX,HSOLS,HBO1B,GAMA0B,NOSEPS,
      SEPDIS(B),SEP(B),CSTRUT(8),CSTRT2(8),GOSQ,PHIS,PHIB,
      RATIOL

      DIMENSION VJALFA(21), VJBETA(21), SEPCOS(8)

      MMAX2=2*MMAX
      BEJA = RATIOL*ALFA
      ALFASQ=ALFA**2

      CALCULATE FACTORS FOR STRUT NOT CENTERED

      CO=COS(B*ALFA*2.0)
      S1=SIN(B*ALFA*2.0)
      CON=1.0
      IF (NLOC2.EQ.0) GO TO 32

      CALCULATE FACTORS FOR TANDEM STRUTS

      CO=(CO+COS(D*ALFA*2.0))
      S1=(S1+SIN(D*ALFA*2.0))
      CON=2.0*(1.0+COS((B-D)*ALFA*2.0))
      CONTINUE

      COMPUTE AUXILIARY FUNCTIONS VJALFA AND VJBETA

      CALL BESSJ(ALFA,MMAX2,VJALFA)
      CALL BESSJ(BETA,MMAX2,VJBETA)

      COMPUTE AUXILIARY FUNCTIONS ES AND EB

      VS=PHIS*ALFASQ
      VB = PHIB*BETA**2
      ESA = 1.0
      EBA = 0.0
      IF(VS .LT. 300.) ESA = ESA-EXP(-VS)
      IF(VB .LT. 300.) EBA = EXP(-VB)
      ES=SQ*ESA**2/ALFASQ
      EB=SQ*EBA**2/ALFASQ
      ESB = SQ*ESA*EBA

      TB,TS,WB,WS,TW12,TS12,WB12, AND WS12 ARE ALL SYMMETRIC WRT M
      AND N SO WE NEED ONLY CALCULATE THE UPPER HALF OF THESE
      MATRICES

      DO 55 M=1,MMAX

```

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SUBROUTINE RINTEG 74/74 OPT=0 ROUND=0/ TRACE

```

60      MAA = 2*M
      MBB = 2*M+1
      DO 55 N=M,MMAX
      NAA = 2*N
      NBB = 2*N+1
      TSA = WTINT*ES-VJALFA(MAA)*VJALFA(NAA)*CON
      WSA = WTINT*ES-VJALFA(MBB)*VJALFA(NBB)*CON
      TBA = WTINT*EB-VJBETA(MAA)*VJBETA(NAA)
      WBA = WTINT*EB-VJBETA(MBB)*VJBETA(NBB)
      TSBA = -WTINT*ESB-VJBETA(NAA)*VJALFA(MAA)*CO
      TSBA = -WTINT*ESB-VJBETA(NBB)*VJALFA(MBB)*CO
      WBSA = WTINT*ESB-VJBETA(NBB)*VJALFA(MBB)*SI
      WBSA = WTINT*ESB-VJBETA(NBB)*VJALFA(MBB)*SI
      TSBB = -WTINT*ESB-VJBETA(MAA)*VJALFA(NAA)*CO
      TSBB = -WTINT*ESB-VJBETA(MAA)*VJALFA(NAA)*CO
      WBSB = WTINT*ESB-VJBETA(MBB)*VJALFA(NBB)*CO
      WBSB = WTINT*ESB-VJBETA(MBB)*VJALFA(NBB)*CO
      TBB = TB(M,N)+TBA
      WBB(M,N) = WB(M,N)+WBA
      TSBB(M,N) = TSBB(M,N)+TSBA
      TSBB(M,N) = TSBB(M,N)+TSBA
      WBSB(M,N) = WBSB(M,N)+WSBA
      WBSB(M,N) = WBSB(M,N)+WSBA
      IF(M.EQ.N) GO TO 54
      TSBN(M) = TSBN(M)+TSBB
      TSBN(M) = TSBN(M)+TSBBP
      WBSN(M) = WBSN(M)+WSBB
      WBSN(M) = WBSN(M)+WSBBP
      CONTINUE
      TS(M,N) = TS(M,N)+TSA
      WS(M,N) = WS(M,N)+WSA
      DO 55 L=1,NDSEPS
      TS12(L,M,N) = TS12(L,M,N)+TSA*SEPCOS(L)
      WS12(L,M,N) = WS12(L,M,N)+WSA*SEPCOS(L)
      IF(EBA.EQ.0.0) GO TO 55
      TB12(L,M,N) = TB12(L,M,N)+TBA*SEPCOS(L)
      WB12(L,M,N) = WB12(L,M,N)+WBA*SEPCOS(L)
      TS12(L,M,N) = TS12(L,M,N)+TSBA*SEPCOS(L)
      TS12P(L,M,N) = TS12P(L,M,N)+TSBAP*SEPCOS(L)
      WS12(L,M,N) = WS12(L,M,N)+WSBA*SEPCOS(L)
      WS12P(L,M,N) = WS12P(L,M,N)+WSBAP*SEPCOS(L)
      IF(M.EQ.N) GO TO 55
      TS12(L,N,M) = TS12(L,N,M)+TSBB*SEPCOS(L)
      TS12P(L,N,M) = TS12P(L,N,M)+TSBBP*SEPCOS(L)
      WS12(L,N,M) = WS12(L,N,M)+WSBB*SEPCOS(L)
      WS12P(L,N,M) = WS12P(L,N,M)+WSBBP*SEPCOS(L)
      CONTINUE
      RETURN
      END
54
55

```

```

1      SUBROUTINE REFLK
2      C
3      C
4      C
5      C
6      C
7      C
8      C
9      C
10     C
11     C
12     C
13     C
14     C
15     C
16     C
17     C
18     C
19     C
20     C
21     C
22     C
23     C
24     C
25     C
26     C
27     C
28     C
29     C
30     C
31     C
32     C
33     C
34     C
35     C
36     C
37     C
38     C
39     C
40     C
41     C
42     C
43     C
44     C
45     C
46     C
47     C
48     C
49     C
50     C
51     C
52     C
53     C
54     C
55     C
56     C
57     C
58     C

```

REFLECT THE SYMMETRICAL MATRICES OF T AND W

COMMON/AUX/TS(10,10),WS(10,10),TB(10,10),WB(10,10),TSB(10,10),  
 WSB(10,10),TS12(8,10,10),WS12(8,10,10),TB12(8,10,10),  
 WB12(8,10,10),TSB12(8,10,10),WSB12(8,10,10),  
 TSBP(10,10),WSBP(10,10),TSB12P(9,10,10),WSB12P(8,10,10)

COMMON/OMEGA/MAX,HSOLB,HBOLB,GAMAOS,GAMA0B,NOSEPS,  
 SEPDIS(8),SEP(8),CSTRUT(8),CSTR2(8),GOSQ,PHIS,PHIB,  
 RATIOI

DO 63 M=1,MMAX  
 EM=FLOAT(M)  
 U = 2.0\*EM-1.0  
 DO 63 N=M,MMAX  
 EN=FLOAT(N)  
 FOURMN=4.0\*EN\*EN  
 UV=U\*(2.0\*EN-1.0)  
 TS(M,N) = TS(M,N)\*UV  
 TS(N,M) = TS(M,N)  
 WS(M,N) = WS(M,N)\*FOURMN  
 WS(N,M) = WS(M,N)  
 TB(M,N) = TB(M,N)\*UV  
 TB(N,M) = TB(M,N)  
 WB(M,N) = WB(M,N)\*FOURMN  
 WB(N,M) = WB(M,N)  
 TSB(M,N) = TSB(M,N)\*UV  
 TSBP(M,N) = TSBP(M,N)\*UV  
 WSB(M,N) = WSB(M,N)\*FOURMN  
 WSBP(M,N) = WSBP(M,N)\*FOURMN  
 IF (M.EQ.N) GO TO 62  
 TSB(N,M)=TSB(M,N)\*UV  
 TSBP(N,M)=TSBP(M,N)\*UV  
 WSB(N,M)=WSB(M,N)\*FOURMN  
 WSBP(N,M)=WSBP(M,N)\*FOURMN  
 CONTINUE

DO 53 L=1,NOSEPS  
 TS12(L,M,N) = TS12(L,M,N)\*UV  
 TS12(L,N,M) = TS12(L,M,N)  
 WS12(L,M,N) = WS12(L,M,N)\*FOURMN  
 WS12(L,N,M) = WS12(L,M,N)  
 TB12(L,M,N) = TB12(L,M,N)\*UV  
 TB12(L,N,M) = TB12(L,M,N)  
 WB12(L,M,N) = WB12(L,M,N)\*FOURMN  
 WB12(L,N,M) = WB12(L,M,N)  
 TSB12(L,M,N) = TSB12(L,M,N)\*UV  
 TSB12P(L,M,N) = TSB12P(L,M,N)\*UV  
 WSB12(L,M,N) = WSB12(L,M,N)\*FOURMN  
 WSB12P(L,M,N) = WSB12P(L,M,N)\*FOURMN  
 IF (M.EQ.N) GO TO 63  
 TSB12(L,N,M)=TSB12(L,M,N)\*UV  
 TSB12P(L,N,M)=TSB12P(L,M,N)\*UV  
 WSB12(L,N,M)=WSB12(L,M,N)\*FOURMN

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SUBROUTINE REFLK 74/74 OPT=0 ROUND=0/ TRACE

REFLK 59  
REFLK 60  
REFLK 61  
REFLK 62

WSB12P(L,N,M)=WSB12P(L,N,M)\*FOURMN  
CONTINUE  
RETURN  
END

63

60



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74/74 OPT=0 ROUND=0/ TRACE

SUBROUTINE BESSJ

```

1      SUBROUTINE BESSJ(X,N,VJ)
2
3      C
4      C
5      C
6      C
7      C
8      C
9      C
10     C
11     C
12     C
13     C
14     C
15     C
16     C
17     C
18     C
19     C
20     C
21     C
22     C
23     C
24     C
25     C
26     C
27     C
28     C
29     C
30     C
31     C
32     C
33     C
34     C
35     C
36     C
37     C
38     C
39     C
40     C
41     C
42     C
43     C
44     C
45     C
46     C
47     C
48     C
49     C
50     C
51     C
52     C
53     C
54     C
55     C
56     C
57     C
58     C

```

EVALUATE THE VALUES OF BESSEL FUNCTION FROM ORDER 0 TO  
ORDER N WITH ARGUMENT X

REAL J, JL, JLL, JLLL  
DIMENSION VJ(N)  
DATA PI /3.1415926535898/  
1 EPS /1.0E-30/  
2 EXPON /2.7182818284590/  
3  
4  
5  
6  
7  
8  
9  
10  
11  
12  
13  
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57  
58

DETERMINE THE MAXIMUM N = NU

D = ALOG(EPS)/X  
C = ALOG(EXPON/2.0)  
B = D-2.0-C  
ALPHA = (-B+SQRT(B\*\*2-4.0\*D\*(2.0-C)))/(2.0\*(2.0-C))  
CLN = ALOG(2.0\*PI-X)  
IF(ALPHA.LT.1.5) ALPHA = 1.5  
DO 1000 I=1,20  
ALN = ALOG(ALPHA)  
F = -(CLN+ALN)/(2.0\*X)+ALPHA\*(C-ALN)-D  
FP = -1.0/(2.0\*X\*ALPHA)+C-1.0-ALN  
DEL = F/FP  
ALPHA = ALPHA-DEL  
IF(X\*ABS(DEL) .LE. 0.01) GO TO 1100  
CONTINUE  
GO TO 8888  
1000  
1100  
CONTINUE  
GNU = ALPHA\*X  
NU = IFIX(GNU)+1  
IF(NU.LT.N+10) NU = N+10  
IF((NU/2)\*2.NE.NU) NU=NU+1  
RECURSE IN PLACE FOR M.GT.N  
SUM = 0.0  
JLLL = 0.0  
JLL = EPS  
NUM1 = NU-1  
NP = N  
IF((NP/2)\*2.EQ.NP) NP = NP-1  
DO 1200 MM = NP,NUM1,2  
W = NUM1-MM+NP  
JL = 2.0\*FLOAT(MM+2)\*JLL/X-JLLL  
J = 2.0\*FLOAT(MM+1)\*JL/X-JLL  
SUM = SUM+2.0\*JL  
JLLL = JL  
JLL = J  
JL = JL  
CONTINUE  
IF(NP.NE.N) GO TO 1300  
JL = 2.0\*FLOAT(N)\*JLL/X-JLLL  
SUM = SUM+2.0\*JL  
JLLL = JLL  
JLL = JL  
CONTINUE  
1300  
I = N+1

```

60      VJ(I) = JLL
        VJ(N) = JLL
        NP = N-1
        DO 1400 MM = 1,NP
            M = NP-MM
            K = M+1
            VJ(K) = 2.0*FLOAT(K)*VJ(M+2)/X-VJ(M+3)
            IF((M/2)*2.EQ.M) SUM = SUM+2*VJ(M+1)
1400    CONTINUE
        SUM = SUM-VJ(1)
        K = N+1
        DO 1500 M = 1,K
            VJ(M) = VJ(M)/SUM
1500    CONTINUE
        RETURN
88888   CONTINUE
        WRITE(6,100) X, ALPHA, DEL
        STOP
100     FORMAT(28H NO CONVERGENCE, X,ALPHA,DEL/3E14.7)
        END

```

```

BESSJ 59
BESSJ 60
BESSJ 61
BESSJ 62
BESSJ 63
BESSJ 64
BESSJ 65
BESSJ 66
BESSJ 67
BESSJ 68
BESSJ 69
BESSJ 70
BESSJ 71
BESSJ 72
BESSJ 73
BESSJ 74
BESSJ 75
BESSJ 76
BESSJ 77
BESSJ 78

```

```

1      SUBROUTINE PCHEB (AS, BS, AB, BB, NN, TITLE)
2      PCHEB
3      PCHEB
4      PCHEB
5      PCHEB
6      PCHEB
7      PCHEB
8      PCHEB
9      PCHEB
10     PCHEB
11     PCHEB
12     PCHEB
13     PCHEB
14     PCHEB
15     PCHEB
16     PCHEB
17     PCHEB
18     PCHEB
19     PCHEB
20     PCHEB
21     PCHEB
22     PCHEB
23     PCHEB
24     PCHEB
25     PCHEB
26     PCHEB
27     PCHEB
28     PCHEB
29     PCHEB
30     PCHEB
31     PCHEB
32     PCHEB
33     PCHEB
34     PCHEB
35     PCHEB
36     PCHEB
37     PCHEB
38     PCHEB
39     PCHEB
40     PCHEB
41     PCHEB
42     PCHEB
43     PCHEB
44     PCHEB
45     PCHEB
46     PCHEB
47     PCHEB
48     PCHEB
49     PCHEB
50     PCHEB
51     PCHEB
52     PCHEB
53     PCHEB
54     PCHEB
55     PCHEB
56     PCHEB
57     PCHEB
58     PCHEB

      PLOT BODY SECTIONAL AREA CURVE AND STRUT WATERPLANE OUTLINE CURVE
      INPUTS
      AS AND BS ARE, RESPECTIVELY, THE VECTORS OF SYMMETRIC-
      AND OF ANTISYMMETRIC-CHEBYCHEV COEFFICIENTS FOR THE STRUT.
      AB AND BB ARE, RESPECTIVELY, THE VECTORS OF SYMMETRIC-
      AND OF ANTISYMMETRIC-CHEBYCHEV COEFFICIENTS FOR THE BODY.

      NN = DIMENSION OF AS, BS, AB, BB
      MAXIMUM VALUE OF NN IS NMAX
      NMAX = 10

      INITIALIZE THE GRID GEOMETRY, THE PLOT VARIABLES AND
      THE ABSISSA VARIABLE.

      COMMON/PLOT/NFIRST,NLAST,NPOINT,XMAX,XMIN,NSCL1,NCHAR,NSCALE(4),
1      PCHAR(2)
      COMMON/XRPLQTQ/II,JJ,KK,LL,NHL,NSBH,NVL,NSBV,HCHAR,VCHAR,
1      ISX,ISY,V,H

      LOGICAL NSCL1

      DIMENSION AS(NN), BS(NN), AB(NN), BB(NN), TITLE(8)
      DIMENSION STAT(101),YS(101),YB(101),LABLE(3)

      GENERATE ORDNATE VALUES FOR STRUT AND BODY POINTS

      DO 2000 I=1, 101
        STAT(I)=2.0*(FLOAT(I-1)*.01-.5)
        THETA=ASIN(STAT(I))
        YS(I)=0.0
        YB(I)=0.0
        DO 1000 NCO=1,NN
          UM=COS(FLOAT(2*NCO-1)*THETA)
          VM=SIN(FLOAT(2*NCO)*THETA)
          YS(I)=YS(I)+AS(NCO)*UM+BS(NCO)*VM
          YB(I)=YB(I)+AB(NCO)*UM+BB(NCO)*VM
        1000 CONTINUE
      2000 CONTINUE

      DETERMINE THE MINIMUM AND MAXIMUM ORDNATE VALUES

      YMAX = -999999.0
      YMIN = +999999.0
      DO 3000 J=1,101
        IF(YMAX.LT. YB(J)) YMAX=YB(J)
        IF(YMAX.LT. YS(J)) YMAX=YS(J)
        IF(YMIN.GT. YB(J)) YMIN=YB(J)
        IF(YMIN.GT. YS(J)) YMIN=YS(J)
      3000 CONTINUE
    
```

```

C      CALL PLOT1 TO SET UP GRID SPACING AND DETERMINE THE AXIS VALUES
C
C      CALL PLOT1 (NSCALE,NHL,NSBH,NVL,NSBV,HCHAR,VCHAR)
C
C      CALL PLOT2 TO EXAMINE THE MINIMUM AND MAXIMUM VALUES OF
C      ABSCISSA AND ORDINATE AND TO ESTABLISH AN INTERNAL FORMULA
C      FOR COMPUTING THE LOCATION IN THE IMAGE REGION CORRESPONDING
C      TO THE POINT TO BE PLOTTED.
C      WHEN NSCL1=.TRUE., THE STANDARD GRID WILL NOT BE USED
C
C      CALL PLOT2 (XMAX,XMIN,YMAX,YMIN,NSCL1)
C
C      CALL PLOT3 FOR ASSIGNING AN ALPHA-CHARACTER TO EACH POINT
C      WHICH WILL BE PLOTTED.
C
C      CALL PLOT3 (PCHAR(1),STAT,YS,NFIRST,NLAST,NPOINT)
C      CALL PLOT3 (PCHAR(2),STAT,YB,NFIRST,NLAST,NPOINT)
C
C      PRINT THE HEADING OF THE PLOT
C
C      WRITE (6,9000) (TITLE(I), I=1,8)
C
C      CALL PLOT4 TO PRINT THE IMAGE OF THE COMPLETED GRAPH ON THE
C      PRINTER, INCLUDING THE VALUES OF ABSCISSA AND ORDINATE AT
C      THE GRID LINES OUTSIDE THE BOTTOM AND LEFT EDGE OF THE GRAPH
C
C      CALL PLOT4 (LABEL,NCHAR)
C
C      RETURN
C
9000 FORMAT(1H1,32X,64HBODY SECTIONAL AREA CURVE AND STRUT WATERPLANE O
1UTLINE CURVE FOR//25X,8A10)
END

```

```

1      C
      SUBROUTINE PLOT1 (NSCALE,A,B,C,D,E,F)
      SETUP SPACING AND DETERMINE THE AXIS VALUES
5      C
      INTEGER A,B,C,D
      LOGICAL V,H
      DIMENSION NSCALE(4)
10     C
      COMMON/XRPLQTQ/I,J,K,L,NHL,NSBH,NVL,NSBV,HCHAR,VCHAR,ISX,ISY,V,H
      C
      I=NSCALE(1)
      J=NSCALE(2)
      K=NSCALE(3)
      L=NSCALE(4)
      NHL=A
      NSBH=B-1
      NVL=C
      NSBV=D-1
      HCHAR=E
      VCHAR=F
      RETURN
      END
2      PLOT1
3      PLOT1
4      PLOT1
5      PLOT1
6      PLOT1
7      PLOT1
8      PLOT1
9      PLOT1
10     PLOT1
11     PLOT1
12     PLOT1
13     PLOT1
14     PLOT1
15     PLOT1
16     PLOT1
17     PLOT1
18     PLOT1
19     PLOT1
20     PLOT1
21     PLOT1
22     PLOT1
23     PLOT1
24     PLOT1
25     PLOT1

```



```

60      7 CONTINUE
        HCT=HCT+1
        IQ=IX+1
        DO 10 J=IQ,110
            LIN(J)=1L
10      CONTINUE
        ENCODE(110,9,GRAF(1,1)) (LIN(J),J=1,110)
65      2 CONTINUE
        3 CONTINUE
        XL=XMIN
        XH=XMAX
        YL=YMIN
        YH=YMAX
        XI=(XH-XL)/FLOAT(IX-1)
        YI=(YH-YL)/FLOAT(IY-1)
        XMOV=1.0-XL/XI
        YMOV=1.0-YL/YI
        V=.TRUE.
        H=.TRUE.
        RETURN
        9 FORMAT(110A1)
        END
70
75
59      PLOT2
60      PLOT2
61      PLOT2
62      PLOT2
63      PLOT2
64      PLOT2
65      PLOT2
66      PLOT2
67      PLOT2
68      PLOT2
69      PLOT2
70      PLOT2
71      PLOT2
72      PLOT2
73      PLOT2
74      PLOT2
75      PLOT2
76      PLOT2
77      PLOT2
78      PLOT2
79      PLOT2
80      PLOT2

```





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FTN 4.6+460

74/74 OPT=0 ROUND=0/ TRACE

SUBROUTINE PLOT4

```

1      SUBROUTINE PLOT4(MCHAR,NCHAR)
      C
      C      PRINT THE IMAGE OF THE COMPLETED GRAPH ON THE PRINTER.
      C      INCLUDING THE VALUES OF THE ABSCISSA AND ORDINATE AT THE
      C      GRID LINES OUTSIDE THE BOTTOM AND LEFT EDGES OF THE GRAPH
      C
      C
      C      INTEGER SA, SB, SC
      C      INTEGER CT, PDQ
      C      LOGICAL V, H
      C
      C      DIMENSION HNUM(15), MCHAR(3), LCHAR(30), VGFM(3), HLFMT(3)
      C
      C      COMMON/XRPLTQ/XL,XH,YL,YH,XI,YI,XMOV,YMOV
      C      COMMON/XRPLGT/GRAF(11,204)
      C      COMMON/XRPLTQ/I,J,K,L,NHL,NSBH,NVL,NSBV,MCHAR,VCHAR,ISX,ISY,V,H
      C
      C      SA=NSBV
      C      SC=NCHAR
      C      SB=NVL
      C      KQ=1
      C      CALL QPLOTZ5(PDQ)
      C      ENCODE(26.2,VGFM(1))J
      C      IF(NSBV.LE.0) NSBV=10
      C
      C      4 CONTINUE
      C      IF(NSBV.GT. 10) GO TO 3
      C      NSBV=NSBV+2
      C      NVL=NVL
      C      NVL=XVL/2.0+.5
      C      KQ=KQ+1
      C      GO TO 4
      C
      C      3 CONTINUE
      C      NNN=NVL-1
      C      MMM=NSBV-8
      C      ENCODE(25.5,HLFMT(1)) PDQ,L,NNN,MMM,L
      C      IF (NCHAR.NE.0) GOTO 14
      C      NCHAR=1
      C      LCHAR(1)=1L
      C      GO TO 15
      C
      C      14 CONTINUE
      C      DECODE(10,17,MCHAR(1)) (LCHAR(IJ),IJ=1,10)
      C      DECODE(10,17,MCHAR(2)) (LCHAR(IJ),IJ=11,20)
      C      DECODE(10,17,MCHAR(3)) (LCHAR(IJ),IJ=21,30)
      C
      C      15 CONTINUE
      C      NCT=0
      C      NSPC=(ISY-NCHAR)/2
      C      LCT=0
      C      CT=NSBH
      C      DO 6 MMX=1,ISV
      C      N=ISY-MMX+1
      C      IF (MMX.LE.NSPC.OR.LCT.GE.NCHAR) GO TO 7
      C      LCT=LCT+1
      C      LCR=LCHAR(LCT)
      C      GO TO 8
      C
      C      7 CONTINUE
      C      LCR=1L
      C
      C      8 CONTINUE

```

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FTN 4.6+460

SUBROUTINE PLOT4 74/74 OPT=0 RCUND=0/ TRACE

```

60      IF (CT.EQ.NSBM.AND.H) GO TO 9
        PRINT 1,LCR,(GRAF(II,N),II=1,11)
        GO TO 13
9      CONTINUE
        CT=-1
        ONN=(YH-MCT*YI)*10.**I
        PRINT VGFMT,LCR,ONN,(GRAF(II,N),II=1,11)
65      MCT=MCT+NSBH+1
        CONTINUE
        CT=CT+1
6      CONTINUE
        MCT=0
        IF (.NOT.V) GO TO 12
        DO 10 N=1,NVL
            HNUM(N)=(XL+MCT*XI)*10.**K
            MCT=MCT+NSBV+KQ
10      CONTINUE
        PRINT 11
        PRINT HLFMT,(HNUM(N),N=1,NVL)
12      CONTINUE
        NSBV=SA
        NVL=SB
        NCHAR=SC
        RETURN
        1  FORMAT(1H,A1,16X,11A10)
        2  FORMAT(15H(1H ,A1,3X,F10.,11,10H,3X,11A10))
        5  FORMAT(1H( ,12,6HX,F10.,11,1H, ,12,1H( ,12,6HX,F10.,11,2H)))
11      FORMAT(1H0)
17      FORMAT(10A1)
        END

```

```

1      SUBROUTINE QPLOT25(PDQ)
      C
      INTEGER A,B,C,D,PDQ
      LOGICAL V,M
      COMMON/XRPLDTF/XL,XH,YL,YH,XI,YI,XM,YM
      COMMON/XRPLDTQ/II,JJ,KK,LL,A,B,C,D,E,F,M,N,V,H
      C
      X=ABS(XL)
      IF(X.LT.AH) X=XH
      K=0
      DO 1 I=1,11
        XU=10** (I-1)
        IF(X.GT.XU) GOTO 2
        K=K+1
      1 CONTINUE
      2 CONTINUE
      PDQ=1
      IF(LL.EQ.0) PDQ=0
      QDQ=PDQ+KK+LL+K
      PDQ=14.0-(10.0-QDQ)/2.0
      RETURN
      END
20

```

```

QPLOT 2
QPLOT 3
QPLOT 4
QPLOT 5
QPLOT 6
QPLOT 7
QPLOT 8
QPLOT 9
QPLOT 10
QPLOT 11
QPLOT 12
QPLOT 13
QPLOT 14
QPLOT 15
QPLOT 16
QPLOT 17
QPLOT 18
QPLOT 19
QPLOT 20
QPLOT 21
QPLOT 22
QPLOT 23
QPLOT 24

```

```

1      SUBROUTINE CHEB (AMC,BMC,MMAX)
2      C
3      C INPUT STRUT OR BODY DATA. COMPUTE CHEBYCHEV COEFFICIENTS
4      C CHECK THE ACCURACY OF CHEBYCHEV APPROXIMATION.
5      C
6      C DIMENSION AMC(10), BMC(10)
7      C
8      C COMMON/NAME/INCHAR(8),NAME(7)
9      C
10     C COMMON/OFFSET/X(100),Y(100),D(100),THETA(100),N,NV(10),NNV
11     C LOGICAL ISBODY
12     C
13     C READ INPUT OFFSET DATA
14     C
15     C READ (5,31) INCHAR
16     C IF (INCHAR(1).EQ.5)STRUT) ISBODY=.FALSE.
17     C IF (INCHAR(1).EQ. 4)BODY) ISBODY=.TRUE.
18     C
19     C CALL READ
20     C
21     C COMPUTE SCALING FACTOR
22     C
23     C CALL SCALE(ISBODY)
24     C
25     C COMPUTE CHEBYCHEV COEFFICIENTS
26     C
27     C CALL COMPUT (AMC,BMC,MMAX,ISBODY)
28     C
29     C CHECK INPUT OFFSET AGAINST OFFSET OBTAINED BY EVALUATING
30     C THE CHEBYCHEV SERIES
31     C
32     C CALL CHECK (AMC,BMC,MMAX,ISBODY)
33     C
34     C COMPUTE WETTED SURFACE AREA
35     C
36     C CALL SURFACE (AMC,BMC,MMAX,ISBODY)
37     C
38     C CHECK NUMBER OF OFFSET INPUT CARDS
39     C
40     C READ (5,32) NINPUT
41     C NINPUT = NINPUT + NNV - 1
42     C IF (NINPUT.EQ.N) GO TO 999
43     C
44     C ERROR IN INPUT CARDS
45     C
46     C ARITE (6,200) INCHAR
47     C STOP
48     C 999 CONTINUE
49     C RETURN
50     C
51     C 31 FORMAT (3A10)
52     C 32 FORMAT (1I3)
53     C 200 FORMAT (' ERROR IN INPUT DATA CARDS ----,8A10)
54     C
55     C END
56     C
57     C
58     C

```

```

1      SUBROUTINE WTSURFB (AMC,BMC,MMAX)
      C
      C      DETERMINE THE SURFACE AREA OF A BODY OF
      C      REVOLUTION GIVEN BY CHEBYCHEV COEFFICIENTS
      C
      C      DIMENSION AMC(10),BMC(10)
      C
      C      COMMON/OUT/HS,HB,XLS,XLB,TSMAX,AX,PI,G,RHO,GNU,WETS,WETB,WTSURF,
      C      VMFPS,DELFCF,TITLE(B),SPACE
      C
      C      RAD=SQRT(AX/PI)
      C      CON=(2.0*RAD/XLB)**2
      C      DX=0.05
      C      DXSO=DX*DX
      C      R=0.0
      C      WETB=0.0
      C      DO 10 I=1,40
      C      RL=R
      C      X=DX*FLOAT(I)-1.0
      C      CALL EVAL (X,MMAX,R,AMC,BMC)
      C      IF (R.LT.0.0) R=0.0
      C      R=SQRT(R)
      C      RM=(PL+R)*0.5
      C      DR=R-RL
      C      WETB=WETB+RM*SQRT(DXSO*CON*DR**2)
      C
      C      10 CONTINUE
      C      WETB=PI*RAD*XLB*WETB
      C      RETURN
      C      END

```

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SUBROUTINE WTSURFS 74,74 OPT=0 ROUND=\*/ TRACE

```

1      SUBROUTINE WTSURFS (AMC,BMC,MMAX)
      C
      C      DETERMINE THE SURFACE AREA OF A STRUT WHOSE THICKNESS
      C      DISTRIBUTION IS GIVEN BY CHEBYCHEV COEFFICIENTS
      C
5      DIMENSION AMC(10),BMC(10)
      COMMON/OUT/HS,HB,XLS,XLB,TSMAX,AX,PI,G,RHO,GNU,WETS,WETB,WTSURF,
      C      VMFPS,DELCP,TITLE(8),SPACE
10     CON=(TSMAX/XLS)**2
      DX=0.05
      DXSQ=DX*DX
      WETS=0.0
      T=0.0
      DO 10 I=1,40
      TL=T
      X=DX*FLOAT(I)-1.0
      CALL EVAL (X,MMAX,T,AMC,BMC)
      DT=T-TL
      WETS=WETS+SQRT(DXSQ+CON*DT**2)
10    CONTINUE
      WETS = WETS - SPACE * 2.0
      WETS=XLS*HS*WETS
      RETURN
      END
25
26

```

```

1  SUBROUTINE READ
C
C  READ OFFSET DATA OF STRUT OR BODY AND CHECK FOR ERROR
C
5  COMMON/OFFSET/X(100),Y(100),D(100),THETA(100),N,NV(10),NNV
COMMON/NORM/YMAX,XDIVER,YDIVER,XADDER
LOGICAL REPEAT
YMAX = 0.
DO 47 I = 2,8
NAME(I-1) = INCHAR(I)
REPEAT = .FALSE.
NNV = 1
DO 40 I = 1,100
N=I
N = NUMBER OF INPUT POINTS
IF (REPEAT) GO TO 339
READ(5,12) X(I),Y(I), IEND
IF (I.EQ.1) GO TO 39
IF (I.GT.2) GO TO 38
SIGN = X(I) - XLAST
IF (SIGN.EQ.0.) GO TO 45
GO TO 39
IF ((X(I)-XLAST)-SIGN .LE. 0.) GO TO 45
XLAST = X(I)
IF (Y(I).GT.YMAX) YMAX = Y(I)
IF (IEND.EQ.5H END) GO TO 42
IF (IEND.NE.5HBREAK) GO TO 40
REPEAT = .TRUE.
NV(NNV) = I
NNV = NNV + 1
GO TO 40
339 X(I) = X(I-1)
Y(I) = Y(I-1)
REPEAT = .FALSE.
40 CONTINUE
WRITE(6,18) NAME
STOP
42 CONTINUE
NV(NNV) = N
GO TO 8
45 CONTINUE
PRINT 46, X(I),Y(I) ,NAME
STOP
8 CONTINUE
RETURN
12 FORMAT (2F10.0, 55X, A5)
18 FORMAT (* TOO MANY INPUT CARDS FOR *,7A10)
46 FORMAT (* CARD OUT OF ORDER *,2E16.8/20X,=FOR-- *,7A10)
END

```

2 READ  
 3 READ  
 4 READ  
 5 READ  
 6 READ  
 7 READ  
 8 READ  
 9 READ  
 10 READ  
 11 READ  
 12 READ  
 13 READ  
 14 READ  
 15 READ  
 16 READ  
 17 READ  
 18 READ  
 19 READ  
 20 READ  
 21 READ  
 22 READ  
 23 READ  
 24 READ  
 25 READ  
 26 READ  
 27 READ  
 28 READ  
 29 READ  
 30 READ  
 31 READ  
 32 READ  
 33 READ  
 34 READ  
 35 READ  
 36 READ  
 37 READ  
 38 READ  
 39 READ  
 40 READ  
 41 READ  
 42 READ  
 43 READ  
 44 READ  
 45 READ  
 46 READ  
 47 READ  
 48 READ  
 49 READ  
 50 READ  
 51 READ  
 52 READ  
 53 READ

```

1      SUBROUTINE SCALE (ISBODY)
2      C
3      C
4      C
5      C
6      C
7      C
8      C
9      C
10     C
11     C
12     C
13     C
14     C
15     C
16     C
17     C
18     C
19     C
20     C
21     C
22     C
23     C
24     C
25     C
26     C
27     C
28     C
29     C
30     C
31     C
32     C
33     C
34     C
35     C
36     C
37     C
38     C
39     C

      COMPUTE SCALING FACTORS AND SCALE THE INPUT FOR LENGTH
      BETWEEN -1.0 AND +1.0 AND MAXIMUM BEAM OR SECTIONAL
      AREA OF 1.0

      COMMON/OFFSET/X(100),Y(100),D(100),THETA(100),N,NV(10),NNV
      COMMON/NAME/INCHAR(8),NAME(7)
      COMMON/NORM/YMAX,XDIVER,YDIVER,XADDER
      LOGICAL ISBODY

      YDIVER = YMAX
      XDIVER = (X(N)-X(1))*0.5
      XADDER = -1. - X(1) / XDIVER
      IF (ISBODY) WRITE (6,17)
      IF (.NOT. ISBODY) WRITE (6,18)
      WRITE(6,19) NAME
      WRITE(6,25)
      WRITE(6,26) (X(I),Y(I),I=1,N)

      IF *YDIVER* IS NOT ZERO, THE Y INPUTS WILL BE DIVIDED BY *YDIVER*
      .... SAME FOR *XDIVER* .....
      THEN *XADDER* IS ADDED TO X INPUTS
      THEN IF *ISBODY*, THE Y INPUTS WILL BE SQUARED

      WRITE(6,206) XDIVER,XADDER,YDIVER
      IF(ISBODY) WRITE(6,207)
      RETURN

17  FORMAT ('H1,* INPUT OFFSET DATA OF BODY *')
18  FORMAT ('H1,* INPUT OFFSET DATA OF STRUT *')
19  FORMAT ('H0.7A10,/')
25  FORMAT ('7X,*X-VALUES=,10X,*Y-VALUES=,10X,*BEFORE SCALING=//')
26  FORMAT ('2I6X,F10.5')
35  FORMAT ('=0 SCALING=--*/' * X VALUES ARE DIVIDED BY *.E16.8,
1      *, THEN ADD *.E16.8 / * Y VALUES ARE DIVIDED BY *.E16.8)
207  FORMAT ('15X,*AND SQUARED*')
      END

```



```

1      SUBROUTINE COMPUT (AMC,BMC,MMAX,ISBODY)
      C
      C      COMPUTE THE COEFFICIENTS OF THE CHEBYCHEV POLYNOMIALS
      C
5      DIMENSION AMC(10),BMC(10)
      COMMON/OFFSET/X(100),Y(100),D(100),THETA(100),N,NV(10),NNV
      COMMON/NAME/INCHAR(8),NAME(7)
      COMMON/NORM/YMAX,XDIVER,YDIVER,XADDER
      LOGICAL ISBODY
10     C
      DO 100 I=1,N
        Y(I) = Y(I) / YDIVER
        IF (ISBODY) Y(I) = Y(I)**2
        XWAS = X(I)
        X(I) = X(I)/XDIVER + XADDER
        IF (ABS(X(I)) .LE. 1.) GO TO 90
        IF (ABS(X(I)) .GT. 1.01) GO TO 90
        WRITE(6,201) X(I),XWAS
        X(I) = AINT(X(I))
        THETA(I) = ASIN(X(I))
90      CONTINUE
100     IF (ISBODY) WRITE (6,13)
        IF (.NOT.ISBODY) WRITE (6,14)
        WRITE(6,19) NAME
        WRITE(6,15)
        WRITE(6,16) (X(I),Y(I),THETA(I),I=1,N)
      C
      C      COMPUTE FOLLOWS
      C
30     CALL CHEV (AMC,BMC,MMAX,ISBODY)
      C
      RETURN
13     FORMAT(1H1,*, NORMALIZED OFFSET DATA FOR BODY *)
14     FORMAT(1H1,*, NORMALIZED OFFSET DATA FOR STRUT *)
15     FORMAT (7X,*X-VALUES*,10X,*Y-VALUES*,10X,* THETA *//)
16     FORMAT (3(6X,F10.5))
19     FORMAT(1H0,7A10,/)
201    FORMAT (*TRUNCATED X= *,2E16.8)
      END

```

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FTN 4.6+460

SUBROUTINE SURFACE 74/74 OPT=0 ROUND=\*/ TRACE

```

1      SUBROUTINE SURFACE (AMC,BMC,MMAX,ISBODY)
      C
      C      FIND THE WETTED SURFACE AREA OF STRUT OR BODY. ALSO THE
      C      WATER PLANE AREA OF STRUT AND DISPLACED VOLUME OF BODY
      C
5      DIMENSION AMC(10),BMC(10)
      COMMON/OUT/HS,HB,XLS,XLB,TSMAX,AX,PI,G,RHO,GNU,WETS,WETB,WTSURF,
1      VMFPS,DELCF,TITLE(8),SPACE
      COMMON/NAME/INCHAR(8),NAME(7)
      LOGICAL ISBODY
      DATA PI / 3.1415926535897 /

10     IF (ISBODY) GO TO 100

      C      COMPUTE WETTED SURFACE AREA OF STRUT
15     CALL WTSURFS (AMC,BMC,MMAX)

      C      COMPUTE WATER PLANE AREA OF STRUT
20     WPA = XLS * TSMAX * AMC(1) * PI / 4.0
      WRITE (6,110) WETS,XLS,TSMAX,WPA
      GOTO 999
100    CONTINUE

      C      COMPUTE WETTED SURFACE AREA OF BODY
25     CALL WTSURFB (AMC,BMC,MMAX)
      WETB = WETB - WPA

      C      COMPUTE DISPLACED VOLUME
30     DISPVOL=XLB*AX*PI/4.0*MC(1)
      WRITE (6,120) WETB,XLB,AX,DISPVOL
      RETURN
35     999 CONTINUE

110    FORMAT (1H0,'WETTED SURFACE AREA OF STRUT IS ',E16.8,
1      ' WHERE STRUT LENGTH IS ',E16.8,
2      ' AND MAXIMUM THICKNESS IS ',E16.8,
3      '/.20X,'WATER PLANE AREA IS ',E16.8)

120    FORMAT(1H0,'WETTED SURFACE AREA OF BODY IS ',E16.8,
1      ' WHERE BODY LENGTH IS ',E16.8,
2      ' AND MAXIMUM AREA IS ',E16.8/
3      20X,' BODY VOLUME IS ',E16.8)
45     END

```

```

1      SUBROUTINE CHEV (AMC,BMC,MMAX,ISBODY)
      C
      C      THIS PROGRAM USES THE OFFSETS TO COMPUTE CHEBYCHEV
      C      COEFFICIENTS VIA SPLINE APPROXIMATION
      C
5      DIMENSION AMC(10),BMC(10)
      COMMON/OFFSET/X(100),Y(100),D(100),THETA(100),N,NV(10),NNV
      COMMON/NAME/INCHAR(8),NAME(7)
      LOGICAL ISBODY
      DATA PI / 3.1415926535897 /
10     C
      C      OBTAIN CURVE FIT OF OFFSETS
      C
      C
      C      ISTART = 1
      C      DO 50 I = 1,NNV
      C      NN = NV(I)
      C      NPTS = NN-ISTART+1
      C      CALL SPLINE(THETA(ISTART),Y(ISTART),D(ISTART),NPTS,BC,1,1,ISBODY)
      C      ISTART = NN + 1
      C      N = NV(NNV)
50     C
      C      AMC AND BMC ARE THE COEFFICIENTS THAT ARE CALCULATED AND STORED
      C
      C      MAIN CALCULATION FOLLOWS
      C
      C      DO 15 J = 1,MMAX
      C      AJ=FLOAT(J)
      C      ARCU = (2.0-AJ-1.0)
      C      ARCV = 2.0-AJ
      C      AMC(J) = SUMSPL(THETA,Y,D,N,ARCU,-1)
      C      BMC(J) = SUMSPL(THETA,Y,D,N,ARCV,+1)
      C      AMC(J)=AMC(J)*2.0/PI
      C      BMC(J) = BMC(J) * 2.0/PI
15     C
      C      CALCULATIONS COMPLETE-PRINT COEFFICIENTS OUT
      C
      C
      C      IF(ISBODY) WRITE (6,22)
      C      IF(.NOT.ISBODY) WRITE (6,23)
      C      WRITE(6,24) NAME
      C      WRITE(6,25) MMAX
      C      WRITE(6,202) (X(I),I=1,N)
      C      WRITE(6,203) (AMC(I),I=1,MMAX)
      C      WRITE(6,204) (BMC(I),I=1,MMAX)
      C      AREA = AMC(1) * PI / 4.0
      C      IF (ISBODY) GO TO 800
      C      WRITE(6,650) AREA
      C      RETURN
      C      WRITE(6,850) AREA
      C      RETURN
800    C
      C      23 FORMAT (1H1,* CHEBYCHEV COEFFICIENTS OF BODY *)
      C      24 FORMAT (1H1,* CHEBYCHEV COEFFICIENTS OF STRUT *)
      C      25 FORMAT (1H0,7A10)
      C      200 FORMAT (1H0,9X,*MMAX = *,14//)
      C      201 FORMAT (5E16.8)
      C      202 FORMAT (7A10)
      C      203 FORMAT (///10X,*X ARRAY "/ (8E16.8))
      C      204 FORMAT (///10X,* AMC ARRAY "/ (8E16.8))

```

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FTN 4.6+460

74/74 OPT=0 ROUND=0/ TRACE

SUBROUTINE CHEV

```

204  FORMAT (//10X," BMC ARRAY  "/ (8E16.8))
650  FORMAT ("AREA COEFFICIENT = AREA/(LSTRUT-TMAX) = ",E16.8)
850  FORMAT ("OVOLUME COEFFICIENT = VOLUME/(LBODY*AMAX) = ",E16.8)
END

```

```

CHEV
CHEV
CHEV
CHEV

```

```

59
60
61
62

```

60

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FTN 4.6+460

74/74 OPT=0 ROUND=0/ TRACE

SUBROUTINE CHECK

```

1      SUBROUTINE CHECK (AMC,BMC,MMAX,ISBODY)
      C
      C      THIS SUBROUTINE CHECKS THE DIFFERENCE BETWEEN APPROXIMATED
      C      OFFSETS AND ORIGINAL OFFSETS
      C
5     DIMENSION AMC(10),BMC(10)
      COMMON/OFFSET/X(100),Y(100),D(100),THETA(100),N,NV(10),NNV
      COMMON/NAME/INCHAR(8),NAME(7)
      LOGICAL ISBODY
      C
10     N = NUMBER OF ORIGINAL OFFSETS GIVEN
      C
      C      MMAX = MAX ORDER OF CHEBYCHEV EXPANSION USED
      C
      C      IF (ISBODY) WRITE (6,121)
      C      IF (.NOT.ISBODY) WRITE (6,122)
15     123 WRITE(6,126) MMAX,NAME
      WRITE(6,200)
      DO 100 I = 1,N
      C
      C      CALL EVAL(X(I),MMAX,YX,AMC,BMC)
      C
20     IF (I.EQ.N) GO TO 10
      XX = (X(I) + X(I+1)) * .5
      C
      C      CALL EVAL (XX,MMAX,YXX,AMC,BMC)
      C
25     WRITE(6,201) (Y(I),X(I),YX,XX,YXX)
      GO TO 100
100    CONTINUE
      RETURN
30     121 FORMAT(1H1," CHECK OFFSET OF BODY USING CHEBYCHEV APPROXIMATION")
      122 FORMAT(1H1," CHECK OFFSET OF STRUT USING CHEBYCHEV APPROXIMATION")
      126 FORMAT (1H0,"CHECK OUT PUT,MMAX=,15=,FOR=.7A10./)
200    FORMAT ('0=,5X,-REAL Y=,12X,-X=,12X,-APPROX Y=,27X,*XX=,10X,
      1      *APPROX Y(XX)=,/)
201    FORMAT (1X,3E16.8,16X,2E16.8)
      END
35

```



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TRACE

OPT=0

ROUND=

74,74

SUBROUTINE SPLINE

```

1      SUBROUTINE SPLINE (X,Y,D,N,BC,KODE,KKODE,ISBODY)
2      THIS SUBROUTINE FITS SMOOTH SPLINE SEGMENTS THROUGH A GIVEN SET
3      OF DISCRETE DATA POINTS
4      DIMENSION X(N),Y(N),D(N)
5      DIMENSION A(100),B(100),C(100),BC(8)
6      LOGICAL ISBODY
7
8      X ARRAY CONTAINS ABSCISSAS FOR INPUT DATA
9      Y ARRAY CONTAINS ORDINATES FOR INPUT DATA
10     ARRAYS A,B,C ARE MAINLY SUB DIAG., DIAGONAL, AND SUPER DIAG.
11     D ARRAY IS THE RIGHT HAND SIDE OF MATRIX EQUATION
12     FINAL ANSWERS ARE PLACED IN D
13
14     SOLUTION TECHNIQUE IS GAUSSIAN ELIMINATION
15     ARRAY BC CONTAINS SPECIFIED BOUNDARY CONDITIONS
16
17     KODE = 0 USER IS SPECIFYING BOUNDARY CONDITIONS
18     KODE = 1 USER IS TAKING AN EXTRAPOLATION OF SECOND
19     DERIVATIVES AS THE BOUNDARY CONDITION
20     KKODE = 0 NO PRINT OUT FROM SPLINE ROUTINE
21     KKODE = 1 SPLINE PRINTS ABSCISSAS,ORDINATES AND SECOND DERIVATIVE
22
23     IF (N.GT.2) GO TO 25
24     D(1) = 0.
25     D(2) = 0.
26     NPRINT = 2
27     GO TO 20
28
29     IF (N.GT.3) GO TO 50
30     YDD = 2.*((X(3)-X(2))*Y(1)+(X(2)-X(1))*Y(3)-(X(3)-X(1))*Y(2))
31     / ((X(3)-X(2))*(X(2)-X(1))-(X(3)-X(1)))
32     D(1) = YDD
33     D(2) = YDD
34     D(3) = YDD
35     NPRINT = 3
36     GO TO 20
37
38     NPRINT = 0
39     II = 1
40     NL1 = N-1
41     NL2 = N-2
42     DO 12 I = 1,N
43     A(I) = 0.
44     B(I) = 0.
45     C(I) = 0.
46     D(I) = 0.
47
48     SET UP MATRICES(A TRIAGONAL STRUCTURE)
49
50     A(1) = (X(3)-X(2))/(X(3)-X(1))
51     C(1) = 2.0
52     B(1) = 1.0 - A(1)
53     D(1) = 6.0*((Y(3)-Y(2))/(X(3)-X(2))-(Y(2)-Y(1))/(
54     (X(2)-X(1)))/(X(3)-X(1))
55     H = X(3) - X(2)
56     DO 19 J=3,NL1
57     HP = X(J+1) - X(J)
58     C(J) = HP/(H+HP)

```

```

60      B(J) = 2.0
        A(J) = 1.0 - C(J)
        D(J) = 6.0*((Y(J+1)-Y(J))/HP-(Y(J)-Y(J-1))/H)/(HP+H)
        H = HP
        19
        C
        C
        C
        65      CHECK BOUNDARY CONDITIONS
        IF (KODE .EQ. 1) GO TO 6
        IF (BC(2) .EQ. 0.0 .AND. BC(3) .EQ. 0.0) GO TO 1
        GO TO 2
        1      WRITE(6,300) BC(2),BC(3)
        GO TO 6
        2      C(2) = 0.0
        A(2) = BC(3)-BC(2)*(X(2)-X(1))/3.0
        B(2) = -BC(2) - (X(2)-X(1))/6.0
        D(2) = BC(4)-BC(1)*Y(1)-BC(2)*(Y(2)-Y(1))/(X(2)-X(1))
        3      IF (BC(6) .EQ. 0.0 .AND. BC(7) .EQ. 0.0) GO TO 4
        GO TO 5
        4      WRITE(6,301) BC(6),BC(7)
        GO TO 7
        5      C(N) = 0.0
        A(N) = BC(6)*(X(N)-X(N-1))/6.0
        B(N) = BC(6)*(X(N)-X(N-1))/3.0+BC(7)
        D(N) = BC(8)-BC(5)*Y(N)-BC(6)*(Y(N)-Y(N-1))/(X(N)-X(N-1))
        GO TO 10
        6      C(2) = (X(2)-X(1))/(X(3)-X(2))
        A(2) = 1.0
        B(2) = -1.0-C(2)
        D(2) = 0.0
        7      IF (KODE .EQ. 0) GO TO 3
        C(N) = (X(N)-X(N-1))/(X(N-1)-X(N-2))
        A(N) = -1.0 - C(N)
        B(N) = 1.0
        D(N) = 0.0
        C
        C
        C
        95      SOLVE EQUATIONS
        C(2) = - A(2)*A(1)/B(1) + C(2)
        DO 13 I=1,NL2
        AUGM = ABS(B(I))
        IF (AUGM .LT. 1.0E-06) GO TO 9
        CONST = A(I+1)/B(I)
        B(I+1) = B(I+1) - CONST*C(I)
        D(I+1) = D(I+1) - CONST*D(I)
        IF (I .NE. NL2) GO TO 13
        A(N) = A(N) - C(N)*C(I) / B(I)
        D(N) = D(N) - C(N)*D(I) / B(I)
        GO TO 13
        9      II = I+1
        D(I) = D(I)/C(I)
        D(I+1) = D(I+1) - B(I+1)*D(I)
        B(I+1) = A(I+1)
        A(I+1) = 0.0
        D(I+2) = D(I+2) - A(I+2)*D(I)
        A(I+2) = 0.0
        IF (I .NE. NL2) GO TO 13
        A(N) = C(N)
        110
        105
        115

```



```

115      13      CONTINUE
      DET = B(N-1)*B(N) - C(N-1)*A(N)
      STORE = D(N)
      D(N) = (B(N-1)*D(N) - D(N-1)*A(N))/DET
      C(N-1) = (D(N-1)*B(N) - C(N-1)*STORE)/DET
      IP = 0
      DO 15 I = 2, NL2
      JI = N-I
      IF (JI .EQ. IP) GO TO 15
      IF (JI .EQ. II) GO TO 8
      D(JI) = (D(JI)-C(JI)*D(JI+1))/B(JI)
      GO TO 15
      8      IP = JI-1
      STORE = D(JI)
      D(JI) = D(JI-1)
      D(JI-1) = (STORE - C(JI-1)*D(JI+1))/B(JI-1)
      15      CONTINUE
      D(1) = (D(1) - A(1)*D(3) - C(1)*D(2))/B(1)
      C
      C
      C      ALL DONE
      20      IF (KKODE .NE. 1) GO TO 1000
      IF (ISBODY) WRITE(6,100) (I,X(I),Y(I),D(I),I=1,N)
      IF (.NOT.ISBCDY) WRITE(6,101) (I,X(I),Y(I),D(I),I=1,N)
      IF (NPRINT.EQ.3) WRITE(6,901)
      IF (NPRINT.EQ.2) WRITE(6,902)
      1000      RETURN
      100      FORMAT (1H1,
      1          3CX,"SPLINE APPROXIMATION OF BODY",//27X,
      2          *ABSCISSA
      3          (12X,110.3E16.8))
      101      FORMAT (1H1,3CX,"SPLINE APPROXIMATION OF STRUT",//27X,
      1          *ABSCISSA
      2          (12X,110.3E16.8))
      300      FORMAT(//,"THE BOUNDARY CONDITIONS SPECIFIED AT THE FIRST POINT
      1      ARE NOT SUFFICIENT", BC(2) = ".E16.8/" BC(3)=".E16.8/" THE
      2      PROGRAM WILL CONTINUE WITH THE SECOND DERIVATIVE AT THE FIRST
      3      POINT EQUAL TO A LINEAR COMBINATION OF THE SECOND AND THIRD"//)
      301      FORMAT(//,"THE BOUNDARY CONDITIONS SPECIFIED AT THE LAST POINT
      1      ARE NOT SUFFICIENT", BC(6)=".E16.8/" BC(7)=".E16.8/"
      2      " THE PROGRAM WILL CONTINUE WITH THE SECOND DERIVATIVE AT THE LAST
      3      POINT EQUAL TO A LINEAR COMBINATION OF THE THIRD AND SECOND
      4      LAST")
      901      FORMAT (*0THREE POINT SPLINE, INTERPOLATION IS QUADRATIC*)
      902      FORMAT (*0TWO POINT SPLINE, INTERPOLATION IS LINEAR*)
      END

```

```

1      REAL FUNCTION SUMSPL(X,Y,S,N,AK,KODE)
2
3      THIS PROGRAM USES THE SPLINE COEFFICIENTS AND INTEGRATES THE
4      TRIGONOMETRIC INTEGRALS
5      OF THE FORM  $\int \sin(AK \cdot X)$  OR  $\int \cos(AK \cdot X)$ 
6      IF KODE = +1 PROGRAM PERFORMS SINE INTEGRATION
7      IF KODE = -1 PROGRAM PERFORMS COSINE INTEGRATION
8      INPUT DATA ARE GIVEN AS  $(Y(I) = F(X(I)), I=1,N)$ 
9      N IS THE TOTAL NUMBER OF INPUT POINTS (ABSCISSAS)
10     S-ARRAY STORES THE SECOND DERIVATIVES OF THE SPLINE FUNCTIONS
11     THE RANGE OF INTEGRATION IS FROM X(1) TO X(N)
12
13     DIMENSION X(100),Y(100),S(100)
14     NL = N-1
15     SUMSPL = 0.0
16     D2 = AK*AK
17     D3 = AK*D2
18     D4 = AK*D3
19     DO 1 I=1,NL
20       H = X(I+1) - X(I)
21       IF (H) 1,1,9
22       ZAA = (S(I+1)-S(I))/(E*H)
23       ZBB = S(I)/2.0
24       ZCC = (Y(I+1)-Y(I))/H - H*(S(I+1)+2.0*S(I))/6.
25       E = SIN(AK*H)
26       F = COS(AK*H)
27       AA1 = (3.*D2*H*H-6.)*F/D4+(D2*H*H*H-6.*H)*E/D3+6./D4
28       AA2 = 3.*H*H*E/D2-6.*E/D4-H*H*H*F/AK+6.*H*F/D3
29       BB1 = 2.*H*F/D2-2.*E/D3+H*H*E/AK
30       BB2 = 2.*H*E/D2+2.*F/D3-H*H*F/AK-2./D3
31       CC1 = F/D2 + H*E/AK -1.0/D2
32       CC2 = E/D2 -H*F/AK
33       DD1 = E/AK
34       DD2 = -F/AK+1.0/AK
35       UU = SIN(AK*X(I))
36       VV = COS(AK*X(I))
37       IF (KODE)2,3,4
38       SUMSPL = SUMSPL + VV*(AA1*ZAA+BB1*ZBB+CC1*ZCC+DD1*Y(I))
39       1 - UU*(AA2*ZAA+BB2*ZBB+CC2*ZCC+DD2*Y(I))
40       GO TO 1
41       SUMSPL = SUMSPL + UU*(AA1*ZAA+BB1*ZBB+CC1*ZCC+DD1*Y(I)) +
42       1 VV*(AA2*ZAA + BB2*ZBB + CC2*ZCC+DD2*Y(I))
43       1 CONTINUE
44       GO TO 5
45       WRITE(6,100)
46       SUMSPL = 1.0
47       RETURN
48       100 FORMAT (1H1,"KODE = 0"/)" SUMSPL IS SET EQUAL TO 1."
49       END
50

```

SUMSPL 2  
SUMSPL 3  
SUMSPL 4  
SUMSPL 5  
SUMSPL 6  
SUMSPL 7  
SUMSPL 8  
SUMSPL 9  
SUMSPL 10  
SUMSPL 11  
SUMSPL 12  
SUMSPL 13  
SUMSPL 14  
SUMSPL 15  
SUMSPL 16  
SUMSPL 17  
SUMSPL 18  
SUMSPL 19  
SUMSPL 20  
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SUMSPL 40  
SUMSPL 41  
SUMSPL 42  
SUMSPL 43  
SUMSPL 44  
SUMSPL 45  
SUMSPL 46  
SUMSPL 47  
SUMSPL 48  
SUMSPL 49  
SUMSPL 50

```

1      C
2      C
3      C
4      C
5      SUBROUTINE SPLFIT(X,Y,S,N,T,YVAL,YD,YDD)
6      FIND THE DERIVATIVES (1ST AND 2ND) OF THE SPLINE FITTED DATA
7      DIMENSION X(100),Y(100),S(100)
8      I = 1
9      IF (T-X(I)) 6,6,4
10     I = I + 1
11     GO TO 3
12     I = I - 1
13     IF (I.EQ.0) I=1
14     H = X(I+1) - X(I)
15     HTX = X(I+1) - T
16     HTT = T - X(I)
17     YVAL = S(I) + (HTX**3)/(6.*H)+S(I+1)*HTT**3/(6.*H)
18     YD = -S(I)*HTX*HTX/(2.*H)+S(I+1)*HTT*HTT/(2.*H)
19     YDD = S(I) *HTX/H+S(I+1)*HTT/H
20     RETURN
21     END
22
SPLFIT 2
SPLFIT 3
SPLFIT 4
SPLFIT 5
SPLFIT 6
SPLFIT 7
SPLFIT 8
SPLFIT 9
SPLFIT 10
SPLFIT 11
SPLFIT 12
SPLFIT 13
SPLFIT 14
SPLFIT 15
SPLFIT 16
SPLFIT 17
SPLFIT 18
SPLFIT 19
SPLFIT 20
SPLFIT 21
SPLFIT 22

```

2 FORMDR  
3 FORMDR  
4 FORMDR  
5 FORMDR  
6 FORMDR  
7 FORMDR  
8 FORMDR  
9 FORMDR  
10 FORMDR  
11 FORMDR  
12 FORMDR  
13 FORMDR  
14 FORMDR

```

1      C
      C
      C
      FUNCTION FORMDR(VL)
      EVALUATE FORM DRAG COEFFICIENT
      DIMENSION X(9), Y(9)
      DATA X / 1.325, 1.38, 1.43, 1.48, 1.55, 1.68, 1.9, 2.2, 2.5 /
      DATA Y / .51, .71, .84, .85, .83, .75, .65, .57, .50 /
      IF (VL-GE.1.325.AND.VL.LT.2.5) GO TO 4
      FORMDR=0.5
      GO TO 5
      4 FORMDR = YINTP (VL,X,Y,9)
      5 RETURN
      END
10

```

```

1      FUNCTION YINTP (XA,X,Y,N)
      C
      C
      C      INTERPOLATING FROM A SET OF DATA (X,Y)
5      DIMENSION X(1), Y(1)
      DO 10 I=1,N
      IF (X(I)-XA) 10,10,2
      2  IN=I-2
      IF(IN) 4,4,6
      4  IN=1
      GO TO 12
      6  NN=N-3
      IF (IN-NN) 12,12,8
      8  IN = NN
      GO TO 12
      10 CONTINUE
      12 IO=IN+3
      YINTP=0.
      DO 20 I=IN,IO
      PROD=Y(I)
      DO 16 J=IN,IO
      IF (I-J) 15,16,15
      15 PROD = PROD*(XA-X(J))/(X(I)-X(J))
      16 CONTINUE
      20 YINTP=YINTP+PROD
      RETURN
      END

```

04/07/81 13.06.42

FTN 4.6+460

TRACE

OPT=0 ROUND=\*

74/74

FUNCTION C-ITTC

CFITTC 2  
CFITTC 3  
CFITTC 4  
CFITTC 5  
CFITTC 6  
CFITTC 7  
CFITTC 8  
CFITTC 9

FUNCTION CFITTC (RN)

THIS FUNCTION DETERMINES THE ITTC CORRELATION ALLOWANCE

DEN = ALDG10 (RN) - 2.0  
CFITTC = 0.075 / DEN\*\*2  
RETURN  
END

1

C

C

5

PROGRAM LISTING OF SYNTHESIS

```

1  PROGRAM SWATH(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT,TAPE8)
2  MAIN
3  PROGRAM FOR THE RESISTANCE AND PROPULSION OF SWATH SHIPS
4  PROGRAMMED BY A. M. REED JUNE 1975
5  POWERING MODULE BY W. G. DAY
6  APPEN AGE DRAG MODULE BY J. W. GRANT
7  REVISED APRIL 1978 BY E. C. CHAI
8
9  COMMON / COEFS / ASM(3), BSM(3), ABM(3), BBM(3), MMAX
10 COMMON / INPUT / XLS, HS, TSMAX, CWP, CLCF, CIY, XLB, HB, AX, CP,
11 1 CLCB, SEPDIS, CSTRUT, CSTR2, FDIS, SPAN, CHORD, TFINS, NLOC
12
13 COMMON / OMEGA / VMFPS, GAMAS, GAMASB, GOSQ, HSOLS, HBOLB, WETS,
14 1 WETB, WETFIN, WTSURF, SEP, PHIS, PHIB, RATIOL, CFS, CFB, APPDRG
15
16 COMMON / PHYSICO / RHO, G, PI, DELCF
17
18 COMMON/PSI/NPTSZ,PTSAF,EXP,N,NALMAX,NAL,TAIL,ALFA
19 1,ALSMAX,NSTEPS
20
21 DIMENSION TITLE(8), VOFF(24), EHP(24), SHP(24)
22
23 DEFINE THE PSI CONSTANTS
24
25
26
27
28
29
30
31
32
33
34
35
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37
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41
42
43
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55
56
57
58

```

READ AND CHECK INPUT  
 CALL RIN(TITLE)  
 CALCULATE THE OMEGA AND BODY CONSTANTS  
 HSOLS = HS/XLS  
 HBOLB = HB/XLB  
 RATIOL = XLB/XLS  
 B = CSTRUT/XLS  
 D = 0.0  
 IF ( NLOC .NE. 0 ) D = CSTR2/XLS  
 SFINS = SPAN\*CHORD  
 TBFIN = 0.01\*TFINS  
 IF(XLB .GT. 30.0 .AND. TBFIN .LT. 0.041666) TBFIN = 0.041666  
 IF(XLB .LE. 30.0 .AND. TBFIN .LT. 0.005208) TBFIN = 0.005208  
 SBFIN = TBFIN\*SPAN  
 SORTL = SORT(XLS)  
 BDIA = SORT(AX/PI)

DETERMINE THE CHEBYSHEV COEFFICIENTS FOR THE SHIP  
 CALCULATE THE THE WETTED SURFACE OF THE BODY AND STRUT  
 PLOT THE STRUT PROFILE AND SECTIONAL AREA CURVE  
 CALL CHEB(TITLE)

DETERMINE THE SPEEDS AND PROCEED THROUGH THE RESISTANCE LOOP  
 READ(5,100) VKMIN, VKMAX, NC  
 IF ( NC .GT. 20 ) GO TO 90





PROGRAM	SWATH	74/74	OPT=0	ROUND=*	TRACE	FTN	4.6+460	04/07/81	13.10.59	PAGE	3
115											
	100	FORMAT(2F10.5,I5)									
	101	FORMAT(1H1,BA10//T5,"V(KNOTS)",T16,"V(FT/SEC)",T27,"SLR(STRUT)",						SYNTHS	116		
		1 T46,"EMP",T58,"SHP",T71,"PC-)						SYNTHS	117		
	102	FORMAT(6(2X,F10.3))						SYNTHS	118		
	103	FORMAT("*****ERROR NC GREATER THAN 20, NC = ",I3)						SYNTHS	119		
		END						SYNTHS	120		
120								SYNTHS	121		

```
1      BLOCK DATA
C
5      COMMON / COEFS / ASM(3), BSM(3), ABM(3), BBM(3), MMAX
C
C      COMMON / PHYSCO / RHO,GNU,G.PI,DELFCF
C
C      COMMON/PSI/NPTSZ,PTSFAF,EXP,NALMAX,NAL,TAIL,ALFA
C      ,ALSMAX,NSTEPS
10     COMMON/PLOT/NFIRST,NLAST,NPOINT,XMAX,XMIN,NSCL1,NCHAR,NSCALE(4),
C      PCHAR(2)
C      COMMON/XRPLOTO/I,J,K,L,NHL,NSBH,NVL,NSBV,HCHAR,VCHAR,ISX,ISY,V,H
C
15     LOGICAL NSCL1
C
C      MAXIMUM ORDER OF CHEBYCHEV APPROXIMATION
C
20     DATA MMAX / 3 /
C
C      DEFINE PHYSICAL CONSTANTS
C
C      DATA RHO / 1.9908 /
C      DATA GNU / 1.297E-5 /
C      DATA G / 32.174 /
C      DATA PI / 3.1415926535898 /
C      DATA DELCF / 0.0005 /
C
C      DEFINE CONSTANTS FOR NUMERICAL INTEGRATION
C
30     DATA NPTSZ / 31 /
C      DATA PTSFAF / 10.0 /
C      DATA EXPN / 7.0 /
C      DATA NALMAX / 300 /
C      DATA ALSMAX / 26.0 /
C
C      DEFINE DATA FOR PLOT ROUTINE
C
40     DATA NHL, NSBH, NVL, NSBV, HCHAR, VCHAR, PCHAR(1), PCHAR(2) /
C      6., 10., 11., 10., 1H., 1H., 1H., 1H. /
C
C      DATA NFIRST, NLAST, NPOINT / 1., 101., 1 /
C
C      DATA XMAX, XMIN, NSCL1 / 1.0, -1.0, .TRUE. /
C
45     DATA NCHAR / 0 /
C
C      DATA NSCALE / 0., 3., 0., 3 /
C
END
```

```

1      SUBROUTINE CHEB(TITLE)
2      COMMON / COEFS , AS ( ), BSM(3), ABM(3), BBM(3), MMAX
3
4      COMMON / INPUT / XLS, MS, TSMAX, CWP, CLCF, CIYY, XLB, HB, AX, CP,
5      1 CLCB, SEPDIS, CSTRUT, CSTRT2, PDIA, SPAN, CHORD, TFINS, NLOC
6
7      COMMON / OMEGA / VMFPS, GAMAOS, GAMAOSB, GOSQ, HSOLS, HBOLB, WETS,
8      1 WETB, WETFIN, WTSURF, SEP, PHIS, PHIB, RATIOL, CFS, CFB, APPDRG
9
10     COMMON / PHYSCO / RHO,GNU,G.PI,DELCF
11
12     DIMENSION TITLE(8)
13
14     DETERMINE THE CHEBYSHEV COEFFICIENTS
15
16     ASM(1) = 4.0*CWP/PI
17     ASM(2) = (1.0 - 16.0*CIYY)*ASM(1)
18     ASM(3) = 1.0 - ASM(1) - ASM(2)
19     BSM(1) = 4.0*CLCF*ASM(1)
20     BSM(2) = 0.0
21     BSM(3) = 0.0
22     ABM(1) = 4.0*CP/PI
23     ABM(2) = 1.0 - ABM(1)
24     ABM(3) = 0.0
25     BBM(1) = 4.0*CLCB*ABM(1)
26     BBM(2) = 0.0
27     BBM(3) = 0.0
28
29     DETERMINE THE WETTED SURFACE
30
31     CALL WSURFB(WETB)
32     CALL WSURFS(WETS)
33     WETB = WETB - XLS*TSMAX*CWP
34     IF ( NLOC .NE. 0 ) WETB = WETB - XLS*TSMAX*CWP
35     WETFIN = 2.0*CHORD*SPAN
36     WTSURF = WETB + WETS + WETFIN
37     IF ( NLOC .NE. 0 ) WTSURF = WTSURF + WETS
38
39     PRINT THE CHEBYSHEV COEFFICIENTS AND THE WETTED SURFACE
40
41     WRITE(6,340) (TITLE(I),I = 1, 8 )
42     WRITE(6,330) (ASM(M),M=1,MMAX)
43     WRITE(6,335) (BSM(M),M=1,MMAX)
44     WRITE(6,345) (ABM(K),K=1,MMAX)
45     WRITE(6,350) (BBM(K),K=1,MMAX)
46     WRITE(6,357) WETS,WETB, WETFIN, WTSURF
47
48     PLOT THE STRUT WATER LINE AND THE BODY AREA DISTRIBUTION
49
50     CALL PCHEB (ASN,BSM,ABM,BBM,MMAX,TITLE)
51     RETURN
52
53     FORMAT(1H0,33X,'STRUT CHEBYSHEV COEFFICIENTS ASM(M)=',(10X,SE16.8))
54     FORMAT(1H0,33X,'STRUT CHEBYSHEV COEFFICIENTS BSM(M)=',(10X,SE16.8))
55     FORMAT(1H0,33X,'STRUT CHEBYSHEV COEFFICIENTS ABM(M)=',(10X,SE16.8))
56     FORMAT(1H0,33X,'STRUT CHEBYSHEV COEFFICIENTS BBM(M)=',(10X,SE16.8))
57
58

```

04/07/81 13.10.59

FTN 4.6+460

74/74 OPT=0 ROUND=0/ TRACE

SUBROUTINE CHEB

CHEB 59  
CHEB 60  
CHEB 61  
CHEB 62  
CHEB 63

357 FORMAT(1H0,4X,\* STRUT WETTED SURFACE IN SQUARE FEET =\*,E14.7,  
1/ 4X,\* BODY WETTED SURFACE IN SQUARE FEET =\*,E14.7,  
2/ 4X,\* FOIL WETTED SURFACE IN SQUARE FEET =\*,E14.7,  
3/ 4X,\* TOTAL WETTED SURFACE IN SQUARE FEET =\*,E14.7)

END

04/07/81 13.10.59

FTN 4.6+460

74/74 OPT=0 ROUND=0/ TRACE

SUBROUTINE RIN

```

1      SUBROUTINE RIN(TITLE)
2      RIN
3      RIN
4      RIN
5      COMMON / INPUT / XLS, HS, TSMAX, CWP, CLCF, CIYY, XLS, HB, AX, CP,
6      1 CLCB, SEPDIS, CSTRUT, CSTR2, PDIA, SPAN, CHORD, TFINS, NLOC
7      RIN
8      RIN
9      RIN
10     RIN
11     RIN
12     RIN
13     RIN
14     RIN
15     RIN
16     RIN
17     RIN
18     RIN
19     RIN
20     RIN
21     RIN
22     RIN
23     RIN
24     RIN
25     RIN
26     RIN
27     RIN
28     RIN
29     RIN
30     RIN
31     RIN
32     RIN
33     RIN
34     RIN
35     RIN
36     RIN
37     RIN
38     RIN
39     RIN
40     RIN
41     RIN
42     RIN
43     RIN
44     RIN
45     RIN
46     RIN
47     RIN
48     RIN
49     RIN
50     RIN
51     RIN
52     RIN
53     RIN
54     RIN
55     RIN
56     RIN
57     RIN
58     RIN

    DIMENSION TITLE(8)
    INPUT
    TITLE = LABEL PRINTED ON OUTPUT
    XLS = LENGTH OF STRUT (FT)
    HS = DRAFT OF STRUT (FT)
    TSMAX = MAXIMUM THICKNESS OF STRUT (FT)
    CWP = WATERPLANE AREA COEFFICIENT
    CWP = AWP / (TSMAX * LS)
    AWP = LS * (TSMAX/2) * (PI/2) * AS1
    CLCF = WATERPLANE MOMENT COEFFICIENT
    CLCF = MY(STRUT) / (AWP*LS)
    MY(STRUT) = (TSMAX/2) * (LS/2)**2 * (PI/2) * BS1
    CIYY = WATERPLANE INERTIA COEFFICIENT
    CIYY = IYY / (AWP*LS**2)
    IYY = (1/2) * (TSMAX/2) * (LS/2)**3 * (PI/2) * (A1 - A2)
    XLS = LENGTH OF BODY (FT)
    HB = DEPTH OF SUBMERGENCE TO BODY CENTERLINE (FT)
    AX = MAXIMUM BODY CROSS-SECTIONAL AREA (FT**2)
    CP = BODY PRISMATIC COEFFICIENT
    CP = DISPLACEMENT(BODY) / (AX * LB)
    DISPLACEMENT(BODY) = LB * AX * (PI/4) * AB1
    CLCB = BODY MOMENT COEFFICIENT
    CLCB = MY(BODY) / (AX*LB**2)
    MY(BODY) = AX * (LB/2)**2 * (PI/4) * BB1
    SEPDIS = SEPARATION DISTANCE OF HULL CENTERLINES (FT)
    CSTRUT = DISTANCE OF CL OF STRUT FROM CL OF BODY (FT)
    (+ FORWARD OF THE BODY CL. - AFT OF THE BODY CL)
    CSTR2 = DISTANCE OF CL OF SECOND STRUT ( IF PRESENT ) FROM
    CL OF BODY (FT)
    NLOC = SWITCH INDICATING THE PRESENCE OF A SECOND STRUT
    NLOC = 0 - ONE STRUT ONLY
    NLOC = 1 - TWO STRUTS
    PDIA = PROPELLER DIAMETER (FT)
    SPAN = SPAN OF A DEMI-FIN (FT)
    CHORD = CHORD OF A DEMI-FIN (FT)
    TFINS = MAXIMUM THICKNESS OF A DEMI-FIN (FT)

    READ INPUT
    READ (5,210) (TITLE(K),K=1,8)
    READ(5,215) XLS,HS,TSMAX
    READ (5,215) CWP,CLCF, CIYY
    READ(5,215) XLS,HB,AX
    READ(5,215) CP,CLCB
    READ(5,215) SEPDIS
    READ(5,216) CSTRUT, CSTR2, NLOC
    READ(5,215) PDIA
    READ(5,215) SPAN,CHORD,TFINS
    ECNO INPUT
  
```



```

1      SUBROUTINE ROUT(TITLE, EHP)
2      ROUT
3      COMMON / INPUT / XLS, HS, TSMAX, CWP, CLCF, CIYV, XLB, HB, AX, CP,
4      1 CLCB, SEPDIS, CSTRUT, CSTRT2, PDIA, SPAN, CHORD, TFINS, NLOC
5      ROUT
6      COMMON / OMEGA / VMFPS, GAMAOB, CAMAOB, COSQ, HSOLS, HBOLB, WETS,
7      1 WETB, WETFIN, WTSURF, SEP, PHIS, PHIB, RATIOL, CFS, CFB, APPDRG
8      ROUT
9      COMMON / PHYSIO / RHO, GNU, G, PI, DELCF
10     ROUT
11     ROUT
12     ROUT
13     ROUT
14     ROUT
15     ROUT
16     ROUT
17     ROUT
18     ROUT
19     ROUT
20     ROUT
21     ROUT
22     ROUT
23     ROUT
24     ROUT
25     ROUT
26     ROUT
27     ROUT
28     ROUT
29     ROUT
30     ROUT
31     ROUT
32     ROUT
33     ROUT
34     ROUT
35     ROUT
36     ROUT
37     ROUT
38     ROUT
39     ROUT
40     ROUT
41     ROUT
42     ROUT
43     ROUT
44     ROUT
45     ROUT
46     ROUT
47     ROUT
48     ROUT
49     ROUT
50     ROUT
51     ROUT
52     ROUT
53     ROUT
54     ROUT
55     ROUT
56     ROUT
57     ROUT
58     ROUT

```

1 SUBROUTINE ROUT(TITLE, EHP)  
 COMMON / INPUT / XLS, HS, TSMAX, CWP, CLCF, CIYV, XLB, HB, AX, CP,  
 1 CLCB, SEPDIS, CSTRUT, CSTRT2, PDIA, SPAN, CHORD, TFINS, NLOC  
 COMMON / OMEGA / VMFPS, GAMAOB, CAMAOB, COSQ, HSOLS, HBOLB, WETS,  
 1 WETB, WETFIN, WTSURF, SEP, PHIS, PHIB, RATIOL, CFS, CFB, APPDRG  
 COMMON / PHYSIO / RHO, GNU, G, PI, DELCF  
 DIMENSION TITLE(8)  
 SUM = A(TRANSPOSE)\*I\*A + B(TRANSPOSE)\*W\*B  
 CALL SUM(SUM1S, SUM1B, SUM1SB, SUM12S, SUM12B, SM12SB)  
 COMPUTE THE CONSTANTS NEEDED FOR OUTPUT  
 FROUDS = VMFPS/SORT(32.155\*XLS)  
 VLS = FROUDS\*SORT(G)/1.6878  
 FROUDB = VMFPS/SORT(32.155\*XLB)  
 VLB = FROUDB\*SORT(G)/1.6878  
 VMKNTS = VMFPS/1.6878  
 B2OLB = SEPDIS/XLB  
 CSOLB=CSTRUT/XLB  
 IF ( NLOC .NE. 0 ) CSOLB2 = CSTRT2/XLB  
 AAS = ( TSMAX/HS )\*(PI/2.0)\*GAMAOB  
 AAB = 2.0\*PI\*(AX/XLB\*\*2)\*(GAMAOB/GAMAOB\*\*2)  
 AASB = (2.0\*PI)\*AX/(HS\*XLS)  
 AAWTSF = (0.5\*RHO\*WTSURF\*VMFPS\*\*2)/1000.  
 COMPUTE THE WAVE RESISTANCE COEFFICIENTS  
 CMS1 = AAS\*SUM1S  
 R1S = CMS1\*RHO\*G\*TSMAX\*HS\*XLS  
 CWS1 = R1S/AAWTSF  
 CMB1 = AAB\*SUM1B  
 R1B = CMB1\*RHO\*G\*AX\*XLB  
 CWB1 = R1B/AAWTSF  
 CMSB1 = AASB\*SUM1SB  
 R1SB = CMSB1\*RHO\*G\*TSMAX\*HS\*XLS  
 CWSB1 = R1SB/AAWTSF  
 CMS12 = AAS\*SUM12S  
 R12S = CMS12\*RHO\*G\*TSMAX\*HS\*XLS  
 CWS12 = R12S/AAWTSF  
 CMB12 = AAB\*SUM12B  
 R12B = CMB12\*RHO\*G\*AX\*XLB  
 CWB12 = R12B/AAWTSF  
 CMSB12 = AASB\*SM12SB  
 R12SB = CMSB12\*RHO\*G\*TSMAX\*HS\*XLS  
 CWSB12 = R12SB/AAWTSF





04/07/81 13.10.59

FTN 4.6+460

74/74 OPT=0 ROUND=0/ TRACE

SUBROUTINE ROUT

```

115 325 FORMAT(1H ,3X,35H STRUT GEOMETRIC CHARACTERISTICS //,5X,
1 BH XLS =,F12.6,9X,8H HS =,F12.6,9X,8H TSMAX =,F12.6)
340 FORMAT(1H0,3X,35H BODY GEOMETRIC CHARACTERISTICS //,5X,
1 BH XLS =,F12.6,9X,8H HB =,F12.6,9X,8H AX =,F12.6)
354 FORMAT(//T25,"RESISTANCES IN POUNDS ARE FOR A DEMI-HULL")
356 FORMAT(//T25,"SEPARATION DISTANCE IN FEET =,F8.3,
1 5X,* 3/LB =,F7.3)
358 FORMAT(//T25,"STRUT CL FROM BODY CL IN FEET =,F8.3,
1 5X,*STRUT OFFSET/LB =,F7.3)
359 FORMAT(//T25,"FORWARD STRUT CL FROM BODY CL IN FEET =,F8.3,
1 5X,*FORWARD STRUT OFFSET/LB =,F7.3//
2 * AFT STRUT CL FROM BODY CL IN FEET =,F8.3,
3 5X,*AFT STRUT OFFSET/LB =,F7.3)
360 FORMAT(1H0,5X,* SHIP SPEED IS ,F8.3,* FPS, *F8.3,* KNOTS, *
1 6X,* STRUT V-L RATIO =,F8.3,6X,*BODY V-L RATIO =,F8.3)
410 FORMAT(//T1 * 35H WAVE RESISTANCE CALCULATIONS FOR ,8A10)
415 FORMAT(1H ,4X,
1 F12.6,9X,8H HS/LS =,F12.6)
420 FORMAT(1H ,4X,
1 F12.6,9X,8H HB/LB =,F12.6)
430 FORMAT(//T30,32H STRUT WAVE DRAG IN POUNDS = ,E14.7,/30X,
2 32H R15/(RHO/2*WTSURF*V**2) = ,F10.3,4HE-03)
440 FORMAT(//T30,32H BODY WAVE DRAG IN POUNDS = ,E14.7,/30X,
2 32H R13/(RHO/2*WTSURF*V**2) = ,F10.3,4HE-03)
445 FORMAT(//T30,32H STRUT-BODY WAVE DRAG IN LBS = ,E14.7,/30X,
2 32H R15B/(RHO/2*WTSURF*V**2) = ,F10.3,4HE-03,
3 10X,10H CW1 TOT =,F10.3,4HE-03)
450 FORMAT(//T30,32H STRUT INTERFERENCE DRAG LBS = ,E14.7,/30X,
2 32H R12S/(RHO/2*WTSURF*V**2) = ,F10.3,4HE-03)
455 FORMAT(//T30,32H BODY INTERFERENCE DRAG LBS = ,E14.7,/30X,
2 32H R12B/(RHO/2*WTSURF*V**2) = ,F10.3,4HE-03)
460 FORMAT(//T30,32H STRUT-BODY INTERFERENCE DRAG LB = ,E14.7,/30X,
2 32H R12SB/(RHO/2*WTSURF*V**2) = ,F10.3,4HE-03,
3 10X,10H CW2 TOT =,F10.3,4HE-03,/,
4 86X," RW TOTAL = ,E14.7,
5 86X," CW TOTAL = ,F10.3,"E-03")
461 FORMAT(//30X,* CFORM = ,F10.3,4HE-03,
1/30X,*RESIDUAL DRAG COEFF. = ,F10.3,*E-03,
2/30X,*RESIDUAL RESISTANCE IN LBS= ,E14.7)
465 FORMAT(30X,32H STRUT FRICTION DRAG IN LBS = ,E14.7,
1/30X,32H RFS/(RHO/2*WTSURF*V**2) = ,F10.3,4HE-03,
2/30X,32H BODY FRICTION DRAG IN LBS = ,E14.7,
3/30X,32H RFB/(RHO/2*WTSURF*V**2) = ,F10.3,4HE-03,
4/86X," RF TOTAL = ,E14.7,
5/86X," CF TOTAL = ,F10.3,"E-03")
470 FORMAT(//30X,"APPENDAGE DRAG IN POUNDS = ,E14.7,
1/30X,"APPENDAGE DRAG COEFFICIENT = ,F10.3,"E-03")
475 FORMAT(//86X," RT = ,E14.7,
1/86X," CT = ,F10.3,"E-03",
2/86X," EHP = ,F10.3)
END
155

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```

1      SUBROUTINE RWAVE(B,D,NLOC2)
C
C
5      SUBROUTINE FOR COMPUTING AUXILIARY FUNCTIONS T AND W
      USING CHEBYCHEV EXPANSION - PROGRAM VERSION OF 8/05/72
      MODIFICATIONS BY A M REED OCTOBER 1974
C
C
10     COMMON / AUX / TS(3,3), WS(3,3), TB(3,3), WB(3,3), TSB(3,3),
1      WSB(3,3), TS12(3,3), WS12(3,3), TB12(3,3), WB12(3,3), TSB12(3,3),
2      WSB12(3,3), TSBP(3,3), WSBP(3,3), TSB12P(3,3), WSB12P(3,3)
C
C
15     COMMON / COEFS / ASM(3), BSM(3), ABM(3), BBM(3), MMAX
C
C
C      COMMON / INPUT / XLS, HS, TSMAX, CWP, CLCF, CIYY, XLB, HB, AX, CP,
1      CLCB, SEPDIS, CSTRUT, CSTR2, PDIA, SPAN, CHORD, TFINS, NLOC
C
C
20     COMMON / OMEGA / VMFPS, GAMMAOS, GAMAOB, GOSQ, HSOLS, HBOLB, WETS,
1      WETB, WETFIN, WTSURF, SEP, PHIS, PHIB, RATIOL, CFS, CFB, APPDRG
C
C
C      COMMON / PHYSCO / RHO,GNU,G,PI,DELFCF
C
25     COMMON/PSI/NPTSZ,PTSFA,EXPN,NALMAX,NAL,TAIL,ALFA
1      ,ALSMAX,NSTEPS
C
C      DIMENSION SIMP(100),VJALFA(7)
C
30     MMAX2=MMAX*2
C
C      SET THE T AND W ARRAYS TO ZERO
C
C      CALL RINIT
C
35     INTEGRATION OF T AND W FROM ALPHA EQUALS GAMMAOS TO GAMMAOS+1.0
      MAKE TRIGONOMETRIC SUBSTITUTION TO AVOID SQUARE ROOT
      SINGULARITY AT ALPHA EQUALS GAMMAOS
C
C      ZETA IS THE VARIABLE OF INTEGRATION--ZETA=SQRT(ALPHA-GAMMAOS)
40     NPTSZ IS THE NUMBER OF POINTS TO TAKE IN THE INTERVAL
      0.0 LESS THAN OR EQUAL ZETA LESS THAN OR EQUAL 1.0
      AINCR IS THE STEP SIZE FOR THE ZETA INTEGRATION
      ALFAZ IS THE VALUE OF ALPHA FOR ZETA VARYING FROM ZERO TO ONE
C
C
45     SEP = (2.0/GAMMAOS)*SEPDIS/XLS
      CALL SIMPSN(NPTSZ,SIMP)
      XNPTZ=FLOAT(NPTSZ)
      AINCR = 1.0/(XNPTZ-1.0)
      HZETA = AINCR/3.0
      DO 30 I=1,NPTSZ
        WTINT = SIMP(I) * HZETA
        EI=FLOAT(I-1)
        ZETA = AINCR*EI
        ALFAZ = GAMMAOS+ZETA**2
        ALFAQ=ALFAZ**2
        SQZTA=2.0/SORT(GAMMAOS+ALFAZ)
C
50
C
55
C
58

```

60	C	SEPCOS = COS(SEP*ALFAZ+SQRT(ALFASQ-GOSQ))	59	RWAVE
		CALL RINTEG(ALFAZ,B,D,NLOC2,WTINT,SEPCOS,SQZTA)	60	RWAVE
	C		61	RWAVE
	30	CONTINUE	62	RWAVE
	C		63	RWAVE
	C	INTEGRATION FOR T AND W FROM ALPHA EQUALS GAMMAOS+1.0 TO ALMAX	64	RWAVE
65	C		65	RWAVE
		NAL = 0	66	RWAVE
		ALFA = GAMMAOS + 1.	67	RWAVE
		PWT = 0.	68	RWAVE
		ALMAX = SQRT((2.302585*EXPN*GAMMAOS) / (2.*HBOLEB*RATIOCL)	69	RWAVE
70	20	+ (GAMMAOS+1.)*2 )	70	RWAVE
		CONTINUE	71	RWAVE
		ISIMP = 1	72	RWAVE
		IF 'ALFA.G1.ALMAX) GO TO 215	73	RWAVE
		IF (NAL.LT.NALMAX) GO TO 212	74	RWAVE
75		WRITE (6,302)	75	RWAVE
		GO TO 215	76	RWAVE
		CONTINUE	77	RWAVE
212		NAL = NAL + 2	78	RWAVE
		DDDA = (2.0*ALFASQ-GOSQ)/SQRT(ALFASQ-GOSQ)	79	RWAVE
80		SSIZE=(2.*PI)/((2.*RATIOCL+DDDA*SEP)*PTSAF)	80	RWAVE
		TWT= SSIZE/3.	81	RWAVE
		WTINT = TWT + PWT	82	RWAVE
		PWT = TWT	83	RWAVE
		GO TO 250	84	RWAVE
85	215	CONTINUE	85	RWAVE
		ISIMP=3	86	RWAVE
		WTINT = PWT	87	RWAVE
		GO TO 250	88	RWAVE
220		CONTINUE	89	RWAVE
		WTINT = 4.*TWT	90	RWAVE
90		ISIMP = 2	91	RWAVE
	250	CONTINUE	92	RWAVE
		ALFASQ=ALFA*2	93	RWAVE
		SQ=1.0/SQRT(ALFASQ-GOSQ)	94	RWAVE
95		SEPCOS = COS(SEP*ALFA/SQ)	95	RWAVE
	C		96	RWAVE
		CALL RINTEG(ALFA,B,D,NLOC2,WTINT,SEPCOS,SQ)	97	RWAVE
	C		98	RWAVE
		ALFA = ALFA + SSIZE	99	RWAVE
100	C	GO TO (220,210,270), ISIMP	100	RWAVE
	C		101	RWAVE
	C	ADD TAIL INTEGRATION TO TS AND WS	102	RWAVE
	C		103	RWAVE
270		CONTINUE	104	RWAVE
		ALFA = ALFA - SSIZE	105	RWAVE
105		NSTEPS = 0	106	RWAVE
		IF (ALSMAX.LE.ALFA) GO TO 278	107	RWAVE
		SSIZE = PI/PTSAF	108	RWAVE
		ANSTEP = (ALSMAX-ALFA)/SSIZE	109	RWAVE
110		NSTEPS = IFIX(ANSTEP/2.)*2 + 2	110	RWAVE
		SSIZE = (ALSMAX-ALFA) / NSTEPS	111	RWAVE
		*I = SSIZE/3.	112	RWAVE
		ANW/I = 1.	113	RWAVE
		ADO = NSTEPS + 1	114	RWAVE
			115	RWAVE

AD-A099 533

DAVID W TAYLOR NAVAL SHIP RESEARCH AND DEVELOPMENT CE--ETC F/G 20/4  
DOCUMENTATION FOR SWATH SHIP RESISTANCE AND PROPULSION PREDICTI--ETC(U)  
APR 81 A M REED

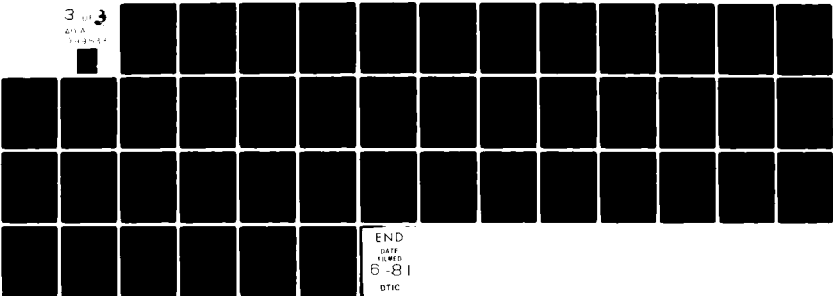
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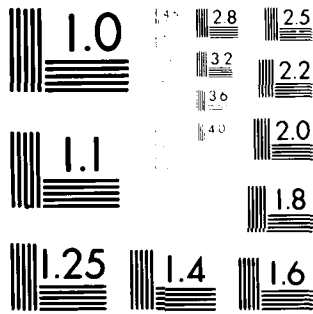
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3 of 3

DTNSRDC



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MICROCOPY RESOLUTION TEST CHART  
NATIONAL BUREAU OF STANDARDS-1963-A

04/07/81 13.10.59

FTN 4.6+460

74/74 OPT=0 ROUND=0 TRACE

SUBROUTINE RWAVE

```

115      CON=1.0
      DO 277 IDO = 1, NDO
        ALFASQ=ALFA**2
        IF (NLOC2.NE.0) CON=2.0*(1.0+CON*((B-D)*ALFA**2.0))
        CALL BESSJ (ALFA,MMAX2,VJALFA)
        VS = PHIS*ALFASQ
        SQ=1.0/SQRT(ALFASQ-GOSQ)
        ESA = 1. - EXP (-VS)
        ES = SQ * ESA**2 / ALFASQ
        DO 276 M = 1,MMAX
          MAA = 2*N
          MBB = MAA + 1
          DO 275 N = M, MMAX
            NAA = 2*N
            NBB = NAA + 1
            WTINT = ANWT * WT
            TSA = WTINT*ES*VJALFA(MAA)*VJALFA(NAA)*CON
            WSA = WTINT*ES*VJALFA(MBB)*VJALFA(NBB)*CON
            TS(M,N) = TS(M,N) + TSA
            WS(M,N) = WS(M,N) + WSA
          CONTINUE
        CONTINUE
        ALFA = ALFA + SSIZE
        BNWT = 2.
        IF (ANWT.LE.2.) BNWT = 4.
        IF (IDO.EQ.NDO-1) BNWT = 1.
        ANWT = BNWT
      CONTINUE
275      CONTINUE
276      CONTINUE
277      CONTINUE
278      CONTINUE
      ALFASQ = ALFA**2
      RAT = GAMMAOS/ALFA
      IF (RAT.LT.1.E-4) GO TO 280
      TAIL=(-SQRT(ALFASQ-GOSQ)/ALFASQ+ASIN(RAT)/GAMMAOS)/(2.0*PI*GOSQ)
      GO TO 290
280      CONTINUE
      TAIL=1.0/(3.0*PI*ALFA*ALFASQ)
      C
      C      CALCULATE TAIL RESULTS
      C
290      CONTINUE
      DO 296 M = 1,MMAX
        DO 295 N = M, MMAX
          SIGN = (-1)**(M+N)
          TS(M,N) = TS(M,N) - SIGN*TAIL
          WS(M,N) = WS(M,N) + SIGN*TAIL
        CONTINUE
      CONTINUE
295      CONTINUE
296      CONTINUE
      C
      C      MULTIPLY BY CONSTANTS AND REFLECT SYMMETRIC MATRICES)
      C
      C      CALL REFLKT
      C
      C      RETURN
302      FORMAT (*1ALFA INTEGRATION REACHED NALMAX*)
      ENU

```

```

1      SUBROUTINE RINTEG(ALFA,B,D,NLOC2,TWINT,SEPCOS,SQ)
C
C      NUMERICAL INTEGRATION FOR AUXILIARY FUNCTIONS T AND W
C
5      COMMON / AUX / TS(3,3), WS(3,3), TB(3,3), WB(3,3), TSB(3,3),
1      WSB(3,3), TS12(3,3), WS12(3,3), TB12(3,3), WB12(3,3), TSB12(3,3),
2      WSB12(3,3), TSBP(3,3), WSBP(3,3), TSB12P(3,3), WSB12P(3,3)
C
10     COMMON / COEFS / ASM(3), BSM(3), ABM(3), BBM(3), MMAX
C
C      COMMON / INPUT / XLS, HS, TSMAX, CWP, CLCF, CIYY, XLB, HB, AX, CP,
1      CLCB, SEPDIS, CSTRUT, CSTRY2, POIA, SPAN, CHORD, TFINS, NLOC
C
15     COMMON / OMEGA / VMFPS, GAMMAOS, GAMAOB, GOSQ, HSOLS, HBOLB, WETS,
1      WETB, WETFIN, WTSURF, SEP, PHIS, PHIB, RATIOL, CFS, CFB, APPDRG
C
C      DIMENSION VJALFA(7),VJBETA(7)
C
C      MMAX IS MAXIMUM NUMBER OF TERMS IN CHEBCHEV SERIES
C
20     MMAX2 = 2*MMAX
C      BETA = RATIOL*ALFA
C      ALFASQ=ALFA**2
C
C      CALCULATE FACTORS FOR STRUT NOT CENTERED
C
C      CO=COS(B*ALFA*2.0)
C      SI=SIN(B*ALFA*2.0)
C      CON=1.0
C      IF (NLOC2.EQ.0) GO TO 32
C
30     CALCULATE FACTORS FOR TANDEM STRUTS
C
C      CO=(CO+COS(D*ALFA*2.0))
C      SI=(SI+SIN(D*ALFA*2.0))
C      CON=2.0*(1.0+COS((B-D)*ALFA*2.0))
C      CONTINUE
C
32     COMPUTE AUXILIARY FUNCTIONS VJALFA AND VJBETA
C
C      CALL BESSJ (ALFA, MMAX2, VJALFA )
C      CALL BESSJ ( BETA, MMAX2, VJBETA )
C
C      COMPUTE AUXILIARY FUNCTIONS ES AND EB FOR ALPHA FROM
C
45     VS=PHIS*ALFASQ
C      VB = PHIB*BETA**2
C      ESA = 1.0
C      EBA = 0.0
C
50     IF(VS .LT. 300.) ESA = ESA-EXP(-VS)
C      IF(VB .LT. 300.) EBA = EXP(-VB)
C      ES=SQ*ESA**2/ALFASQ
C      EB=SQ*EBA**2/ALFASQ
C      ESB = SQ*ESA*EBA
C
55     TB,TS,WB,WS,TW12,TS12,WB12, AND WS12 ARE ALL SYMMETRIC WRT M
C      AND N SO WE NEED ONLY CALCULATE THE UPPER HALF OF THESE
C

```



04/07/81 13.10.59

FTN 4.6+460

74/74 OPT=0 ROUND=0/ TRACE

SUBROUTINE RINTEG

```

C
C
60      DO 56 M=1,MMAX
      MAA = 2*M
      MBB = 2*M+1
      DO 55 N=M,MMAX
      NAA = 2*N
      NBB = 2*N+1
      TSA = WTINT*ES*VJALFA(MAA)*VJALFA(NAA)*CON
      WSA = WTINT*ES*VJALFA(MBB)*VJALFA(NBB)*CON
      IF(EB.EQ.0.0) GO TO 54
      TBA = WTINT*EB*VJBETA(MAA)*VJBETA(NAA)
      WBA = WTINT*EB*VJBETA(MBB)*VJBETA(NBB)
      TSBA = WTINT*ESB*VJBETA(NAA)*VJALFA(MAA)*CO
      TSBB = - WTINT*ESB*VJBETA(NAA)*VJALFA(MBB)*SI
      WSBA = WTINT*ESB*VJBETA(NBB)*VJALFA(MBB)*CO
      WSBB = WTINT*ESB*VJBETA(NBB)*VJALFA(MAA)*SI
      TSBBP = - WTINT*ESB*VJBETA(MAA)*VJALFA(NBB)*SI
      WSBBP = WTINT*ESB*VJBETA(MBB)*VJALFA(NBB)*CO
      TB(M,N) = TB(M,N)+TBA
      WB(M,N) = WB(M,N)+WBA
      TSB(M,N) = TSB(M,N)+TSBA
      TSBBP(M,N) = TSBBP(M,N)+TSBBP
      WSB(M,N) = WSB(M,N)+WSBA
      WSBP(M,N) = WSBP(M,N)+WSBP
      IF(M.EQ.N) GO TO 54
      TSBN(M) = TSB(N,M)+TSBB
      TSBBP(N,M) = TSBBP(N,M)+TSBBP
      WSB(N,M) = WSB(N,M)+WSBB
      WSBP(N,M) = WSBP(N,M)+WSBBP
      CONTINUE
      TS(M,N) = TS(M,N)+TSA
      WS(M,N) = WS(M,N)+WSA
      TS12(M,N) = TS12(M,N)+TSA*SEPCOS
      WS12(M,N) = WS12(M,N)+WSA*SEPCOS
      IF(EBA.EQ.0.0) GO TO 55
      TB12(M,N) = TB12(M,N)+TBA*SEPCOS
      WB12(M,N) = WB12(M,N)+WBA*SEPCOS
      TS12(M,N) = TS12(M,N)+TSBA*SEPCOS
      TS12P(M,N) = TS12P(M,N)+TSBAP*SEPCOS
      WS12(M,N) = WS12(M,N)+WSBA*SEPCOS
      WS12P(M,N) = WS12P(M,N)+WSBAP*SEPCOS
      IF(M.EQ.N) GO TO 55
      TS12(N,M) = TS12(N,M)+TSBB*SEPCOS
      TS12P(N,M) = TS12P(N,M)+TSBBP*SEPCOS
      WS12(N,M) = WS12(N,M)+WSBB*SEPCOS
      WS12P(N,M) = WS12P(N,M)+WSBBP*SEPCOS
      CONTINUE
55      CONTINUE
56      RETURN
      END

```

```

1      SUBROUTINE RINIT
      C
      C      INITIALIZE T AND W ARRAY
      C
5      COMMON / AUX / TS(3,3), WS(3,3), TB(3,3), WB(3,3), TSB(3,3),
      1 WSB(3,3), TS12(3,3), WS12(3,3), TB12(3,3), WB12(3,3), TSB12(3,3),
      2 WSB12(3,3), TSBP(3,3), WSBP(3,3), TSB12P(3,3), WSB12P(3,3)
      C
10     COMMON / COEFS / ASM(3), BSM(3), ABM(3), BBM(3), MMAX
      C
      DO 5 M=1,MMAX
      DO 4 N=M,MMAX
      TS(M,N) = 0.0
      WS(M,N) = 0.0
      TB(M,N) = 0.0
      WB(M,N) = 0.0
      TSB(M,N) = 0.0
      TSBP(M,N) = 0.0
      TSB(N,M)=0.0
      TSBP(N,M)=0.0
      WSB(M,N) = 0.0
      WSBP(M,N) = 0.0
      WSB(N,M)=0.0
      WSBP(N,M)=0.0
      TS12(M,N) = 0.0
      WS12(M,N) = 0.0
      TB12(M,N) = 0.0
      WB12(M,N) = 0.0
      TSB12(M,N) = 0.0
      TSB12P(M,N) = 0.0
      TSB12(N,M)=0.0
      TSB12P(N,M)=0.0
      WSB12(M,N) = 0.0
      WSB12P(M,N) = 0.0
      WSB12(N,M)=0.0
      WSB12P(N,M)=0.0
      C
      C      CONTINUE
      C      RETURN
      C      END
4
5
2      RINIT
3      RINIT
4      RINIT
5      RINIT
6      RINIT
7      RINIT
8      RINIT
9      RINIT
10     RINIT
11     RINIT
12     RINIT
13     RINIT
14     RINIT
15     RINIT
16     RINIT
17     RINIT
18     RINIT
19     RINIT
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35     RINIT
36     RINIT
37     RINIT
38     RINIT
39     RINIT
40     RINIT
41     RINIT

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13.10.59

04/07/81

FTN 4.6+460

74/74 OPT=0 ROUND=\*/ TRACE

SUBROUTINE REFLKT

```

1      SUBROUTINE REFLKT
      C
      C      REFLECT THE SYMMETRICAL MATRICES OF T AND W
      C
      COMMON / AUX / TS(3,3), WS(3,3), TB(3,3), WB(3,3), TSB(3,3),
1     WSB(3,3), TS12(3,3), WS12(3,3), TB12(3,3), WB12(3,3), TSB12(3,3),
2     WSB12(3,3), TSBP(3,3), WSBP(3,3), TSB12P(3,3), WSB12P(3,3)
      C
      COMMON / COEFS / ASM(3), BSM(3), ABM(3), BBM(3), MMAX
      C
      DO 64 M = 1, MMAX
      EN=FLOAT(M)
      U = 2.0*EM-1.0
      DO 63 N=M,MMAX
      EN=FLOAT(N)
      FOURMN=4.0*EM*EN
      UV=U*(2.0*EN-1.0)
      TS(M,N) = TS(M,N)*UV
      TS(N,M) = TS(M,N)
      WS(M,N) = WS(M,N)*FOURMN
      WS(N,M) = WS(M,N)
      TB(M,N) = TB(M,N)*UV
      TB(N,M) = TB(M,N)
      WB(M,N) = WB(M,N)*FOURMN
      WB(N,M) = WB(M,N)
      TSB(M,N) = TSB(M,N)*UV
      TSBP(M,N) = TSBP(M,N)*UV
      WSB(M,N) = WSB(M,N)*FOURMN
      WSBP(M,N) = WSBP(M,N)*FOURMN
      IF (M.EQ.N) GO TO 62
      TSB(N,M)=TSB(M,N)*UV
      TSBP(N,M)=TSBP(M,N)*UV
      WSB(N,M)=WSB(M,N)*FOURMN
      WSBP(N,M)=WSBP(M,N)*FOURMN
      CONTINUE
62     TS12(M,N) = TS12(M,N)*UV
        TS12(N,M) = TS12(M,N)
        WS12(M,N) = WS12(M,N)*FOURMN
        WS12(N,M) = WS12(M,N)
        TB12(M,N) = TB12(M,N)*UV
        TB12(N,M) = TB12(M,N)
        WB12(M,N) = WB12(M,N)*FOURMN
        WB12(N,M) = WB12(M,N)
        TSB12(M,N) = TSB12(M,N)*UV
        TSB12P(M,N) = TSB12P(M,N)*UV
        WSB12(M,N) = WSB12(M,N)*FOURMN
        WSB12P(M,N) = WSB12P(M,N)*FOURMN
        IF (M.EQ.N) GO TO 63
        TSB12(N,M) = TSB12(M,N)*UV
        TSB12P(N,M) = TSB12P(M,N)*UV
        WSB12(N,M) = WSB12(M,N)*FOURMN
        WSB12P(N,M) = WSB12P(M,N)*FOURMN
      CONTINUE
63     CONTINUE
64     CONTINUE
      RETURN
      END

```

FUNCTION CFITTC	74/74	DPT=0	ROUND=*	TRACE	FTN 4.6+460	04/07/81	13.10.59	PAGE	1
-----------------	-------	-------	---------	-------	-------------	----------	----------	------	---

1	C	FUNCTION CFITTC(RN)							
	C	THIS FUNCTION DETERMINES THE ITTC CORRELATION ALLOWANCE							
	C								
5	C	THIS FUNCTION DETERMINES THE ITTC CORRELATION ALLOWANCE							
	C								
10		DEN=ALOG10(RN)-2.0							
		CFITTC=0.075/DEN**2							
		RETURN							
		END							

CFITTC	2
CFITTC	3
CFITTC	4
CFITTC	5
CFITTC	6
CFITTC	7
CFITTC	8
CFITTC	9
CFITTC	10
CFITTC	11
CFITTC	12



```

1      SUBROUTINE WSURFB(AREA)
      C
      C      THIS SUBROUTINE DETERMINES THE SURFACE AREA OF A BODY OF
      C      REVOLUTION GIVEN BY CHEBYSHEV COEFFICIENTS
      C
      C      COMMON / COEFS / ASM(3), BSM(3), ABM(3), BBM(3), MMAX
      C
      C      COMMON / INPUT / XLS, HS, TSMAX, CWP, CLCF, CIYY, XLB, HB, AX, CP,
1      CLCB, SEPD1S, CSTRUT, CSTR2, PDIA, SPAN, CHORD, TFINS, NLOC
      C
      C      COMMON / PHYSCO / RHO,GNU,G,PI,DELCF
      C
      RAD=SQRT(AX/PI)
      CON=(2.0*PI/RAD/XLB)**2
      DX=0.05
      DXSQ=DX*DX
      R=0.0
      AREA=0.0
      DO 10 I=1,40
      RL=R
      X=DX*FLOAT(I)-1.0
      R=EVAL(X,ABM,BBM,MMAX)
      IF (R.LT.0.0) R=0.0
      R=SQRT(R)
      RM=(RL+R)*0.5
      DR=R-RL
      AREA=AREA+RM*SQRT(DXSQ+CON*DR**2)
10     CONTINUE
      AREA=PI*RAD*XLB*AREA
      RETURN
      END
30

```

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FIN 4.6+460

SUBROUTINE WSURFS 74/74 OPT=0 ROUND=0/ TRACE

```

1      SUBROUTINE WSURFS(AREA)
      C
      C      THIS SUBROUTINE DETERMINES THE SURFACE AREA OF A STRUT WHOSE
      C      THICKNESS DISTRIBUTION IS GIVEN BY CHEBYSHEV COEFFICIENTS
      C
      C
      C      COMMON / COEFS / ASM(3), BSM(3), ABM(3), BSM(3), MMAX
      C
      C      COMMON / INPUT / XLS, HS, TSMAX, CWP, CLCF, CIYY, XLB, HB, AX, CP,
      C      1 CLCB, SEPDIS, CSTRUT, CSTRT2, PDIA, SPAN, CHORD, TFINS, NLOC
      C
      C      CON=(TSMAX/XLS)**2
      C      DX=0.05
      C      DXSQ=DX**2
      C      AREA=0.0
      C      T=0.0
      C      DO 10 I=1,40
      C          TL=T
      C          X=DX*FLOAT(I)-1.0
      C          T=EVAL(X,ASM,BSM,MMAX)
      C          DT=T-TL
      C          AREA=AREA+SORT(DXSQ+CON*DT**2)
      C
      C      CONTINUE
      C      AREA=XLS*HS*AREA
      C      RETURN
      C      END
10
20
25

```

```

1      SUBROUTINE SIMPSN(NPTS,SIMP)
      C
      C      SET UP SIMPSON'S MULTIPLIERS FOR INTEGRATION
      C      ODD NUMBER OF POINTS GREATER THAN 1 REQUIRED
      C
5      DIMENSION SIMP(NPTS)
      IF((NPTS/2)*2.NE.NPTS) GO TO 3
      WRITE(6,90)
      NPTS=NPTS+1
      CONTINUE
10     SIMP(1)=1.0
      SIMP(NPTS)=1.0
      NPTSM1=NPTS-1
      SM=2.0
      DO 5 J=2,NPTSM1
          SM=6.0-SM
          SIMP(J)=SM
      CONTINUE
      RETURN
20     FORMAT(1H0,'EVEN NO. OF POINTS GIVEN - ADDITIONAL POINT SUPPLIED+')
      END
      SIMPSN 2
      SIMPSN 3
      SIMPSN 4
      SIMPSN 5
      SIMPSN 6
      SIMPSN 7
      SIMPSN 8
      SIMPSN 9
      SIMPSN 10
      SIMPSN 11
      SIMPSN 12
      SIMPSN 13
      SIMPSN 14
      SIMPSN 15
      SIMPSN 16
      SIMPSN 17
      SIMPSN 18
      SIMPSN 19
      SIMPSN 20
      SIMPSN 21
      SIMPSN 22

```



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FTN 4.6+460

74/74 OPT=0 ROUNO=\*/ TRACE

SUBROUTINE SUM

```

1      SUBROUTINE SUM(SUM1S,SUM1B,SUM1SB,SUM12S,SUM12B,SUM12SB)
2      SUM
3      SUM
4      SUM
5      SUM
6      SUM
7      SUM
8      SUM
9      SUM
10     SUM
11     SUM
12     SUM
13     SUM
14     SUM
15     SUM
16     SUM
17     SUM
18     SUM
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20     SUM
21     SUM
22     SUM
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35     SUM
36     SUM
37     SUM
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42     SUM
43     SUM
44     SUM
45     SUM
46     SUM
47     SUM
48     SUM

      SUM COMPUTES THE MATRIX PRODUCTS
      SUM = A(TRANPOSE) * T * A + B(TRANPOSE) * W * B

      COMMON / AUX / TS(3,3), WS(3,3), TB(3,3), WB(3,3), TSB(3,3),
1     WSB(3,3), TS12(3,3), WS12(3,3), TB12(3,3), WB12(3,3), TSB12(3,3),
2     WSB12(3,3), TSBP(3,3), WSBP(3,3), TSB12P(3,3), WSB12P(3,3)

      COMMON / COEFS / ASM(3), BSM(3), ABM(3), BBM(3), MMAX

      SUMA1 = 0.0
      SUMB1 = 0.0
      SUMA2 = 0.0
      SUMB2 = 0.0
      SUMA3 = 0.0
      SUMB3 = 0.0
      SUMA4 = 0.0
      SUMB4 = 0.0
      SUMA5 = 0.0
      SUMB5 = 0.0
      SUMA6 = 0.0
      SUMB6 = 0.0
      DO 20 M=1,MMAX
      DO 10 N=1,MMAX
          SUMA1 = SUMA1+ASM(M)*ASM(N)*TS(M,N)
          SUMB1 = SUMB1+BSM(M)*BSM(N)*WS(M,N)
          SUMA2 = SUMA2+ABM(M)*ABM(N)*TB(M,N)
          SUMB2 = SUMB2+BSM(M)*BSM(N)*WB(M,N)
          SUMA3 = SUMA3+ABM(N)*(ASM(M)*TSB(M,N)+BSM(M)*TSBP(M,N))
          SUMB3 = SUMB3+BSM(N)*(BSM(M)*WSB(M,N)+ASM(M)*WSBP(M,N))
          SUMA4 = SUMA4+ASM(M)*ASM(N)*TS12(M,N)
          SUMB4 = SUMB4+BSM(M)*BSM(N)*WS12(M,N)
          SUMA5 = SUMA5+ABM(M)*ABM(N)*TB12(M,N)
          SUMB5 = SUMB5+BSM(M)*BSM(N)*WB12(M,N)
          SUMA6 = SUMA6+ABM(N)*(ASM(M)*TSB12(M,N)+BSM(M)*TSB12P(M,N))
          SUMB6 = SUMB6+BSM(N)*(BSM(M)*WSB12(M,N)+ASM(M)*WSB12P(M,N))
      CONTINUE
10     CONTINUE
20     SUM1S = SUMA1+SUMB1
      SUM1B = SUMA2+SUMB2
      SUM1SB = SUMA3+SUMB3
      SUM12S = SUMA4+SUMB4
      SUM12B = SUMA5+SUMB5
      SUM12SB = SUMA6+SUMB6
      RETURN
      END

```

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TRACE

74/74

SUBROUTINE FINORG

OPT=0

ROUND=

/

TRACE

```

1  SUBROUTINE FINORG(RHDS,XNUS,VSWF,SFINS,TFINS,CFINS,TBFIN,
   +SBFIN,DS)
   C
   C
   C THESE THREE ROUTINES (FINORG, FOILSC, AND FRICT) ARE EXCERPTS
   C FROM CODING DOCUMENTED IN 'AN INVESTIGATION OF APPENDAGE DRAG'
   C BY MARC P. LASKY (NSRDC SPD EVALUATION REPORT 458-H-01)
   C THIS PACKAGE WAS COMPLETED ON 25 JUN 1975 BY JERRY GRANT
   C NSRDC CODE 1524 THE WORK WAS FUNDED UNDER 1-1507-100-60
   C *****
   C
10  CLACULATION OF THICKNESS-CHORD RATIOS AND FULL-SCALE PARAMETERS
   C
   C
   C TOC = TFINS / CFINS
   C TOC2=TOC*TOC
   C TOC4=TOC2*TOC2
   C TFINS2 = TFINS * TFINS
   C IF (TBFIN.LE.0) GO TO 3105
   C CLOTB = CFINS / TBFIN
   C
20  3105 CONTINUE
   C
   C FLAT PLATE FRICTION COEFFICIENT BASED ON LOCAL REYNOLDS NUMBER
   C
   C CALL FRICT(CFSFIN,VSWF,CFINS,XNUS)
   C
   C CONSTANTS TO CONVERT DRAG COEFFICIENTS TO RESISTANCE IN POUNDS
   C XS = SHIP CONSTANT
   C
   C XS=.5*RHDS*SFINS*VSWF
   C
30  CALCULATION OF DRAG COMPONENTS FOR A SYMMETRICAL FOIL SECTION
   C
   C CALL FOILSC(XS,CFSFIN,TOC,TOC2,TOC4,SFINS,TFINS2,SBFIN,CLOTB,RFS,
   +RFSAS,RPS,RINTS,RBS)
   C
35  TOTAL OF COMPONENT DRAGS
   C
   C DS=RFS+RFSAS+RPS+RINTS+RBS
   C
   C
   C COMPONENTS OF FIN DRAG ARE DEFINED IN SUBROUTINE FOILSC
   C ASSUMPTION - - - NO INDUCED DRAG DUE TO LIFT - - -
   C
40  RETURN
   C
   C END

```

```

1      SUBROUTINE FOILSC(XS,CFS,TOC,TOC2,TOC4,SS,TS2,SBS,CLOTB,RFS,
      +RVAS,RPS,RINTS,RBS)
      C
      C      FLAT FRICTIONAL RESISTANCE
      C
      C      RFS=XS*2.*CFS
      C
      C      RESISTANCE DUE TO VELOCITY AUGMENTATION
      C
      C      RVAS=XS*4.*CFS*TOC
      C
      C      RESISTANCE DUE TO PRESSURE OR SEPARATION (VISCOUS IN NATURE)
      C
      C      RPS=XS*120.*CFS*TOC4
      C
      C      ADDED RESISTANCE DUE TO INTERSECTION WITH HULL
      C
      C      RINTS=(XS/SS)*TS2*((.75*TOC)-(.0003/TOC2))
      C
      C      BASE DRAG DUE TO BLUNTNESS OF TRAILING EDGE
      C
      C      IF(SBS.LE.0.) GO TO 9000
      C      RBS=(XS/SS)*SBS*(.135/((CLOTB*CFS)**(1./3.)))
      C      CONTINUE
      C      RBS=0.
      C      RETURN
      C      END
9000
25
28

```

```

1      SUBROUTINE FRICT(CF,VF,XLEN,XNU)
      C
      C
      C      FLAT PLATE FRICTIONAL COEFFICIENT BASED ON LOCAL REYNOLDS NO.
      RE=VF*XLEN/XNU
      IF(RE.LT.50000.) GO TO 30
      CFTURB=.075/ALOG10(RE/100.)**2
      Y=CFTURB
      CONTINUE
10     CFTURB=.058564/ALOG10(RE*Y)**2
      IF(ABS(CFTURB-Y).LE.1.0E-07) GO TO 20
      Y=(CFTURB+Y)/2.
      GO TO 10
      CONTINUE
20     CF=CFTURB*(143.18/RE)
      RETURN
      CONTINUE
30     CF=1.328/SQRT(RE)
      RETURN
      END
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1      SUBROUTINE SHPCMP(VDES,EMPOES,POIA,BDIA,HB,VOFF,EHP,SHP,NV,TITLE)
2      SHPCMP
3      SHPCMP
4      SHPCMP
5      SHPCMP
6      SHPCMP
7      SHPCMP
8      SHPCMP
9      SHPCMP
10     SHPCMP
11     SHPCMP
12     SHPCMP
13     SHPCMP
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49     SHPCMP
50     SHPCMP
51     SHPCMP
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57     SHPCMP
58     SHPCMP

      THESE PROGRAMS WHICH DETERMINE A PROPELLER DESIGN AND OFF
      DESIGN PERFORMANCE ARE EXCERPTS FROM CODING BY ROBERT F. RODDY
      THIS PACKAGE WAS ASSEMBLED IN JUNE 1975 BY WILLIAM G. DAY
      NSRDC CODE 1524 THE WORK WAS FUNDED UNDER 1-1507-100-60
      *****
      COMMON/CDESC,RHOD(3),ANUD(3),IP
      COMMON/CPROP,IPTYP(3),DIAM(3),VADES(3),RPMDES(3),TDES(3),QDES(3),
1      EFFDES(3),DMWTD(3),CAV(3),Z(3),H(3),BAR(3),PO(3),J(3),
2      IERROR(3),KT(3),KQ(3)
      DIMENSION TITLE(8)
      IPTYP --INDICATE PROPULSOR TYPE
      DIAM --DIAMETER OF PROPULSOR
      VADES --SPEED OF ADVANCE OF PROPULSOR AT DESIGN VA IN KNOTS
      RPMDES --RPM AT DESIGN POINT
      TDES --THRUST OF PROPULSOR SYSTEM IN LBS
      QDES --TORQUE OF PROPULSOR SYSTEM IN FT-LBS
      EFFDES --EFFICIENCY OF PROPULSOR
      DMWTD --THRUST WAKE (1-WT)
      CAV --PERCENT BACK CAVITATION ALLOWED ON WATER SCREWS
      Z --NUMBER OF BLADES OF PROPULSOR
      H --DEPTH OF WATER TO CENTER LINE OF PROPULSOR SHAFT
      BAR --BLADE AREA RATIO OF PROPULSOR
      PD --P/O OF PROPULSOR
      J --J OF PROPULSOR
      IERROR --INDICATOR OF ERROR MESSAGE FOR PROPULSOR
      KT --KT OF PROPULSOR
      KQ --KQ OF PROPULSOR
      INTEGER Z
      REAL J,KT,KQ
      DIMENSION VOFF(NV),EHP(NV),SHP(NV)
      IP = 1
      IS = 1
      RHOD(1S) = 1.9905
      ANUD(1S) = 0.000012817
      CAV(1S) = 2.5
      Z(1S) = 4.
      DIAM(1S) = POIA
      IPTYP(1S) = 1
      VOF = 0.0
      TOF = 0.0
      THRUST DEDUCTION (1-T) IS
      OMT = 1. - (0.05/(DIAM(1S)/BDIA))=1.26)
      THRUST WAKE (1-WT) IS

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TRACE

74/74

SUBROUTINE SHPCMP

```

C
60      DMWT = 1. - (0.71) * EXP(1.58 * (DIAM, IS) * 0.12)
      CMTD(IIS) = DMWT
      H(IIS) = HB
      *DES(IIS) = EMPDES * 550.0 / (VDES * DMWT)
      VADES(IIS) = VDES * DMWT / 1.6878

C
65      DETERMINE THE CHARACTERISTICS AND PERFORMANCE OF PROPELLOR
C
C      CALL PRODES(IIS)
C
C      PRINT PERFORMANCE DATA OF PROPELLOR
C
C      CALL PROPP(IIS, TITLE)
C
C      SHDES = 6.2831853 * QDES(IIS) * RPMDES(IIS) / 35000.
      PC = TDES(IIS) * VDES * DMWT / (SHDES * 550.0)
      SHPINV = SHDES
      WRITE(6, 703) SHDES, PC
      CT = 8.0 * TDES(IIS) / (3.14159 * RHOD(IP) * (VADES(IIS) * DIAM(IIS) * 1.6878) ** 2)
      WRITE(6, 704) CT, DMWT, DMWT

C
80      CALCULATE OPEN WATER CURVE OF PROPELLOR
C
C      CALL PROPER(IIS, VOF, TOF, DUMMY, TITLE)
C
C      DO 22 I=1, NV
      VKOFF = VOFF(I) / 1.6878
      TOFF = EMP(I) * 550.0 / (VOFF(I) * DMWT)

C
C      DETERMINE OFF DESIGN PERFORMANCE
C
C      CALL PROPERO(IIS, VKOFF, TOFF, SHP(I), TITLE)
C
22      CONTINUE
      RETURN
C
703      FORMAT(//, 1X, *SHP= *, F12.3, 5X, *ETA = *, F6.3, ///)
C
704      FORMAT(20X, *THRUST COEFFICIENT = *, F6.3, / 20X, *THRUST DEDUCTION(1-T)
      1 = *, F6.3 / 20X, *THRUST WAKE (1-WT) = *, F6.3)
      END

```

```

1      SUBROUTINE PRODES(IS)
2
3      C
4      C PRODES IS USED IN DESIGN OF PROPULSION SYSTEM TO DETERMINE THE
5      C CHARACTERISTICS AND PERFORMANCE AT DESIGN CONDITION
6
7      C
8      C INPUT-OUTPUT PARAMETERS ARE INTRODUCED THROUGH COMMON BLOCK /CPROP/.
9      C ARGUMENT -IS- INDICATES PROPULSION SYSTEM BEING CONSIDERED.
10
11      C
12      C COMMON/BARCK/IE
13
14      C
15      C COMMON/CDESC/RHOD(3),ANJD(3),IP
16
17      C
18      C COMMON/CPROP/IPTYP(3),DIAM(3),VADES(3),RPMDES(3),TDES(3),QDES(3),
19      C 1 EFFDES(3),OMWTD(3),CAV(3),Z(3),H(3),BAR(3),PD(3),J(3),
20      C 2 ERROR(3),KT(3),KQ(3)
21
22      C
23      C REAL J,KT,KQ
24
25      C
26      C INTEGER Z,IPTYP
27
28      C
29      C ERROR(1S)=0
30      C IE=0
31      C ITQ=1
32      C IPJ=2
33      C IPTYP=IPTYP(1S)
34      C BAR(1S) = 0.70
35      C WRITE(6,600)
36      C CONTINUE
37
38      C
39      C 511
40      C
41      C OPTIMIZE RPM OR DIAMETER OF PROPULSOR
42
43      C
44      C CALL TROOST(VADES(1S),QDES(1S),TDES(1S),RPMDES(1S),DIAM(1S),Z(1S),
45      C 1PD(1S),BAR(1S),KT(1S),KQ(1S),EFFDES(1S),J(1S),ITQ,IPJ,RHOD(IP),
46      C 2IE)
47      C IF(1ERROR(1S).EQ.3.OR.1ERROR(1S).EQ.4) GO TO 515
48
49      C
50      C EVALUATE BLADE AREA RATIO
51
52      C
53      C CALL BURIL( TDES(1S), DIAM(1S), H(1S), VADES(1S), RPMDES(1S),
54      C 1 CAV(1S), BAR(1S), 1ERROR(1S), PD(1S), NRET )
55      C IF ( NRET .NE. 0 ) GO TO 511
56
57      C
58      C 515 CONTINUE
59      C 1ERROR(1S)=100*IE+1ERROR(1S)
60      C RETURN
61      C 600 FORMAT(1H1)
62      C END

```

```

1      SUBROUTINE PROPER(IS,VOF,TOF,PWR,TITLE)
2      C
3      C SUBROUTINE "PROPER" CALCULATES THE OPEN WATER CURVES AND OFF-DESIGN
4      C PERFORMANCE FOR PROPELLOR SYSTEM "IS"
5      C
6      C COMMON/CDESC/RHOD(3),ANUD(3),IP
7      C
8      C COMMON/CPROP/IPTYP(3),DIAM(3),VADES(3),RPMDES(3),TDES(3),QDES(3),
9      C EFFDES(3),OMWTD(3),CAV(3),Z(3),H(3),BAR(3),PD(3),J(3),
10     C IERROR(3),KT(3),KQ(3)
11     C
12     C COMMON/PCOF/CT(4),CO(4)
13     C
14     C COMMON/ROOTC/A(4)
15     C
16     C DIMENSION TITLE(8)
17     C REAL J,KT,KQ,JK,JOF,KTT,KQO
18     C
19     C INTEGER Z
20     C
21     C IJK=0
22     C PDC=PD(IS)
23     C
24     C EVALUATE THE COEFFICIENTS OF THE KT AND KQ POLYNOMIAL
25     C
26     C CALL POLCOF(PDC ,BAR(IS),Z(IS))
27     C JK=0.0
28     C
29     C PRINT OPEN WATER CURVE TABLE
30     C
31     C WRITE(6,905) TITLE
32     C WRITE (6,906)
33     C CONTINUE
34     C
35     C KTT =CT(1)+(CT(2)+(CT(3)+CT(4)*JK )*JK )*JK
36     C KQO =CQ(1)+(CQ(2)+(CQ(3)+CQ(4)*JK )*JK )*JK
37     C EEE=KTT*JK/(KQO*6.2831853)
38     C WRITE (6,902) JK,KTT,KQO,EEE
39     C IF(KTT.LT.0.03) GO TO 970
40     C JK=JK+0.05
41     C IF ( JK .LE. 2.0 ) GO TO 210
42     C GO TO 970
43     C ENTRY PROPERO
44     C
45     C CALCULATE OFF DESIGN PERFORMANCE
46     C
47     C VAFF=VOF*1.6879*OMWTD(IS)
48     C COEFF=TOF/(RHOD(IP)*DIAM(IS)*DIAM(IS)*VAFF*VAFF)
49     C DO 950 I=1,4
50     C A(I)=CT(I)
51     C CONTINUE
52     C CALL ROOTC(PD(IS),Z(IS),BAR(IS),COEFF,2.1,XKT,XKQ,EEE,JOF)
53     C XKQ =CQ(1)+(CQ(2)+(CQ(3)+CQ(4)*JOF )*JOF )*JOF
54     C KXT =CT(1)+(CT(2)+(CT(3)+CT(4)*JOF )*JOF )*JOF
55     C EEE=XKT*JOF/(XKQ*6.2831853)
56     C PWR=RHOD(IP)*XKQ*DIAM(IS)*DIAM(IS)*VAFF*VAFF*VAFF/(87.5352188*
57     C JOF*JOF*JOF)
58     C
59     C CONTINUE
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SUBROUTINE PROPER 74/74 OPT=0 ROUND=\*\*/ TRACE FTN 4.6+460 04/07/81 13.10.59 PAGE 2

60 RETURN  
 905 FORMAT(1H1,\*, TABLE OF OPEN WATER CURVE FOR \*,8A10)  
 906 FORMAT(1H0,\*,  
 902 FORMAT (5X,F10.2,F10.4,F10.5,F10.3)  
 END  
 PROPER 59  
 PROPER 60  
 PROPER 61  
 PROPER 62  
 PROPER 63

```
1      SUBROUTINE PROPP(IS,TITLE)
C
C      THIS ENTRY PRINTS ALL DATA IN COMMON BLOCK "CPROP"
C
5      COMMON/CPROP/IPTYP(3),DIAM(3),VADES(3),RPMDES(3),TDES(3),QDES(3),
1      EFDES(3),OMWTD(3),CAV(3),Z(3),H(3),BAR(3),PD(3),J(3),
2      IERROR(3),KT(3),KQ(3)
C
10     DIMENSION TITLE(8)
C
15     INTEGER Z
C
20     REAL J,KT,KQ
C
25     WRITE(6,700) TITLE
30     WRITE(6,701) VADES(IS),TDES(IS),DIAM(IS),QDES(IS),RPMDES(IS)
1,EFDES(IS),BAR(IS),KT(IS),CAV(IS),PD(IS),KQ(IS),Z(IS),J(IS),
2 IPTYP(IS),IERROR(IS)
C
35     PRINT ERROR MESSAGE
C
C      IR=IERROR(IS)
C      CALL ERROR(IR)
C      RETURN
700  FORMAT(1H1,8A10)
701  FORMAT(12X,31H  PROPULSOR CHARACTERISTICS
1//1X,18HVELOCITY-(KNOTS) -,F9.2,7X,16HTHRUST-(LBS) -,F10.0/1X,
218HDIAMETER-(FEET) -,F9.2,7X,16HTORQUE-(FT-LBS)-,F10.0/1X,
318HRPM -,F8.1/1X,
511HEFFICIENCY-,F7.3,7H BAR-,F6.3,7H KT-,F7.4/1X,
611HCAV OR TIP-,F6.1,8H P/D-,F6.3,7H KQ-,F8.5/1X,
711HNO. BLADES-,13.7X,4HJ -,F6.3//
1X,17HPROPULSOR TYPE -,I4
2/ 1X,17HERROR TYPE -,I4)
END
```

```

1      C
      C
      C
      SUBROUTINE ERROR(IE)
      PRINT ERROR MESSAGE OF PROPULSOR

5      IF(IE.EQ.0) WRITE(6,100)
      IF(IE.EQ.100) WRITE(6,200)
      IF(IE.EQ.200) WRITE(6,300)
      IF(IE.EQ.3) WRITE(6,400)
      IF(IE.EQ.4) WRITE(6,500)
      IF(IE.EQ.5) WRITE(6,600)
      IF(IE.EQ.6) WRITE(6,700)
      RETURN

10     100 FORMAT(1H+,25X,*NO ERROR*)
      200 FORMAT(1H+,25X,*LIMIT VALUE FOR P/D HAS BEEN USED*)
      300 FORMAT(1H+,25X,*ITERATION MALFUNCTION--PD(2) USED FOR P/D*)
      400 FORMAT(1H+,25X,*MAX BAR=.95 USED--MARINE SCREW*)
      500 FORMAT(1H+,25X,*MIN BAR=.4 USED--MARINE SCREW*)
      600 FORMAT(1H+,25X,*MAX TIP SPEED USED--AIR SCREW*)
      700 FORMAT(1H+,25X,*BLADE NUMBER OUTSIDE PROGRAM LIMIT--CLOSEST NUMBER
1      1 USED*)
      END
20

```

```

1  SUBROUTINE TROOST(VA1,P,T,N1,D,Z,PNEW,BAR,KT,KQ,EFFNEW,J,ITQ,IPJ, TROOST 2
   1RHO, IERROR) TROOST 3
5  C THIS SUBROUTINE IS TO BE USED WITH SUBROUTINE ROOT AND FUNCTION CALC. TROOST 4
   C EITHER RPM OR DIAMETER CAN BE OPTIMIZED GIVEN THE OTHER(SEE VARIABLE TROOST 5
   C "IPJ" BELOW) TROOST 6
   C TROOST 7
   C TROOST 8
10  C IF J,PD,ETC. ARE KNOWN AND ONLY KT,KQ AND EFF ARE NEEDED THE SECOND TROOST 9
   C ENTRY TO "TROOST" MAY BE USED. THIS IS "TROOST2" TROOST 10
   C IF OPEN WATER CURVES ARE DESIRED THIS ENTRY POINT LENDS ITSELF EASILY TROOST 11
   C TO GENERATING THESE CURVES. TROOST 12
   C EXPLANATION OF VARIABLES IN THE SUBROUTINE STATEMENT TROOST 13
   C TROOST 14
   C TROOST 15
15  C TROOST 16
   C TROOST 17
   C TROOST 18
   C TROOST 19
   C TROOST 20
20  C TROOST 21
   C TROOST 22
   C TROOST 23
   C TROOST 24
   C TROOST 25
25  C TROOST 26
   C TROOST 27
   C TROOST 28
   C TROOST 29
   C TROOST 30
30  C TROOST 31
   C TROOST 32
   C TROOST 33
   C TROOST 34
   C TROOST 35
35  C TROOST 36
   C TROOST 37
   C TROOST 38
   C TROOST 39
   C TROOST 40
40  C TROOST 41
   C TROOST 42
   C TROOST 43
   C TROOST 44
   C TROOST 45
45  C TROOST 46
   C TROOST 47
   C TROOST 48
   C TROOST 49
   C TROOST 50
50  C TROOST 51
   C TROOST 52
   C TROOST 53
   C TROOST 54
   C TROOST 55
55  C TROOST 56
   C TROOST 57
   C TROOST 58

```

SUBROUTINE TROOST(VA1,P,T,N1,D,Z,PNEW,BAR,KT,KQ,EFFNEW,J,ITQ,IPJ,  
 1RHO, IERROR)  
 C THIS SUBROUTINE IS TO BE USED WITH SUBROUTINE ROOT AND FUNCTION CALC.  
 C EITHER RPM OR DIAMETER CAN BE OPTIMIZED GIVEN THE OTHER(SEE VARIABLE  
 C "IPJ" BELOW)  
 C IF J,PD,ETC. ARE KNOWN AND ONLY KT,KQ AND EFF ARE NEEDED THE SECOND  
 C ENTRY TO "TROOST" MAY BE USED. THIS IS "TROOST2"  
 C IF OPEN WATER CURVES ARE DESIRED THIS ENTRY POINT LENDS ITSELF EASILY  
 C TO GENERATING THESE CURVES.  
 C EXPLANATION OF VARIABLES IN THE SUBROUTINE STATEMENT  
 C  
 C VA1 -WAKED SHIP VELOCITY (KNOTS)  
 C P -TORQUE PER SHAFT(FT-LBS)  
 C T -PROPELLER THRUST (POUNDS) PER SHAFT  
 C N1 -PROPELLER RPM  
 C D -PROPELLER DIAMETER (FEET)  
 C Z -NUMBER OF BLADES PER PROPELLER  
 C PD1 -PITCH (AT 0.7 R) IN FEET DIVIDED BY DIAMETER (IE. P/D)  
 C BAR -BLADE AREA RATIO (EXPANDED AREA/DISC AREA)  
 C KT -THRUST COEFFICIENT (KT=T/(RHO\*N\*\*2\*D\*\*4) )  
 C KQ -TORQUE COEFFICIENT (KQ=Q/(RHO\*N\*\*2\*D\*\*5) )  
 C EFF1 -OPEN WATER EFFICIENCY (EFF=J\*KT/(2\*PI\*KQ) )  
 C J -ADVANCE COEFFICIENT(J=VA/(N\*D) )  
 C ITQ -INDEXING COEFFICIENT-CAN EQUAL ONLY 1 OR 2  
 C 1--THRUST IS AN INPUT  
 C 2--POWER IS AN INPUT  
 C IPJ -INDEXING COEFFICIENT-CAN EQUAL 1 THROUGH 5  
 C 1--NO OPTIMIZATION, J KNOWN, CALCULATES KT,KQ,EFF1 ONLY  
 C 2--OPTIMIZES N WITH KT/J\*\*2  
 C 3--OPTIMIZES N WITH KQ/J\*\*3  
 C 4--OPTIMIZES D WITH KT/J\*\*4  
 C 5--OPTIMIZES D WITH KQ/J\*\*5  
 C RHO -WATER DENSITY FOR PROPELLER OPERATION(LB-SEC\*\*2/FT\*\*4)  
 C  
 C REAL N,J,KT,KQ,N1  
 C  
 C INTEGER Z  
 C  
 C DIMENSION EFF(5),PD(5),S(2),COEFF(5)  
 C  
 C IF(Z.GT.7.OR.Z.LT.2) IERROR=6  
 C IF(Z.GT.7) Z=7  
 C IF(Z.LT.2) Z=2  
 C N=N1/60.  
 C VA=VA1\*1.6878  
 C IF(IPJ.EQ.1) GO TO 21  
 C S(1)=T  
 C S(2)=P\*87.5352186  
 C IF(IPJ.GE.4) COEFF(IPJ)=S(ITQ)\*N/(RHO\*VA\*\*IPJ)  
 C IF(IPJ.LE.3) COEFF(IPJ)=S(ITQ)/(RHO\*D-D\*VA\*\*IPJ)  
 C M=0  
 C DEL PD=.05  
 C PD(3)=0.40  
 C  
 C FIRST FIND 3 POINTS WHICH CONTAIN THE MAXIMUM EFFICIENCY

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74/74 OPT=0 ROUND=\*/ TRACE

SUBROUTINE TROOST

```

C
40 CONTINUE
DO 50 I=1,2
  PD(1)=PD(I+1)
  EFF(I)=EFF(I+1)
CONTINUE
PD(3)=PD(2)+DEL PD
IF(PD(3).GT.1.4) GO TO 97
  M=M+1
CALL ROOT(PD(3).Z,BAR,COEFF(IPJ),IPJ,ITQ,KT,KQ,EFFIN,J)
EFF(3)=EFFIN
IF(M.LE.2.OR.EFF(3).GE.EFF(2)) GO TO 40

C
70 ITERATE TO MAXIMUM EFFICIENCY
C THIS METHOD IS REFERENCED IN--
C "INTRODUCTION TO NUMERICAL ANALYSIS" BY F.B. HILDEBRAND
C MC GRAW-HILL 1956, PAGES 50 AND 56.
C
75 PD(4)=PD(2)-DELPD/2.0
PD(5)=PD(2)+DELPD/2.0
CALL ROOT(PD(4).Z,BAR,COEFF(IPJ),IPJ,ITQ,KT,KQ,EFF(4),J)
CALL ROOT(PD(5).Z,BAR,COEFF(IPJ),IPJ,ITQ,KT,KQ,EFF(5),J)
PDNEW=PD(2)-0.0175*(-EFF(1)-0.5*EFF(4)+0.5*EFF(5)+EFF(3))/
  (EFF(1)-0.5*EFF(4)-EFF(2)-0.5*EFF(5)+EFF(3))
IF(PDNEW.LT.PD(1).OR.PDNEW.GT.PD(3)) GO TO 96

C
80 1 FINAL COMPUTED VALUES OF KT AND KQ ARE COMMON WITH
C SUBROUTINE ROOT AND HAVE ALREADY BEEN CALCULATED
C
85 CALL ROOT(PDNEW,Z,BAR,COEFF(IPJ),IPJ,ITQ,KT,KQ,EFFNEW,J)
GO TO 960
CONTINUE

C
90 ITERATION MALFUNCTION WITH PDNEW OUTSIDE THE LIMITS
C OF PD(1) OR PD(3). THE VALUE AT PD(2) HAS BEEN
C USED.
C
95 IERROR = 2
PDNEW=PD(2)
CALL ROOT(PDNEW,Z,BAR,COEFF(IPJ),IPJ,ITQ,KT,KQ,EFFNEW,J)
CONTINUE
GO TO 100
CONTINUE

C
100 AT THIS POINT P/D=1.4 HAS BEEN USED AND THE SEARCH FOR
C THE MAXIMUM HAS BEEN TERMINATED
C
105 IERROR = 1
EFFNEW=EFF(2)
PDNEW=PD(2)
CONTINUE
IF(IPJ.LE.3) NT=VA1-101.268/(D*J)
IF(IPJ.GE.4) D=VA1-1.6878/(N1/60.0)*J)
P=KQ-RHQ*N1-D**5/3600.
WRITE (6,988) VA1,J,PDNEW
GO TO 30
CONTINUE

C
21 CONTINUE

```

```

115 PDX=0.0
    DPD=0.2
    PDY=1.72
    J=VA/(N*D)
    KT=T/(RHO*N*D*D*D)
    XY=CALC(J,BAR,PDY,Z,1)
    WRITE(6,989)
    WRITE(6,990) VA1,J,KT,PDY
    IF(KT.GT.XY) GO TO 28
    PDX=PDY
    CONTINUE
22 PDX=PDY-DPD
    XX=CALC(J,BAR,PDX,Z,1)
    WRITE(6,990) VA1,J,KT,PDY,PDX,XX
    IF(KT.LT.XX) GO TO 22
    CONTINUE
23 DPD=(PDY-PDX)*((KT-XY)/(XY-XX))
    XX=XY
    PDX=PDY
    PDY=PDY+DPD
    XY=CALC(J,BAR,PDY,Z,1)
    WRITE(6,990) VA1,J,KT,PDY,PDX,XX,XY
    IF(ABS(KT-XY).GT.0.0001) GO TO 23
    PDNEW=PDY
    CALL TROST2(KT,KQ,J,PDNEW,BAR,Z,EFFNEW)
    IERROR=0
    GO TO 29
    CONTINUE
28 C
    C
    C      AT THIS POINT P/D=1.4 HAS BEEN USED
    PDNEW = 1.4
    IERROR = 1
    CALL TROST2(KT,KQ,J,PDNEW,BAR,Z,EFFNEW)
29 CONTINUE
    P=KQ-RHO*N*D*D*D
    CONTINUE
30 RETURN
    988 FORMAT(1H,* FIRST LOOP - ROOT CALL*,8F10.3)
    989 FORMAT(1H,* SECOND LOOP - CALC CALL*)
    990 FORMAT(20X,6(F10.3,2X))
    END
116 TROOST
117 TROOST
118 TROOST
119 TROOST
120 TROOST
121 TROOST
122 TROOST
123 TROOST
124 TROOST
125 TROOST
126 TROOST
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74/74 OPT=0 ROUND=0/ TRACE

SUBROUTINE ROOT

```

515      TQ1=TQ1-COEFF-J2**IPJ
        CONTINUE
        IF (ABS(TQ1)-EPS.LE.0.) GO TO 52
        DE=DEL*TQ1/(TQ2-TQ1)
        IF (ABS(DE).LT.ABS(DEL)) GO TO 518
        DEL=SIGN(DEL,DE)
        GO TO 519
518      CONTINUE
        DEL=DE
519      CONTINUE
        I=I+1
        GO TO 51
52      CONTINUE
        IF (IJK.EQ.2) GO TO 53
        KT=CALC(J2,BAR,PD,Z,1)
        KQ=CALC(J2,BAR,PD,Z,2)
        EFFIN=KT*J2/(KQ-6.2831853)
53      CONTINUE
        RETURN
        END

```

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ROOT
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1      C
      SUBROUTINE BURIL( T,D,H,VA,N,CAVI,BAR,IERROR,PD,NRET)
      THIS SUBROUTINE USES BURRILL'S CAVITATION CRITERIA TO DETERMINE
      IF THE BAR USED IS SUFFICIENT AND, IF IT IS NOT, TO ESTIMATE
      WHAT BAR IS NECESSARY
      COMMON/BARCK/IE
      REAL N
      NRET = 0
      BARC=BARB
      BARB=BAR
      THRUST=T
      AD=0.7853975*D*D
      DELTP=14.45+0.45*H
      QSUBT=(VA/7.12)**2+(N*D/329.0)**2
      SIGN=DELTP/QSUBT
      TAU=0.17096999E-1
      1+.23641524*SIGN
      1-.52794965E-2*CAVI
      1+.78910550E-1*SIGN-CAVI
      1+.42061131E-5*SIGN-CAVI**3
      1-.98059874E-1*SIGN**2-CAVI
      1-.40621894E-2*SIGN**2-CAVI**2
      1-.18207486E-7*SIGN**2-CAVI**5
      1+.75936652E-2*SIGN**3-CAVI
      1+.92023581E-2*SIGN**3-CAVI**2
      1-.17649923E-3*SIGN**5-CAVI**2
      1-.34804349E-4*SIGN**5-CAVI**4
      1+.99981727E-6*SIGN**5-CAVI**5
      AP=THRUST/(TAU-QSUBT*144.0)
      PAR=AP/AQ
      EAR=PAR/(1.067-0.229*PD)
      IF(ABS(BAR-EAR).LE.0.0005) GO TO 90
      IF((IE.EQ.1.AND.ABS(EAR-BARC).LE.0.01)) GO TO 95
      BAR=EAR
      IF(BAR.GT.0.95) GO TO 70
      IF(BAR.LT.0.4) GO TO 80
      NRET = 1
      GO TO 95
      CONTINUE
      EAR IS GREATER THAN 0.95, USE 0.95 FOR EAR
      BAR = 0.95
      IERROR = 3
      NRET = 1
      GO TO 95
      CONTINUE
      EAR IS LESS THAN 0.4 USE 0.4 FOR BAR
      BAR=0.4
      IERROR = 4
      NRET = 1
      GO TO 95

```

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OPT=0 ROUND=0/ TRACE

74/74

SUBROUTINE BURIL

BURIL 59  
BURIL 60  
BURIL 61  
BURIL 62  
BURIL 63

90 CONTINUE  
95 IERROR = 0  
CONTINUE  
RETURN  
END

60

1		SUBROUTINE POLCOF(PD,BAR,Z)	2	POLCOF
	C		3	POLCOF
	C	DETERMINE THE COEFFICIENTS OF THE POLYNOMIALS WHICH APPROXIMATE	4	POLCOF
	C	KT AND KQ CURVE	5	POLCOF
5	C		6	POLCOF
	C	COMMON/OFFDES/PJAY(4)	7	POLCOF
	C		8	POLCOF
	C	COMMON/PCOF/CT(4),CQ(4)	9	POLCOF
10	C		10	POLCOF
	C	REAL KT,KQ,J	11	POLCOF
	C	INTEGER Z	12	POLCOF
	C		13	POLCOF
		J=0.0	14	POLCOF
15		KT=CALC1(J,BAR,PD,Z,1)	15	POLCOF
		DO 5 I=1,4	16	POLCOF
		CT(I)=PJAY(I)	17	POLCOF
	5	CONTINUE	18	POLCOF
		KQ=CALC1(J,BAR,PD,Z,2)	19	POLCOF
20		DO 7 I=1,4	20	POLCOF
		CQ(I)=PJAY(I)	21	POLCOF
	7	CONTINUE	22	POLCOF
		RETURN	23	POLCOF
		END	24	POLCOF
			25	POLCOF

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74/74 CPT=0 ROUND=// TRACE

SUBROUTINE BESSJ

```

1      SUBROUTINE BESSJ(X,N,VJ)
      C
      C      EVALUATE BSESL FUNCTION FROM ORDER 0 TO ORDER N
      C
5      REAL J, JL, JLL, JLLL
      DIMENSION VJ(N)
      DATA PI /3.1415926535898/,
1      EPS /1.0E-30/,
2      EXPON /2.7182818284590/
      C
10     DETERMINE THE MAXIMUM N = NU
      C
      C
      C      D = ALOG(EPS)/X
      C      C = ALOG(EXPON/2.0)
      C      B = D-2.0-C
15     ALPHA = (-B+SQRT(B**2-4.0*D*(2.0-C)))/(2.0*(2.0-C))
      CLN = ALOG(2.0*PI*X)
      IF(ALPHA.LT.1.5) ALPHA = 1.5
      DO 1000 I=1,20
20      ALN = ALOG(ALPHA)
      F = -(CLN+ALN)/(2.0*X)+ALPHA*(C-ALN)-D
      FP = -1.0/(2.0*X+ALPHA)+C-1.0-ALN
      DEL = F/FP
      ALPHA = ALPHA-DEL
25      IF(X*ABS(DEL) .LE. 0.01) GO TO 1100
      CONTINUE
1000  GO TO 8888B
1100  CONTINUE
      GNU = ALPHA-X
      NU = IFIX(GNU)+1
30      IF(NU.LT.N+10) NU = N+10
      IF((NU/2)*2.NE.NU) NU=NU+1
      C
      C      RECURSE IN PLACE FOR M.GT.N
      C
35      SUM = 0.0
      JLLL = 0.0
      JLL = EPS
      NUM1 = NU-1
      NP = N
40      IF((NP/2)*2.EQ.NP) NP = NP-1
      DO 1200 MM = NP,NUM1,2
      M = NUM1-MM+NP
      JL = 2.0*FLOAT(M+2)-JLL/X-JLLL
      J = 2.0*FLOAT(M+1)-JL/X-JLL
      SUM = SUM+2.0*JL
      JLLL = JL
      JLL = J
1200  CONTINUE
      IF(NP.NE.N) GO TO 1300
      JL = 2.0*FLOAT(N)*JLL/X-JLLL
      SUM = SUM+2.0*JL
      JLLL = JLL
      JLL = JL
1300  CONTINUE
      I = N+1
      VJ(I) = JLLL

```

```

60      VJ(N) = JLL
      NP = N-1
      DO 1400 MM = 1,NP
      M = NP-MM
      K = M+1
      VJ(K) = 2.0*FLOAT(K)*VJ(M+2)/X-VJ(M+3)
      IF((M/2)*2.EQ.N) SUM = SUM+2*VJ(M+1)
      1400 CONTINUE
      SUM = SUM-VJ(1)
      K = N+1
      DO 1500 M = 1,N
      VJ(M) = VJ(M)/SUM
      1500 CONTINUE
      99999 CONTINUE
      RETURN
      88888 CONTINUE
      WRITE(6,100) X, ALPHA, DEL
      100 FORMAT(28H NO CONVERGENCE, X, ALPHA, DEL/3E14.7)
      END
      BESSJ 59
      BESSJ 60
      BESSJ 61
      BESSJ 62
      BESSJ 63
      BESSJ 64
      BESSJ 65
      BESSJ 66
      BESSJ 67
      BESSJ 68
      BESSJ 69
      BESSJ 70
      BESSJ 71
      BESSJ 72
      BESSJ 73
      BESSJ 74
      BESSJ 75
      BESSJ 76
      BESSJ 77

```



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74/74 OPT=0 ROUND=+/- TRACE

SUBROUTINE PCHEB

```

1      C
2      SUBROUTINE PCHEB (AS, BS, AB, BB, NN, TITLE)
3      C
4      C
5      C
6      C
7      C
8      C
9      C
10     C
11     C
12     C
13     C
14     C
15     C
16     C
17     C
18     C
19     C
20     C
21     C
22     C
23     C
24     C
25     C
26     C
27     C
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34     C
35     C
36     C
37     C
38     C
39     C
40     C
41     C
42     C
43     C
44     C
45     C
46     C
47     C
48     C
49     C
50     C
51     C
52     C
53     C
54     C
55     C
56     C
57     C
58     C

```

PLOT BODY SECTIONAL AREA CURVE AND STRUT WATERPLANE OUTLINE CURVE  
 INPUTS  
 AS AND BS ARE, RESPECTIVELY, THE VECTORS OF SYMMETRIC-  
 AND OF ANTISYMMETRIC-CHEBYCHEV COEFFICIENTS FOR THE STRUT.  
 AB AND BB ARE, RESPECTIVELY, THE VECTORS OF SYMMETRIC-  
 AND OF ANTISYMMETRIC-CHEBYCHEV COEFFICIENTS FOR THE BODY.  
 NN = DIMENSION OF AS, BS, AB, BB  
 MAXIMUM VALUE OF NN IS NMAX  
 NMAX = 10

INITIALIZE THE GRID GEOMETRY, THE PLOT VARIABLES AND  
 THE ABSCISSA VARIABLE.

COMMON/PLOT/NFIRST,NLAST,NPOINT,XMAX,XMIN,NSCL1,NCHAR,NSCALE(4),  
 PCHAR(2)  
 COMMON/XRPLLOT/II,JJ,KK,LL,NHL,NSBH,NVL,NSBV,HCHAR,VCHAR,  
 ISX,ISY,V,H  
 LOGICAL NSCL1

DIMENSION AS(NN), BS(NN), AB(NN), BB(NN), TITLE(8)  
 DIMENSION STAT(101),YS(101),YB(101),LABEL(3)

GENERATE ORDINATE VALUES FOR STRUT AND BODY POINTS

```

DO 2000 I=1, 101
  STAT(I)=2.0*(FLOAT(I-1)*.01-.5)
  THETA=ASIN(STAT(I))
  YS(I)=0.0
  YB(I)=0.0
  DO 1000 NCO=1,NN
    UM=COS(FLOAT(2*NCO-1)*THETA)
    VM=SIN(FLOAT(2*NCO)*THETA)
    YS(I)=YS(I)+AS(NCO)*UM+BS(NCO)*VM
    YB(I)=YB(I)+AB(NCO)*UM+BB(NCO)*VM
  1000 CONTINUE
2000 CONTINUE

```

DETERMINE THE MINIMUM AND MAXIMUM ORDINATE VALUES

```

YMAX = -9999999.0
YMIN = +9999999.0
DO 3000 J=1, 101
  IF(YMAX.LT. YB(J)) YMAX=YB(J)
  IF(YMAX.LT. YS(J)) YMAX=YS(J)
  IF(YMIN.GT. YB(J)) YMIN=YB(J)
  IF(YMIN.GT. YS(J)) YMIN=YS(J)
3000 CONTINUE

```

CALL PLOT1 TO SET UP GRID SPACING AND DETERMINE THE AXIS VALUES

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TRACE

74/74

SUBROUTINE PCHEB

```

C
C
60      CALL PLOT1 (NSCALE,NHL,NSBH,NVL,NSBV,HCHAR,VCHAR)
C
C      CALL PLOT2 TO EXAMINE THE MINIMUM AND MAXIMUM VALUES OF
C      ABSCISSA AND ORDINATE AND TO ESTABLISH AN INTERNAL FORMULA
C      FOR COMPUTING THE LOCATION IN THE IMAGE REGION CORRESPONDING
C      TO THE POINT TO BE PLOTTED.
C      WHEN NSCL1=.TRUE., THE STANDARD GRID WILL NOT BE USED
65      CALL PLOT2 (XMAX,XMIN,YMAX,YMIN,NSCL1)
C
C      CALL PLOT3 FOR ASSIGNING AN ALPHA-CHARACTER TO EACH POINT
C      WHICH WILL BE PLOTTED.
70      CALL PLOT3 (PCHAR(1),STAT,YS,NF:RST,NLAST,NPOINT)
C      CALL PLOT3 (PCHAR(2),STAT,YB,NF:RST,NLAST,NPOINT)
C
C      PRINT THE HEADING OF THE PLOT
75      WRITE (6,9000) (TITLE(I), I=1,8)
C
C      CALL PLOT4 TO PRINT THE IMAGE OF THE COMPLETED GRAPH ON THE
C      PRINTER, INCLUDING THE VALUES OF ABSCISSA AND ORDINATE AT
C      THE GRID LINES OUTSIDE THE BOTTOM AND LEFT EDGE OF THE GRAPH
C
C      CALL PLOT4 (LABLE,NCHAR)
C
C      RETURN
C
C
80      9000 FORMAT(1H1,32X,64HBODY SECTIONAL AREA CURVE AND STRUT WATERPLANE O
C          1UTLINE CURVE FOR//25X,8A10)
C          END
90

```

1		SUBROUTINE PLOT1 (NSCALE,A,B,C,D,E,F)	2
C			PLOT1
C		SETUP SPACING AND DETERMINE THE AXIS VALUES	PLOT1
C			PLOT1
5	C		PLOT1
		INTEGER A,B,C,D	PLOT1
		LOGICAL V,H	PLOT1
	C		PLOT1
		DIMENSION NSCALE(4)	PLOT1
10	C		PLOT1
		COMMON/XRPLOTO/I,J,K,L,NHL,NSBH,NVL,NSBV,HCHAR,VCHAR,ISX,ISY,V,M	PLOT1
	C		PLOT1
		I=NSCALE(1)	PLOT1
15		J=NSCALE(2)	PLOT1
		K=NSCALE(3)	PLOT1
		L=NSCALE(4)	PLOT1
		NHL=A	PLOT1
		NSBH=B-1	PLOT1
		NVL=C	PLOT1
20		NSBV=D-1	PLOT1
		HCHAR=E	PLOT1
		VCHAR=F	PLOT1
		RETURN	PLOT1
		END	PLOT1

```

1      SUBROUTINE PLOT2(XMAX,XMIN,YMAX,YMIN,NSCL1)
C
C      EXAMINE THE MINIMUM AND MAXIMUM VALUES OF ABSCISSA AND ORDINATE
C      AND ESTABLISH AN INTERNAL FORMULA FOR COMPUTING THE LOCATION
C      IN THE IMAGE REGION CORRESPONDING TO THE POINT TO BE PLOTTED
C
C
10     REAL LIN
      INTEGER VCT,VLC,T,HCT,HLCT
      LOGICAL NSCL1,V,H
C
      DIMENSION LIN(110)
C
      COMMON/XPLOTG/XL,XH,YL,YH,XI,YI,XMOV,YMOV
      COMMON/XPLOTG/GRAF(11,204)
      COMMON/XPLOTG/II,JJ,KK,LL,NHL,NSBH,NVL,NSBV,HCHAR,VCHAR,IX,IY,V,H
C
      IF(NSCL1) GOTO 1
      II=0
      JJ=3
      KK=0
      LL=3
      NHL=6
      NVL=11
      NSBH=9
      NSBV=9
      HCHAR=1L-
      VCHAR=1LI
C
1      CONTINUE
      HLCT=0
      HCT=NSBH
      DO 2 I=1,204
        IF(HLCT.EQ.NHL) GOTO 3
        IY=I
        IX=J
        VLCT=0
        VCT=NSBV
        DO 4 J=1,110
          IF(VLCT.EQ.NVL) GO TO 5
          IX=J
          IF(VCT.EQ.NSBV) GOTO 6
          LIN(J)=1L
          GOTO 40
        CONTINUE
        LIN(J)=VCHAR
        VCT=-1
        VLCT=VLCT+1
40     CONTINUE
        VCT=VCT+1
4      CONTINUE
5      CONTINUE
        VLCT=0
        IF(HCT.NE.NSBH) GOTO 7
        HCT=-1
        HLCT=HLCT+1
        DO 8 J=1,IX
          LIN(J)=HCHAR
8      CONTINUE

```

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04/07/81 13.10.59

FTN 4.6+460

SUBROUTINE PLOT2 74/74 OPT=0 ROUND=0/ TRACE

```

60      7  CONTINUE
        HCT=HCT+1
        IQ=IX+1
        DO 10 J=IQ,110
            LIN(J)=1L
        10 CONTINUE
        ENCODE(110,9,GRAF(1,1)) (LIN(J),J=1,110)
        2  CONTINUE
        3  CONTINUE
        XL=XMIN
        XH=XMAX
        YL=YMIN
        YH=YMAX
        XI=(XH-XL)/FLOAT(IX-1)
        YI=(YH-YL)/FLOAT(IY-1)
        XMOV=1.0-XL/XI
        YMOV=1.0-YL/YI
        V=.TRUE.
        H=.TRUE.
        RETURN
        9  FORMAT(110A1)
        END
        PLOT2 59
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        PLOT2 66
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        PLOT2 79
        PLOT2 80

```

SUBROUTINE PLOT3

```

1 SUBROUTINE PLOT3 (PCHAR,X,Y,SDATA,FDATA,DDATA)
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4 C
5 C ASSIGN AN ALPHA-CHARACTER TO EACH POINT WHICH WILL BE PLOTTED
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1      C      SUBROUTINE PLOT4(MCHAR,NCHAR)
2      C
3      C      PRINT THE IMAGE OF THE COMPLETED GRAPH ON THE PRINTER,
4      C      INCLUDING THE VALUES OF THE ABSCISSA AND ORDINATE AT THE
5      C      GRID LINES OUTSIDE THE BOTTOM AND LEFT EDGES OF THE GRAPH
6      C
7      C
8      C
9      C      INTEGER SA, SB, SC
10     C      INTEGER CT,PDQ
11     C      LOGICAL V,M
12     C
13     C      DIMENSION HNUM(15), MCHAR(3), LCHAR(30), VGFM(3), HLFMT(3)
14     C
15     C      COMMON/XRPLTQ/XL,XH,YL,YH,XI,YI,XMOV,YMOV
16     C      COMMON/XRPLTG/GRAF(11,204)
17     C      COMMON/XRPLTQ/I,J,K,L,NHL,NSBH,NVL,NSBV,HCHAR,VCHAR,ISX,ISY,V,H
18     C
19     C      SA=NSBV
20     C      SC=NCHAR
21     C      SB=NVL
22     C      KQ=1
23     C      CALL QPLOT25(PDQ)
24     C      ENCODE(26,2,VGFM(1))J
25     C      IF(NSBV.LE.0) NSBV=10
26     C
27     C      4 CONTINUE
28     C      IF(NSBV.GT. 10) GO TO 3
29     C      NSBV=NSBV+2
30     C      NVL=NVL
31     C      NVL=XVL/2.0+.5
32     C      KO=KQ+1
33     C      GO TO 4
34     C
35     C      3 CONTINUE
36     C      NNN=NVL-1
37     C      MMM=NSBV-8
38     C      ENCODE(25,5,HLFMT(1)) PDQ,L,NNN,MMM,L
39     C      IF (NCHAR.NE.0) GOTO 14
40     C      NCHAR=1
41     C      LCHAR(1)=1L
42     C      GO TO 15
43     C
44     C      14 CONTINUE
45     C      DECODE(10,17,MCHAR(1)) (LCHAR(IJ),IJ=1,10)
46     C      DECODE(10,17,MCHAR(2)) (LCHAR(IJ),IJ=11,20)
47     C      DECODE(10,17,MCHAR(3)) (LCHAR(IJ),IJ=21,30)
48     C
49     C      15 CONTINUE
50     C      MCT=0
51     C      NSPC=(ISY-NCHAR)/2
52     C      LCT=0
53     C      CT=NSBH
54     C      DO 6 MMNX=1,ISY
55     C      N=ISY-MMNX + 1
56     C      IF (MMNX.LE.NSPC.OR.LCT.GT.NCHAR) GO TO 7
57     C      LCT=LCT+1
58     C      LCR=LCHAR(LCT)
59     C      GO TO 8
60     C
61     C      7 CONTINUE
62     C      LCR=1L
63     C
64     C      8 CONTINUE

```

```

60      IF (CT.EQ.NSBH.AND.H) GO TO 9
        PRINT 1,LCR,(GRAF(I,N),I=1,11)
        GO TO 13
9        CONTINUE
        CT=1
        QNN=(YH-MCT+YI)*10.**I
        PRINT VGFMT,LCR,QNN,(GRAF(I,N),I=1,11)
        MCT=MCT+NSBH+1
13       CONTINUE
        CT=CT+1
6        CONTINUE
        MCT=0
        IF(.NOT.V) GO TO 12
        DO 10 N=1,NVL
            HNUM(N)=(XL+MCT+XI)*10.**K
            MCT=MCT+NSBV+KQ
10        CONTINUE
        PRINT 11
        PRINT HL FMT,(HNUM(N),N=1,NVL)
12       CONTINUE
        NSBV=SA
        NVL=SB
        NCHAR=SC
        RETURN
1       FORM=I(1H,A1,16X,11A10)
2       FORMAT(15H(1H,A1,3X,F10.,I1,10H,3X,11A10))
5       FORMAT(1H(,12,6HX,F10.,I1,1H,I2,1H(,12,6HX,F10.,I1,2H)))
11      FORMAT(1H0)
17      FORMAT(10A1)
        END
59      PLOT4
60      PLOT4
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1      C      SUBROUTINE QPLOTZS(PDQ)
          INTEGER A,B,C,D,PDQ
          LOGICAL V,H
5      C      COMMON/XRPLDTF/XL,XH,YL,YH,XI,YI,XM,YM
          COMMON/XRPLDTQ/II,JJ,KK,LL,A,B,C,D,E,F,M,N,V,H
          C
          X=ABS(XL)
          IF(X.LT.XH) X=XH
          K=0
          DO 1 I=1,11
              XU=10**((I-1)
              IF(X.GT.XU) GOTO 2
              K=K+1
          1 CONTINUE
          2 CONTINUE
          PDQ=1
          IF(LL.EQ.0) PDQ=0
          QQ=PDQ+KK+LL+K
          PDQ=14.0-(10.0-QQ)/2.0
          RETURN
          END
20

```

```

1      C
      C
      C
      FUNCTION FORMDR(VL)
      EVALUATE FORM DRAG COEFFICIENT
      DIMENSION X(9), Y(9)
      DATA X / 1.325, 1.38, 1.43, 1.48, 1.55, 1.68, 1.9, 2.2, 2.5 /
      DATA Y / .51, .71, .84, .85, .83, .75, .65, .57, .50 /
      IF (VL.GE.1.325.AND.VL.LT.2.5) GO TO 4
      FORMDR=0.5
      GO TO 5
      4 FORMDR = YINTP (VL,X,Y,9)
      5 RETURN
      END
10
2      FORMDR
3      FORMDR
4      FORMDR
5      FORMDR
6      FORMDR
7      FORMDR
8      FORMDR
9      FORMDR
10     FORMDR
11     FORMDR
12     FORMDR
13     FORMDR
14     FORMDR

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```

1      C
      C
      C
      FUNCTION YINTP (XA,X,Y,N)
      INTERPOLATING THROUGH A SET OF DISCRETE DATA
      DIMENSION X(1), Y(1)
      1 DO 10 I=1,N
      IF (X(I)-XA) 10,10,2
      2 IN=I-2
      IF(IN) 4,4,6
      4 IN=1
      GO TO 12
      6 NN=N-3
      IF (IN-NN) 12,12,8
      8 IN=NN
      GO TO 12
      10 CONTINUE
      12 IO=IN+3
      YINTP=0.
      DO 20 I=IN,IO
      PROD=Y(I)
      DO 16 J=IN,IO
      IF (I-J) 15,16,15
      15 PROD=PROD*(XA-X(J))/(X(I)-X(J))
      16 CONTINUE
      20 YINTP=YINTP+PROD
      21 RETURN
      END

```

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